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## BIOLOGY AND MEDICINE

## RADIATION EFFECTS

**3408** CH-3782

Argonne National Lab., Lemont, Ill.

BIOLOGY DIVISION QUARTERLY REPORT [FOR]

NOVEMBER 1946 TO JANUARY 1947. Austin M. Brues, ed. Feb. 1, 1947. Decl. Dec. 20, 1955. 101p.

Contract W-31-109-eng-38. \$15.30(ph OTS);

\$5.40(mf OTS).

**3409** HW-38198

Hanford Atomic Products Operation, Richland, Wash.

RADIOLOGICAL SCIENCES DEPARTMENT RESEARCH AND DEVELOPMENT ACTIVITIES. Quarterly Progress Report April-June, 1955. H. M. Parker. July 11, 1955. Decl. Dec. 6, 1955. 31p. Contract W-31-109-eng-52. \$4.80(ph OTS); \$2.70(mf OTS).

Progress is reported in the radiobiological-ecological survey of the Columbia River; the effects of  $\beta$  particles from  $\text{Ru}^{106}$  plaques mounted against the skin of swine and rabbits; the tissue distribution of Pu following intragastric administration in swine; factors affecting the cutaneous absorption of Pu in swine; the tissue distribution and maximum permissible concentration of Ru in rats; tritium absorption and metabolism in rats; the radioisotope build-up in rats receiving reactor effluent as drinking water; factors influencing the uptake of fission products in plants; and modifications in methods of radiation monitoring and waste disposal. (C.H.)

## RADIATION HAZARDS AND PROTECTION

**3410** HW-25239

Hanford Works, Richland, Wash.

RECAPITULATION OF TOLERABLE CONCENTRATION OF RADIOIODINE ON EDIBLE PLANTS. Aug. 4, 1952. Decl. Dec. 6, 1955. 5p. \$1.80(ph OTS); \$1.80(mf OTS).

Preliminary results from a two-year study led to the conclusion that sheep will be undamaged if fed  $5 \mu\text{C I}^{131}/\text{day}$ . The corresponding limit on vegetation consumed is  $6 \times 10^{-5} \mu\text{C I}^{131}/\text{gm}$ . (C.H.)

**3411** K-236

Carbide and Carbon Chemicals Corp. [K-25 Plant], Oak Ridge, Tenn.

DESIGN OF AIR-BORNE ALPHA EMITTER SAMPLER.

D. J. Johnson. June 30, 1948. Decl. Nov. 29, 1955. 9p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

An investigation was undertaken to determine the feasibility of either redesigning the existing air-borne alpha emitter sampler (vacuum cleaner type) or to provide a substitute which would overcome some of the undesirable features of the existing sampling unit. As the present unit could not be lightened sufficiently to meet the weight requirements of a redesigned unit, it was decided to use a

light weight, high speed industrial type blower. Flow measurement was accomplished by installing a small pressure gauge, calibrated in CFM, up-stream of a fixed orifice on the discharge nozzle. The flow regulator consisted of a simple Butterfly valve located between the filter holder and the blower section nozzle. One unit was assembled and field tested with satisfactory results. (auth)

**3412** M-4087

Monsanto Chemical Co., [Dayton, Ohio].

GENERAL HEALTH SAFETY RULES. Louis B. Silverman. Apr. 7, 1944. Decl. Nov. 29, 1955. Includes Attachment: HEALTH METER. Apr. 26, 1944. 11p. \$3.30(ph OTS); \$2.40(mf OTS).

Several rules and procedures are outlined for persons working in hot laboratories or areas. (C.W.H.)

**3413** NYO-5163

Mallinckrodt Chemical Works, St. Louis.

RADON MEASUREMENTS IN WAREHOUSE AND BOX CARS CONTAINING HIGH GRADE ORE. S. H. Anonsen. Feb. 11, 1946. Decl. Dec. 1, 1955. 5p. Contract [W-14-108-eng-8]. \$1.80(ph OTS); \$1.80(mf OTS).

## TOXICOLOGY STUDIES

**3414** M-4337

Rochester, N. Y. Univ.

REPORT ON THE ACUTE TOXICITY FRACTIONS OF  $\text{C}_7\text{F}_{14}$  AND  $\text{C}_8\text{F}_{18}$ . C. J. Spiegl and Benjamin Amdur. Dec. 27, 1945. Decl. Dec. 7, 1955. 5p. \$1.80(ph OTS); \$1.80(mf OTS).

Approximate animal inhalation toxicity studies of the vapors of  $\text{C}_7\text{F}_{14}$  and  $\text{C}_8\text{F}_{18}$  "Low Boiler" performed for periods of 3 and 14 hr duration in rats and mice have indicated a toxicity of the same order as that of  $\text{CCl}_4$  for each of the materials. Animals survived for 14 days following a 14-hr exposure to a concentration of 1.4 mg/l of  $\text{C}_7\text{F}_{14}$  and a concentration of 1.1 mg/l of  $\text{C}_8\text{F}_{18}$ . A comparison of repeated exposure was dangerous. (auth)

## CHEMISTRY

**3415** CC-3069

[Carnegie Inst. of Tech., Pittsburgh]

THE SOLUBILITY OF HELIUM IN TUBALLOY [(URANIUM)]. "A" Report No. 7 [for] Period May 1, 1944 to January 31, 1945. H. Seltz and C. W. Young. June 28, 1945. Decl. Dec. 15, 1955. 16p. Contract W-7405-eng-277. \$3.30(ph OTS); \$2.40(mf OTS).

Uranium was allowed to stand in contact with He at one atm. pressure at a fixed temperature for an extended period, the excess He was pumped off quickly, the system closed off, and the pressure increase measured as a func-



tion of time. The metal was employed both in the form of a powder and for massive measurements. Under the conditions used the amount of He dissolved was not more than  $10^{-7}$  moles per mole of U, and possibly no He was dissolved. (C.H.)

### 3416 CL-1039

Chicago. Univ. Metallurgical Lab.

SOLUBILITY DATA ON INORGANIC COMPOUNDS OF RARE EARTHS, PROTOACTINIUM, THORIUM, URANIUM, NEPTUNIUM, AND PLUTONIUM. Sol Wexler, comp. Nov. 5, 1943. Decl. Dec. 13, 1955. 15p. Contract [W-7405-eng-37]. (A-1432). \$4.80(ph OTS); \$2.70 (mf OTS).

Data on inorganic compounds of the rare earths, Pa, Th, U, Np, and Pu, which are insoluble in water, are given in tabular form. The material is divided into five sections: the name and formula; the conditions of precipitation; the solubility in various inorganic solvents; miscellaneous properties such as color, products on ignition, etc.; and the references. Quantitative solubility data are given where it has been found in the literature. Compounds have been listed in alphabetical order. (auth)

### 3417 NYO-5148

Mallinckrodt Chemical Works, St. Louis.

PACKAGING AND STORAGE OF [ORE REFINERY] RESIDUE CAKES. J. Harold Yeager. Dec. 14, 1945. Decl. Dec. 7, 1955. 7p. Contract W-14-108-eng-8. \$1.80(ph OTS); \$1.80(mf OTS).

It was found that ore refinery residue cakes could be best neutralized by using a strong caustic solution and adding 5 to 7 lbs of NaOH per 100 lbs of wet gangue. The most successful containers used to store the neutralized cake were new W-11 lacquered clamp-top drums. Reconditioned or second-hand drums were not considered satisfactory. Wooden kegs were also considered unsatisfactory because of leakage between the staves. Drying of the neutralized cake was tried and found to be the best method for storage. This method was disregarded in favor of the wet method because of the space and expense required for a dryer. (J.E.D.)

### 3418 RMO-2726

Tennessee Valley Authority, Wilson Dam, Ala.

UTILIZATION OF FLORIDA LEACHED ZONE MATERIAL. PROGRESS REPORT [FOR] MAY 1954. May 27, 1954. Decl. Dec. 22, 1955. 12p. \$1.80(ph OTS); \$1.80(mf OTS).

In one of the processes studied for the beneficiation of leached zone ore, about two-thirds of the phosphate and uranium are separated as a slime concentrate after a preferential grinding operation. Quartz gangue then is floated from the tailing to leave a secondary concentrate of granular phosphate. The adverse effect of residual slime in the flotation step is reduced by desliming the tailing twice at  $40 \mu$  with a hydraulic cyclone. In batch flotation tests on the twice-deslimed sand, 92% of the phosphate was recovered at a grade of 31.7%  $P_2O_5$  with the use of 0.3 lb of collector per ton of dry feed; at the same time 84% of the uranium was recovered at a grade of 0.017% uranium. In continuous flotation tests, 63% of the phosphate and uranium were recovered at a grade of 31.8%  $P_2O_5$  and 0.016% uranium with the use of 0.4 lb of collector per ton of dry feed. Tests of the production of fertilizer from Florida leached zone ore were continued. Calcined, unbeneficiated leached zone ore was extracted in the pilot plant with 0.9

lb  $H_2SO_4$  and 0.9 lb  $HNO_3$  per lb of  $P_2O_5$  in the ore. When the extract was ammoniated to a pH of 6 or less, the loss of nitrogen on drying the ammoniated slurry at  $200^\circ F$  in a laboratory oven was less than 1%. When the slurry had a pH of 7.7, 8% of the nitrogen was lost. Other tests indicated that it would be necessary to increase the ratio of recycle fines to ammoniated slurry in the granulation step as the proportion of sulfuric acid used in extraction was increased. Preliminary studies were made on a bench scale of separating the ammonium nitrate and tributyl phosphate-kerosene from the uranium by washing the filter cake with water. (auth)

## ANALYTICAL PROCEDURES

### 3419 A-1076

Madison Square Area, Manhattan District, New York.

ANALYTICAL INFORMATION REPORT FOR THE PERIOD FEBRUARY 16-MARCH 31, 1945. Apr. 1, 1946. Decl. Dec. 8, 1955. 57p. \$9.30(ph OTS); \$3.60(mf OTS).

Procedures are presented for the indirect titration of U with potassium bromate; the spectrographic determination of Fe, Mg, and Mn in high-purity U metal and oxides; procedures for the determination of minute traces of Cu, Ni, Fe, Co, Zn, Pb, and Cd by a combined electrolysis-distillation-polarographic method; the colorimetric determination of Fe; the spectrophotometric determination of U; the spectrophotometric determination of Mg; the colorimetric determination of Mn and Mg; a comparison of the gravimetric and volumetric methods for the determination of free  $UO_2$  in U brown oxides (97 to 98%  $UO_2$  and 2 to 3%  $U_3O_8$ ); the standardization of ceric sulfate; the preparation of ceric sulfate solution; the analysis of U oxides; the determination of C and H in U metal by burning the sample in an atmosphere of  $O_2$ ; and the colorimetric determination of N in  $Mg$ . (C.H.)

### 3420 A-2157

Columbia Univ., New York. Div. of War Research.

ANALYSIS OF CONSTITUENTS AND IMPURITIES IN  $BCl_3$ . Charles M. Judson. Nov. 30, 1944. Decl. Dec. 7, 1955. 7p. Contract W-7405-eng-50. (100B-R-243). \$1.80(ph OTS); \$1.80(mf OTS).

Methods are described for the determination of  $SiCl_4$ ,  $BF_3$ ,  $Cl_2$ , and S in  $BCl_3$ . (C.H.)

### 3421 A-2158

Columbia Univ., New York. Div. of War Research.

COMPLETE ANALYSIS OF B SAMPLES. Charles M. Judson. Nov. 30, 1944. Decl. Dec. 8, 1955. 13p. Contract W-7405-eng-50. (100B-R-244). \$3.30(ph OTS); \$2.40(mf OTS).

Methods are described for the chemical analysis of elemental B. Methods for the determination of  $H_2O$  adsorbed on B, and the determination of Si, Fe, Ta, W, Mo, and other impurities in elemental B are described. (C.H.)

### 3422 A-2940

National Bureau of Standards, Washington, D. C.

THE DETERMINATION OF TRACES OF URANIUM IN LEAF ASH AND SOIL. G. W. Imirie, Jr. Nov. 1946. Decl. Dec. 13, 1955. 10p. \$1.80(ph OTS); \$1.80(mf OTS).

A fluorimetric method is presented for the determination of trace uranium in leaf ash and soil. (C.W.H.)



**3423 A-3502**

Du Pont de Nemours (E. I.) and Co. Jackson Lab., [Wilmington, Del.]

THE RECOVERY OF URANIUM FROM MALLINCKRODT CHEMICAL "306 [RESIDUES]." Problem Report [for] Period August 24, 1944–October 25, 1944. F. B. Stilmar. Dec. 10, 1945. Decl. Dec. 8, 1955. 6p. Contract W-7412-eng-151. (JWD-64) \$1.80(ph OTS); \$1.80(mf OTS).

A laboratory procedure is described for the recovery of U from Mallinckrodt Chemical 306, which analyzes 55% U and 1.6% P. (C.H.)

**3424 A-4018**

Kellex Corp., New York.

THE DETERMINATION OF URANYL ION BY DIRECT TITRATION WITH CHROMOUS SULFATE. Robert H. Lafferty, Jr., and Rasha Winget, Jr. Apr. 1, 1946. Decl. Dec. 8, 1955. 6p. (Research Paper No. D23). \$1.80(ph OTS); \$1.80(mf OTS).

A procedure is described for the direct potentiometric titration of uranyl ion with chromous sulfate. The method is said to determine between 100 and 500 mg of U with an accuracy of 0.3% and a precision of 0.6%. There is no interference from fluoride ion using this method. (C.H.)

**3425 AECD-3850**

Massachusetts Inst. of Tech., Cambridge, Metallurgical Project.

SPECTROPHOTOMETRIC DETERMINATION OF SILICON IN ZIRCONIUM. E. B. Read and J. P. Martin. Feb. 28, 1951. Decl. Dec. 6, 1955. 4p. Contract [W-7405-eng-53]. (MIT-EBR-8). \$1.80(ph OTS); \$1.80(mf OTS).

The spectrophotometric determination of Si in Zr is based on the solubility of  $\text{SiCl}_4$  in very dilute  $\text{HNO}_3$  solution, and the complexing of the fluorides with boric acid. The optical density of the Si complex is measured at 710 m $\mu$ . (C.W.H.)

**3426 AECD-3991**

Mallinckrodt Chemical Works, St. Louis.

THE DETERMINATION OF COPPER IN URANIUM MATERIAL. J. Reed McCoy. Mar. 7, 1946. Decl. with deletions Dec. 7, 1955. 8p. \$1.80(ph OTS); \$1.80(mf OTS).

A procedure is described which uses dithizone for the colorimetric determination of Cu in  $\text{UF}_4$ . The method covers all phases of interference which are present in U materials. Results of analyses are tabulated. (C.H.)

**3427 CC-2403**

[Ames Lab., Ames, Iowa.]

ANALYSIS FOR OXIDE IN THORIUM METAL. Problem Assignment No. 7. A. S. Ayers. May 12, 1945. Decl. Dec. 13, 1955. 4p. Contract W-7405-eng-82. \$1.80(ph OTS); \$1.80(mf OTS).

To estimate the oxygen picked up by Th in casting, a rapid method of running the acid insoluble content of the metal was developed. The quickest procedure consists of reacting with mixed acids, fuming with perchloric, and filtration to separate the "free" thorium from the "combined." The precipitate is ignited and weighed as  $\text{ThO}_2$ . (auth)

**3428 CC-2670**

Chicago. Univ. Metallurgical Lab.

PRELIMINARY REPORT ON A COLORIMETRIC METHOD FOR THE DETERMINATION OF MICROGRAM QUANTITIES OF THORIUM. Problem Assignment 252 MLC 4407. W. Byerly, L. Niedrach, W. Davin, and H. Dyas.

EXPERIMENTS IN THE DISSOLUTION OF  $\text{O}_2$  METAL [ $\text{UO}_2$ ]. Problem Assignment 251 MLC 4301. R. W. Bane. Jan. 1, 1945. Decl. Dec. 16, 1955. 11p. Contract W-7401-eng-37. \$3.30(ph OTS); \$2.40(mf OTS).

Thorium can be precipitated as a salt of p-dimethyl-aminoazophenylarsonic acid at a pH of about 1.5. The precipitate, collected on a sintered glass filter, is washed with dilute ammonium hydroxide to dissolve the dye. The amount of Th is determined by measuring the concentration of the dye spectrophotometrically at a wavelength of 450 millimicrons. Zirconium, which interferes, can be separated and determined using the same reagent in strong hydrochloric. The behavior of Th metal upon treatment with various acids and upon fusion with  $\text{KHSO}_4$  is described. Three satisfactory procedures are given for dissolving the metal with sulfuric acid, phosphoric acid, and by a potassium hydrogen sulfate fusion. A study was made of methods for the dissolutions of  $\text{UO}_2$ . Results are summarized. (C.H.)

**3429 CC-2933**

[Ames Lab., Ames, Iowa.]

ANALYSIS OF IRON IN THORIUM, BERYLLIUM, AND CERIUM. Problem Assignment No. 117. R. P. Ericson and E. J. Fornefeld. Sept. 10, 1945. Decl. Dec. 16, 1955. 10p. Contract W-7405-eng-82. \$1.80(ph OTS); \$1.80(mf OTS).

Procedures are summarized for the colorimetric determination of Fe in Ce, Th, and Be metals and their compounds. (C.H.)

**3430 CC-2994**

[Chicago. Univ. Metallurgical Lab.]

ANALYSIS OF HEAVY WATER BY EQUILIBRATION. R. B. Fischer, R. A. Potter, and R. J. Voskuyl. May 15, 1945. Decl. Dec. 15, 1955. 24p. Contract W-7401-eng-37. \$4.80 (ph OTS); \$2.70(mf OTS).

The deuterium concentration of heavy water can be determined by equilibrating the water with deuterium gas in the presence of a catalyst with subsequent analysis of the equilibrated gas on the mass spectrometer. The apparatus, procedures, water sampling methods, the deuterium gas, catalyst, peptizing agent, and reaction conditions are described. The range, precision, and accuracy of the method are discussed. An equation for calculating results and a graph for routine calculation of results are appended. (C.H.)

**3431 CC-3241**

[Ames Lab., Ames, Iowa.]

THE RAPID DETERMINATION OF NITRIC ACID AND THORIUM IN THORIUM NITRATE SOLUTIONS. A. S. Newton, J. Powell, and P. Figard. Nov. 27, 1945. Decl. Dec. 14, 1955. 14p. Contract W-7405-eng-82. \$3.30(ph OTS); \$2.40(mf OTS).

Two physico-chemical methods of determining nitric acid and thorium nitrate in solutions containing these two materials were investigated. Conductimetric titration with sodium hydroxide can be used to determine nitric acid accurately. The titration of thorium nitrate requires a separate standardization of the base however, since a basic salt is precipitated rather than the normal hydroxide. The titration of thorium is reproducible however, so an empirical standardization can be used. The measurement of the specific gravity and refractivity of the solutions provides a method of determining the concentrations in



terms of these two variables. Equations for the concentrations in terms of specific gravity and refractivity are given, both in pure solutions and in those saturated with methyl isobutyl ketone. (auth)

**3432** CC-3638

Argonne National Lab., Lemont, Ill.

A STUDY OF THORIUM PEROXIDE SULFATE. J. W. Hamaker and C. W. Kock. Oct. 1, 1945. Decl. Dec. 15, 1955. 16p. Contract W-31-109-eng-38. \$3.30(ph OTS); \$2.40(mf OTS).

Thorium peroxide was precipitated from thorium nitrate solutions containing varying amounts of sulfate ion and of hydrogen ion. The washed solids were analyzed both wet and dry. Analyses were made for Th, peroxide oxygen, sulfate, nitrate, and water contents. X-ray powder photographs of the dried samples showed the presence of only two phases. When precipitated from high sulfuric acid, the solid phase was isomorphous with  $\text{ThOOSO}_4 \cdot 3\text{H}_2\text{O}$ . More weakly acid solutions whose sulfate content was varied over wide limits yielded a solid isomorphous with Th peroxide nitrate and containing 3.0 to 3.8 peroxide O atoms for each Th atom. The sulfate content of this latter phase varied continuously between the limits  $\text{SO}_4^-/\text{Th(IV)}^-$  0.34 to 0.01 with nitrate ion present when the sulfate content was very low. This continuous variation in composition is in agreement with the previously proposed structure of this phase. (auth)

**3433** CF-48-10-219

[Oak Ridge National Lab., Tenn.]

SPECIAL RADIOISOTOPE METHODS. SECTION II. S. A. Reynolds. Sept. 20, 1948. Decl. Dec. 7, 1955. 13p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

Methods for the determination of Ba, Sr, Ce, Cs, Nb, the lanthanum group, Y, Pu, Am, Cm, the rare earths, and Zr are outlined. (B.J.H.)

**3434** CN-2041

[Clinton Labs., Oak Ridge, Tenn.]

DEVELOPMENT OF RADIOCHEMICAL ANALYTICAL PROCEDURES FOR PLUTONIUM—(2) RECOMMENDATIONS FOR A STANDARD PROCEDURE AND TESTS IN URANYL SOLUTIONS. Progress Report. D. E. Koshland, Jr., comp. Jan. 8, 1945. Decl. Dec. 13, 1955. 39p. Contract W-7405-eng-39. \$6.30(ph OTS); \$3.00(mf OTS).

The development of procedures for the analysis of the total Pu in solution and the % Pu(VI) in solution is described. The variables affecting the choice of the procedures, the reproducibility of the procedures, and the finally recommended procedures are discussed in detail. (auth)

**3435** DP-74

Du Pont de Nemours (E. I.) & Co. Savannah River Lab., Augusta, Ga.

DETERMINATION OF ORGANIC MATERIAL IN AQUEOUS SOLUTIONS. E. R. Russell. Aug. 1954. Decl. Dec. 22, 1955. 17p. Contract AT(07-2)-1. \$3.30(ph OTS); \$2.40(mf OTS).

A method was developed for determining the concentration of trace quantities of organic material in aqueous solutions. The organic material is oxidized in solution, followed by gasometric measurement of the carbon dioxide. The technique may be applied to radioactive solutions, and as little as 0.3 of a micromole of carbon can be determined. (auth)

**3436** DP-75

Du Pont de Nemours (E. I.) & Co. Savannah River Lab., Augusta, Ga.

DIELECTRIC DETERMINATION OF TRIBUTYL PHOSPHATE IN KEROSENE. H. M. Hubbard. Aug. 1954. Decl. Dec. 22, 1955. 19p. Contract AT(07-2)-1. \$3.30(ph OTS); \$2.40(mf OTS).

The Sargent Model V Chemical Oscillometer was applied to the dielectric constant determination of tri-n-butyl phosphate (TBP) in mixtures of TBP and kerosene over the range of 0 to 10% TBP. Under the most favorable conditions, the precision approached 0.02% absolute. (auth)

**3437** HW-13300

Hanford Works, Richland, Wash.

THE COULOMETRIC TITRATION OF 8-HYDROXYQUINOLINE. William N. Carson, Jr. June 16, 1949. Decl. Dec. 6, 1955. 16p. Contract [W-31-109-Eng-52]. \$3.30(ph OTS); \$2.40(mf OTS).

A method of determining 8-hydroxyquinoline by titration with electrolytically generated  $\text{Br}_2$  has been developed. Results show good precision in the range 0.4 to 1.6 mg total 8-hydroxyquinoline, with 99% confidence limits of less than  $\pm 2\%$ . An electronically-regulated constant current source, required by the method, is described. A new indicator system with high sensitivity to free  $\text{Br}_2$  is discussed. (auth)

**3438** HW-15846

Hanford Works, Richland, Wash.

A COMPARISON OF TWO METHODS FOR THE SPECTROCHEMICAL ANALYSIS OF PLUTONIUM. H. H. Van Tuyl. Feb. 1, 1950. Decl. Dec. 19, 1955. 13p. Contract W-31-109-eng-52. \$3.30(ph OTS); \$2.40(mf OTS).

Spectrochemical analyses of plutonium by the carrier concentration and cupferron extraction-copper spark methods show diversities as high as a factor of fifty. Analysis by the direct copper spark method, analysis of thorium standards, and theoretical considerations all indicate that the carrier concentration method is more accurate than the cupferron method for all elements studied. (auth)

**3439** HW-17175

Hanford Works, Richland, Wash.

THE DETERMINATION OF TRIBUTYL PHOSPHATE IN DEODORIZED SHELL BASE WITH THE INFRARED SPECTROMETER. R. H. Moore. Mar. 10, 1950. Decl. Dec. 22, 1955. 12p. Contract W-31-109-eng-52. \$1.80(ph OTS); \$1.80(mf OTS).

A preliminary investigation of an infrared spectrometer method for the determination of TBP in deodorized Shell base is reported. It was observed that small and variable amounts of water,  $\text{HNO}_3$ , and U have no adverse effect on the results. (J.E.D.)

**3440** HW 18320

Hanford Works, Richland, Wash.

FISSION PRODUCT ANALYSIS OF URINE. R. C. Thorburn. May 31, 1950. Decl. Dec. 21, 1955. 19p. Contract W-31-109-eng-52. \$3.30(ph OTS); \$2.40(mf OTS).

Detailed steps are outlined for the analysis of  $\text{Sr}^{89}$ ,  $\text{Sr}^{89}-\text{Y}^{90}$ ,  $\text{Ru}^{106}-\text{Rh}^{106}$ ,  $\text{Cs}^{137}$ , and  $\text{Ce}^{144}-\text{Pr}^{144}$  in urine by an ion exchange process. (K.S.)

**3441** HW-30898

Hanford Atomic Products Operation, Richland, Wash.

THE FLAME PHOTOMETRIC DETERMINATION OF



**CADMIUM IN CADMIUM-LEAD ALLOYS.** D. W. Brite. Feb. 19, 1954. Decl. Dec. 7, 1955. 11p. Contract W-31-109-eng-52. \$1.80(ph OTS); \$1.80(mf OTS).

A flame-photometric method was developed for a rapid and accurate determination of Cd in Pb-Cd alloys, using a Bechman Model DU Spectrophotometer. The method is applicable throughout the entire range of 0 to 100% Cd, with a lower limit of detection of 0.05% Cd. Relative precision varies from  $\pm 1.1\%$  at 75% Cd level to  $\pm 2.5\%$  at the 2% level. The time required for making a determination is about 20 min after an instrument calibration has been made. (K.S.)

**3442 K-81**

Carbide and Carbon Chemicals Corp. [K-25 Plant], Oak Ridge, Tenn.

**AN IMPROVED APPARATUS FOR THE DETERMINATION OF OXYGEN IN NITROGEN BY THE DEW POINT METHOD.** W. W. Harwood, T. Kwasnoski, and J. C. Barton. Nov. 20, 1947. Decl. Dec. 5, 1955. 10p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

Certain alterations and improvements in the gas-cooling system have been made on the apparatus designed for the determination of  $O_2$  in tank  $N_2$ . The sensitivity was improved in the concentration range of 0 to 100 ppm of  $O_2$ . (C.W.H.)

**3443 K-513**

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

**CHEMICAL DECOMPOSITION OF SOLUTIONS OF AMMONIUM NITRATE.** S. S. Kirsilis, T. S. McMillan, J. C. Posey, and H. A. Bernhardt. Oct. 10, 1949. Decl. Dec. 27, 1955. 36p. Contract [W-7405-eng-26]. (KLO-148). \$6.30(ph OTS); \$3.00(mf OTS).

Studies were made of a number of chemical methods for the safe decomposition of ammonium nitrate in filtrates from the uranyl ammonium phosphate precipitation from Hanford waste solutions. Among the more successful methods tested were the boiling out of ammonia after addition of alkali; decomposition of ammonia to nitrogen by means of sodium nitrite; reduction of nitrate by oxalic acid; reduction of nitrate by a mixture of sucrose and formic acid, and the decomposition of ammonium nitrate by hydrochloric acid in the presence of silica gel. The alkali method is simplest and presents the least corrosion difficulties. The organic reduction and the silica gel methods require the use of strongly acid solutions, with attendant corrosion problems, but result in an evaporated solid residue only half as great as that from the alkali method. Several other methods were investigated but were found to possess greater practical disadvantages than the methods described above. (auth)

**3444 KAPL-210**

Knolls Atomic Power Lab., Schenectady, N. Y.

**THE DETERMINATION OF MOLYBDENUM IN URANIUM-MOLYBDENUM ALLOYS: A COLORIMETRIC METHOD.** Eve Mosher and Richard H. Gale. July 7, 1949. Decl. Dec. 5, 1955. 9p. Contract W-31-109-Eng-52. \$1.80(ph OTS); \$1.80(mf OTS).

A modified thiocyanate method has been developed for the determination of Mo in Mo-U alloys. Cupferron is used to separate the U and Mo prior to the absorbance measurements. Interfering ions include  $V^{5+}$ ,  $Al^{3+}$ , and  $Fe^{3+}$ . (C.W.H.)

**3445 MCW-134**

Mallinckrodt Chemical Works, St. Louis.

**A COMPARISON OF RESULTS OF ORE ASSAYS BY MALLINCKRODT AND NATIONAL BUREAU OF STANDARDS PROCEDURES.** J. R. Simmler and S. H. Huston. Sept. 1948. Decl. Dec. 2, 1955. 10p. \$3.30(ph OTS); \$2.40(mf OTS).

A complete comparison of results of the ore assay methods conducted by MCW and the National Bureau of Standards as well as original assay results are tabulated. Contrary to previous observations, the results of the MCW method were consistently higher: fair agreement between operators using both methods was noted. The investigational assays did not generally agree well by either method with the original values. The average deviation by both methods was about 0.65%. (J.E.D.)

**3446 NYO-5087**

Mallinckrodt Chemical Works, St. Louis.

**THE DETERMINATION OF CALCIUM IN IMPURE X [U] LIQUORS.** G. L. Martin. Mar. 3, 1945. Decl. Dec. 2, 1955. 3p. \$1.80(ph OTS); \$1.80(mf OTS).

In connection with the development of the continuous extraction process, it was necessary to determine Ca in various liquors involved in the process. In addition to U, these liquors contained phosphate, Fe, and rare earths in varying amounts. The standard volumetric procedure in which  $KMnO_4$  is used to titrate Ca oxalate was chosen. Several methods of separating the Ca from the interfering ions were investigated. The method evolved consisted of precipitating the Ca by adding  $NH_4OH$  to a hot acid solution containing both the Ca and the oxalate. The detailed analytical procedure is given. (L.M.T.)

**3447 NYO-5130**

Mallinckrodt Chemical Works, St. Louis.

**DETERMINATION OF BARIUM IN AAA [PITCHBLENDE] GANGUE.** J. R. McCoy and G. L. Martin. July 11, 1945. Decl. Dec. 7, 1955. 9p. \$1.80(ph OTS); \$1.80(mf OTS).

A method is developed for determining Ba in a sulfate cake composed of large amounts of  $PbSO_4$ ,  $CaSO_4$ , and silicon. Ba is determined gravimetrically by means of a  $BaCrO_4$  precipitation following a suitable removal of all the interfering elements. As a result of the interference of trace amounts of Pb, the accuracy of this determination can hardly exceed 5%. (K.S.)

**3448 NYO-5134**

Mallinckrodt Chemical Works, St. Louis.

**THE RADIUM-URANIUM RATIO IN AAA [PITCHBLENDE] ORE.** G. L. Martin. July 1945. Decl. Dec. 7, 1955. 5p. Contract [W-14-108-eng-8]. \$1.80(ph OTS); \$1.80(mf OTS).

An attempt was made to establish the best value for the theoretical ratio of Ra to U in pitchblende ore and a review is made of the accuracy of the method. Results indicate that the theoretical value for the Ra to U ratio is uncertain within rather wide limits. The best available value seems to be  $3.68 \times 10^{-7}$ . The average value obtained on 43 pitchblende ore samples submitted to the laboratory is  $3.85 \pm 0.18 \times 10^{-7}$ . Comparison of results obtained on check samples and standard samples indicate that the results are as accurate as can be expected, considering the inherent inaccuracies of the method. Before the ratio in ore can be fixed at any figure, it will be necessary to analyze samples representing larger quantities of ore than those that were



run. Without knowing something of the history of the material, it is impossible to decide if the theoretical ratio can be applied to this material. (J.E.D.)

**3449 NYO-5208**

Mallinckrodt Chemical Works, St. Louis.

DETERMINATION OF URANIUM IN [BY-PRODUCT] BARIUM CAKE [SULFATE CAKE]. J. Boyd. Sept. 26, 1947. Decl. Dec. 2, 1955. 12p. \$3.30(ph OTS); \$2.40 (mf OTS).

The short acid digestion method (Black Book method) for determining U in by-product Ba cake does not give accurate results owing to the presence of interfering elements which are not removed by  $\text{HNO}_3$  treatment. A revised technique, using aqua regia, is found to yield more accurate data. (K.S.)

**3450 NYO-5210**

Mallinckrodt Chemical Works, St. Louis.

THE RADIUM—URANIUM RATIO IN AAA [PITCH-BLENDE] ORE. III. F. A. Morecombe. Oct. 27, 1947. Decl. Dec. 2, 1955. 4p. \$1.80(ph OTS); \$1.80(mf OTS).

No significant changes are made in the results reported in NYO-5134. (K.S.)

**3451 NYO-5213**

Mallinckrodt Chemical Works, St. Louis.

A STUDY OF ANALYTICAL METHODS FOR THE DETERMINATION OF URANIUM IN CHEMICAL 6 RP [ORE REFINERY RAFFINATE CAKE]. Gerald C. Reid. Dec. 18, 1947. Decl. Dec. 2, 1955. 13p. \$3.30(ph OTS); \$2.40(mf OTS).

An improved ether extraction procedure is given for the analysis of ore refinery raffinate cake, a hydroxide precipitate from the ether extraction, containing much  $\text{Ca}_2(\text{NO}_3)_2$ . The actual U content is determined to a degree of accuracy sufficient for material balance purposes. (K.S.)

**3452 NYO-5214**

Mallinckrodt Chemical Works, St. Louis.

THE DETERMINATION OF URANIUM IN PLANT [ORE REFINERY] SEWER WATER. O. J. Buckheim. Jan. 8, 1948. Decl. Dec. 2, 1955. 4p. \$1.80(ph OTS); \$1.80(mf OTS).

A number of methods for U determination were tested, and satisfactory results were obtained by precipitating a minute quantity as a phosphate, using a coprecipitant. (K.S.)

**3453 NYO-5217**

Mallinckrodt Chemical Works, St. Louis.

DETERMINATION OF TRIVALENT URANIUM IN (URANIUM) DIOXIDE AND THE PREPARATION AND SOME PROPERTIES OF TRIVALENT URANIUM SOLUTIONS. J. R. Simmler. Jan. 21, 1948. Decl. Dec. 2, 1955. 10p. \$3.30(ph OTS); \$2.40(mf OTS).

Uranium dioxide dissolved in phosphoric acid under an atmosphere of carbon dioxide, and diluted with 25% sulfuric acid, did not have an initial high positive potential as compared to the high positive potential of samples of the same composition containing trivalent U. The trivalent U solutions can be prepared by reducing a solution of approximately 1%  $\text{UO}_2\text{Cl}_2$  with zinc amalgam. The solutions of  $\text{UO}_2\text{Cl}_2$  were reduced in 2.5%, 22.5% HCl and 22.5%  $\text{H}_2\text{SO}_4$  concentrations. The U in the HCl solutions was almost completely reduced to the trivalent state. The U in the  $\text{H}_2\text{SO}_4$  solution was not as completely reduced. Trivalent

U was titrated potentiometrically with ceric sulfate in different acid concentrations. The formation of hydrogen on the platinum indicator electrode had a disturbing effect on the potential readings. This effect was particularly true at the beginning of the titration and became less disturbing as the amount of trivalent U became less. The approximate reduction potential of trivalent U, using the normal oxidation potential of ceric/cerous couple as -1.61 volts, is +0.72 volts. (K.S.)

**3454 NYO-5218**

Mallinckrodt Chemical Works, St. Louis.

AN INVESTIGATION OF THE DETERMINATION OF HEXAVALENT URANIUM IN BROWN OXIDE [ $\text{UO}_2$ ]. J. R. Simmler. Jan. 28, 1948. Decl. Dec. 2, 1955. 28p. \$4.80(ph OTS); \$2.70(mf OTS).

**3455 NYO-5219**

Mallinckrodt Chemical Works, St. Louis.

THE DETERMINATION OF URANIUM IN K-65 (GANGUE LEAD CAKE). John W. Stevenson. Jan. 1948. Decl. Dec. 2, 1955. 10p. \$1.80(ph OTS); \$1.80(mf OTS).

The determination of 1 to 3% U in the presence of 1 to 3% Mo, V, Ba, Mg, Na, Sr, Ni, Ca, Co, Fe, and Zr, and much larger amounts of Pb, Si, Al, and sulfate ion was investigated. The two major problems are the extraction of U from the sample, and the isolation of the extracted U. Various analytical methods were applied, and the results indicated that the method in use is subject to both positive and negative errors. Positive errors may run as high as 15%. A recommended method is given which is believed to be free from these errors; however, a radical change in sample composition would warrant further investigation. The principal features of this method are multiple  $\text{HNO}_3$  extractions from the sample and multiple ether extractions of the filtrates from the acid extractions. The final determination is made by a colorimetric  $\text{Na}_2\text{CO}_3\text{—H}_2\text{O}_2$  method. (K.S.)

**3456 NYO-5229**

[Mallinckrodt Chemical Works, St. Louis].

A CHEMICAL AND SPECTROSCOPIC COMPARISON OF THE COPPER CONTENT IN CHEMICAL TA-7 [ $\text{UF}_4$ ]. Joseph R. Simmler and Byron D. Field. May 1948. Decl. Dec. 2, 1955. 2p. \$1.80(ph OTS); \$1.80(mf OTS).

A series of  $\text{UF}_4$  samples were prepared to which a known amount of Cu had been added giving a Cu range from 3 to 20 ppm. Chemical and spectrographic analysis of the  $\text{UF}_4$  samples were compared and any difference, especially in the Cu content, was noted. The two methods were in fair agreement. (K.S.)

**3457 NYO-5230**

Mallinckrodt Chemical Works, St. Louis.

SOLUTION PROCEDURE OF PITCHBLENDE AS USED BY THE NATIONAL BUREAU OF STANDARDS. Joseph R. Simmler. May 1948. Decl. Dec. 7, 1955. 3p. \$1.80 (ph OTS); \$1.80(mf OTS).

Steps are outlined for dissolving small samples of pitchblende into solution, and analyzing for U content by a fusion procedure. Results indicate that complete dissolution of the U ore is obtained by this procedure. (K.S.)

**3458 NYO-5236**

Mallinckrodt Chemical Works, St. Louis.

THE SPECIFIC GRAVITY OF DILUTE SOLUTIONS OF URANIUM IN ETHER. Gerhard P. Lang. Nov. 6, 1950. Decl. Dec. 2, 1955. 5p. \$1.80(ph OTS); \$1.80(mf OTS).



The specific gravity of dilute solution of  $\text{UO}_2(\text{NO}_3)_2$  in ether was used for the determination of U in the ether from column A-3. The specific gravity measurements are tabulated. (J.E.D.)

**3459** Y-390

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

COLORIMETRIC DETERMINATION OF URANIUM AND VANADIUM WITH BENZOHYDROXAMIC ACID. L. G. Overholser and W. R. Grimes. April 20, 1949. Decl. Dec. 6, 1955. 55p. Contract W-7405-eng-26. \$9.30 (ph OTS); \$3.60(mf OTS).

The reaction of benzohydroxamine acid with uranyl ions was investigated and the reaction was applied to the colorimetric determination of U. Various factors such as effect of pH, reagent and buffer concentration, temperature, and the effect of diverse ions were studied. Comparable work, on the reaction of benzohydroxamic acid with vanadate ions, was performed and a colorimetric method was developed for V. The colorimetric methods were applied to U and V in mixtures containing also Fe, Al, Cu, Ni, Co, Cr, and Mn. Results of such determinations, following separations by the Hg cathode, penta-ether, phosphate, and cupferron methods, are given. Results of similar determinations in carnotite ores are also presented. (auth)

**3460** Y-407

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

THE FLUORESOMETER. Stanton B. Smith and Hugh G. Neil. Jan. 29, 1946. Decl. Dec. 7, 1955. 25p. Contract W-7405-eng-26. \$4.80(ph OTS); \$2.70(mf OTS).

The fluoreometer Model 2B has been in daily use for determining U in urine samples for a period of six months and has given very satisfactory performance. The sample is fused in a cake of sodium fluoride 0.75 in. in diameter and 1 mm thick (300 milligrams). This cake is activated with ultraviolet light from an S-4 sunlamp and the fluorescence measured by means of a phototube and sensitive DC amplifier. The range of the instrument is 6 micrograms to 0.001 micrograms, results being reproducible from the same sample to within 1% at the high end and to within 10% at the low end of the range. The zero stability is better than one-half of one percent. (auth)

**3461** Y-602

Carbide and Carbon Chemicals Co. Y-12 Plant, Oak Ridge, Tenn.

CHEMICAL DETERMINATION OF PHTHALATE ION. L. G. Overholser and W. R. Grimes. Apr. 17, 1950. Decl. Dec. 8, 1955. 26p. Contract W-7405-eng-26. \$4.80(ph OTS); \$2.70(mf OTS).

A method for determination of phthalate ion in aqueous solution by precipitation at pH 3.3 of a lead phthalate compound of constant composition has been developed. Subsequent drying of the precipitate at 105°C and weighing of the material permits estimation of phthalate present to  $\pm 1\%$ . Chloride and thiocyanate ions, if present to the extent of more than 5 millimoles per sample, should be removed by precipitation with Ag. The material is not, in spite of previously reported data, the normal Pb phthalate but its composition is sufficiently reproducible to justify its use in analysis. The presence of 1 mole of acetate ion per 2 moles of phthalate ion in the dried precipitate has been demonstrated. The weight of precipitate obtained

from a known quantity of phthalate and the Pb content of the dried material justify the conclusion that the compound precipitated is  $\text{Pb}(\text{C}_2\text{H}_3\text{O}_2)_2 \cdot 4\text{PbC}_8\text{H}_4\text{O}_4$ . (auth)

Refer also to abstracts 3515, 3535, and 3567.

## DEUTERIUM AND DEUTERIUM COMPOUNDS

**3462** A-754

Columbia Univ., New York. Div. of War Research. EXCHANGE OF DEUTERIUM BETWEEN MERCAPTANS AND WATER. Clyde Hutchison and Daniel Gillies. July 9, 1943. Decl. Dec. 8, 1955. 40p. Contract W-7405-eng-50. (2R-238). \$6.30(ph OTS); \$3.00(mf OTS).

Isopropyl mercaptan was investigated as a possible substance for use in the extraction of deuterium from water by the dual temperature process. Data are presented from studies on the equilibrium separation coefficients for the exchange of D between water and mercaptans at various temperatures; the rates of exchange of D between mercaptans and water; the settling rates of water-mercaptan emulsions; the solubility of isopropyl mercaptan in water and the solubility of water in isopropyl mercaptan; the corrosive action of mercaptans on steel; and the hydrolysis of alkaline solutions of isopropyl mercaptan. (C.H.)

**3463** A-3954

National Bureau of Standards, Washington, D. C. VISCOSITY OF DEUTERIUM OXIDE FROM 5° TO 95°C. R. C. Hardy and R. L. Cottingham. [194?]. Decl. Dec. 8, 1955. 6p. \$1.80(ph OTS); \$1.80(mf OTS).

Data are presented on the absolute viscosity of deuterium oxide of 99.56 mol % purity over the range 5 to 95°C, and on the absolute viscosity of pure deuterium oxide and distilled water over the same temperature range. A table is given showing values for the ratios of the viscosity of pure deuterium oxide, deuterium oxide of 99.56 mol % purity, and water, at various temperatures to the viscosity of water at 20°C. The table also contains values for the ratio of the viscosity of pure deuterium oxide and deuterium oxide of 99.56 mol % purity at various temperatures to the viscosity of water at the same temperature. (auth)

**3464** K-843

Carbide and Carbon Chemicals Co. K-25 Plant, Oak Ridge, Tenn.

EVALUATION OF HEAVY WATER PRODUCTION AT GASEOUS DIFFUSION PLANT SITES. S. Blumkin, R. W. Dehoney, and J. Shacter. Nov. 26, 1951. Decl. Dec. 27, 1955. 16p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

The production of heavy water by distillation, utilizing heat available from other process sources—specifically at a gaseous diffusion site—is discussed. The high temperature-high pressure process, because of the low relative volatility, requires a very large and costly cascade of distillation columns. The low temperature-low pressure process, involving larger relative volatility, appears to be more economical. On a quick design basis, neither process can furnish heavy water at unit costs which compete with those predicted for other methods of separation. (auth)

Refer also to abstract 3735.



## FLUORINE AND FLUORINE COMPOUNDS

**3465** A-740

Du Pont de Nemours (E. I.) &amp; Co. Jackson Lab., Wilmington, Del.

PRODUCTION OF FLUORINATED LUBE OIL. Problem Report. R. G. Benner. May 7, 1943. Decl. Dec. 7, 1955 34p. (100XR-1353) \$6.30(ph OTS); \$3.00(mf OTS).

One hundred and fifteen pounds of distilled fluorinated lube oil with a boiling range of 147 to 208°C/10 mm was prepared by the vapor phase fluorination method. In addition enough crude oil was made to produce 12 gal or 204 lb more of this material. Procedures are described and properties of the cuts are tabulated. (C.H.)

**3466** A-2553

Du Pont de Nemours (E. I.) and Co. Jackson Lab., [Wilmington, Del.]

THE CONTROL OF THE HF CONCENTRATION OF ELECTROLYTE BY ELECTRICAL CONDUCTANCE MEASUREMENTS. Problem Report [for] Period February 23, 1944 to November 27, 1944. S. G. Turnbull, Jr. Jan. 11, 1945. Decl. Dec. 13, 1955. 40p. Contract W-7412-eng-151. (JWD-40) \$6.30(ph OTS); \$3.00 (mf OTS).

The control of the HF concentration of electrolyte in fluorine production units is compared with other methods of HF control. Absolute values for the specific conductance of electrolyte are given, and their dependence upon the HF content and the temperature are discussed. The design of conductance cells for controlling the HF content of electrolyte is discussed from theoretical and constructional viewpoints. The effects of errors that occur in the conductance method are described, and methods for reduction of these to negligible quantities are prescribed. Among these may be mentioned the errors resulting from the contact resistance of electrodes, frequency effects, and errors due to dissolved iron or water. The results of control runs using this method of measurement are described for conductance cells of various design. (auth)

**3467** M-4556

Du Pont de Nemours (E. I.) & Co., Wilmington, Del. FINAL REPORT ON BPX-6. LOW TEMPERATURE CONDENSATION OF HF FROM FLUORINE. W. J. Cordes. Sept. 21, 1945. Decl. Dec. 6, 1955. 39p. \$7.80(ph OTS); \$3.30(mf OTS).

Fluorine produced in the nickel-anode electrolytic cells contains about 25% HF as an impurity which caused process difficulties. In an effort to reduce process difficulties HF has been experimentally condensed in a shell-and-tube condenser using a dry ice-trichlorethylene mixture as coolant. It was demonstrated that the HF concentration in the fluorine could be reduced to about 5%. Heat transfer coefficients and other design data were obtained. (auth)

**3468** M-4558

Du Pont de Nemours (E. I.) &amp; Co. Engineering Dept., Wilmington, Del.

MEASUREMENT OF FLUORINE CELL BUILDING PRODUCTION AND EFFICIENCY; REMOVAL AND RECOVERY OF HF FROM HYDROGEN. Final Report on BPX-2. W. O. Jewett and J. D. Ensign. June 27, 1944. Decl. Dec. 5, 1955. 57p. (CWC-ED-1). \$9.30(ph OTS); \$3.60(mf OTS).

Methods were determined for purifying and metering the by-product hydrogen manufactured in electrolytic

fluorine cells. The metered hydrogen was used as a current efficiency measurement of the cells and was recovered for use in hydrogenation processes. Hydrofluoric acid present in the hydrogen as it came from the cells was removed by scrubbing the hydrogen with water and caustic or by adsorption on activated carbon. The latter method allowed it to be re-used in the cell operation. (auth)

Refer also to abstract 3414.

## GRAPHITE

**3469** BNL-69

Brookhaven National Lab., Upton, N. Y. THERMAL CONDUCTIVITY OF GRAPHITE. R. C. Garth and V. L. Sailor. Nov. 28, 1949. Decl. Jan. 6, 1956. 19p. Contract [AT-30-2-gen-16]. \$3.30(ph OTS); \$2.40(mf OTS).

The coefficient of thermal conductivity of several samples of graphite used in BNL reactors has been measured. The conductivity in the direction parallel to the axis of extrusion was higher than in transverse directions. The effect of mechanical mistreatment was to decrease the conductivity. The heat transfer coefficient for machined surfaces of graphite was also measured. (auth)

**3470** CC-3161

Carnegie Inst. of Tech., Pittsburgh.

THE EFFECT OF NEUTRON BOMBARDMENT ON THE SPECIFIC HEAT OF GRAPHITE AT LOW TEMPERATURES. Report for Period Aug. 1, 1944, to June 30, 1945. ("A" Report No. 13). I. Estermann and G. I. Kirkland. Sept. 5, 1945. Decl. Dec. 15, 1955. 31p. Contract W-7405-eng-277. \$6.30(ph OTS); \$3.00(mf OTS).

Results are reported from a preliminary study of the effect of neutron bombardment on the specific heat of graphite at low temperatures. Theoretical considerations are reviewed. Results are reported from a series of measurements of the effects of bombardment or annealing on the specific heat at various temperatures. It was found that a strongly bombarded specimen had a higher specific heat than a virgin one, and that annealing at 500°C reduced the specific heat of the bombarded piece. (C.H.)

**3471** CE-364

Chicago. Univ. Metallurgical Lab.

EROSION OF GRAPHITE BY STEEL SHOT. A. W. Simon. Dec. 2, 1942. Decl. Dec. 15, 1955. 4p. (A-419). \$1.80(ph OTS); \$1.80(mf OTS).

Preliminary experiments were undertaken to determine the amount of erosion produced when #8 steel shot passed through a 2-in diameter boring in a graphite block 15 in. long. The velocity of the shot was reduced by means of orifice plates with apertures of 1 and 1½ in. respectively, placed at the outlet of the block. The shot was circulated by means of a pneumatic conveyor. It was found that with the 1 in. aperture in place, conditions of uniform "flow" of shot with a velocity of 2.6 inches per second were produced, and that under these conditions there was negligible erosion after 8 hours of operation; on the other hand, with the 1½ in. aperture in place conditions approximating "free fall" with a maximum possible velocity of 20.2 ft. per second (actual velocity reduced by collisions) were produced, and that under these conditions



there was considerable erosion after 4 hours of operation. It is concluded that if it were necessary to use the process employing circulating uranium shot, it might be possible to find conditions under which the erosion could be reduced to a minimum. (auth)

### 3472 KAPL-789

Knolls Atomic Power Lab., Schenectady, N. Y.  
MEASUREMENTS OF THERMAL CONDUCTIVITY  
ELECTRICAL RESISTIVITY AND THERMOELECTRIC  
POWER OF GRAPHITE. W. W. Tyler and A. C. Wilson,  
Jr. July 24, 1952. Decl. Dec. 6, 1955. 54p. Contract  
W-31-109-Eng-52. \$6.30(ph OTS); \$3.00(mf OTS).

The thermal conductivity, electric conductivity, and thermoelectric power were measured in the temperature range from 20 to 300°K for samples of CSF graphite, AGOT graphite, lampblack graphite, natural molded graphite, and two samples of pile-irradiated CSF graphite. The results of these measurements are presented and discussed briefly in relation to theory. (C.H.)

### 3473 Y-149

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

PURIFICATION OF GRAPHITE: INITIAL STUDIES. W. L. Ross and C. B. Graham. Mar. 10, 1948. Decl. Dec. 8, 1955. 15p. Contract W-7405-eng-26. \$3.30(ph OTS); \$2.40(mf OTS).

An experiment is described in which it was determined that the impurities in C-18 graphite can be almost completely eliminated. The process involves vapor phase chlorination of the graphite with chlorine gas at approximately 1800°C. It was found that good purification was attained by using a sweep flow of gases through the reactor. (auth)

Refer also to abstracts 3738 and 3810.

## LABORATORIES AND EQUIPMENT

### 3474 AECD-3865

Hanford Works, Richland, Wash.

THE HANFORD POLAROGRAPH. William N. Carson, Jr. April 14, 1949. Decl. Dec. 5, 1955. 13p. Contract [W-31-109-eng-52]. (HW-R-13051). \$3.30(ph OTS); \$2.40(mf OTS).

The Hanford Polarograph measures the current at two points, one above the halfwave potential and one below the halfwave potential, on the current-voltage curve (polarogram) obtained from a polarographic cell. The difference in these values, less a constant residual current experimentally determined, comprises the diffusion current. The operation of the polarograph has been simplified so that a determination of the diffusion current can be made in two minutes. Comparison of the curves, diffusion current vs. concentration, obtained from the Hanford polarograph and a Sargent Model XXI polarograph on the same solutions shows no significant difference. (auth)

### 3475 CF-51-10-97

Oak Ridge National Lab., Tenn.

OPERATING MANUAL—INSTRUMENTS. C. B. Amberson and A. M. Larson. Oct. 4, 1951. 135p. Decl. Dec. 19, 1955. 135p. Contract [W-7405-eng-26]. \$21.30(ph OTS); \$6.90(mf OTS).

An operating manual is given for the instrumentation

for recording and controlling the process variables in remotely controlled equipment of radiochemical processing plants. (B.J.H.)

### 3476 K-39

Carbide and Carbon Chemicals Corp. [K-25 Plant], Oak Ridge, Tenn.

USE OF THE LINE RECORDER AS A HELIUM LEAK DETECTOR. N. H. Pease. Sept. 10, 1947. Decl. Dec. 5, 1955. 3p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Experiments were conducted with the line recorder main magnet shunted to determine if the He peak could be detected with high enough sensitivity so that He leak testing of cells could be accomplished from the operating floor. Weakening of the magnetic field by means of a shunting piece of iron reduces the voltage needed to resolve the mass 4 peak to a value which may be obtained from the high voltage supply. The tests made show that the He peak could be observed, but even if the sensitivity of the line recorder were increased by all known practical means it could not equal the sensitivity of the G.E. Leak Detector. (auth)

### 3477 KLX-1356

Kellex Corp., New York.

PROJECT COMPLETION REPORT; THOMPSON QUICK DISCONNECT DEVELOPMENT. Job 24-B3. E. W. Ruhl. Aug. 16, 1951. Decl. Dec. 5, 1955. 26p. Contract AT(30-1)-850. \$4.80(ph OTS); \$2.70(mf OTS).

The development, prototype production, and testing of a modified Thompson Quick Disconnect for use in radiochemical process lines is discussed. A 1-in. pipe connector has been developed for use where highly corrosive radioactive fluids are transferred under limited temperature conditions. (auth)

## RADIATION CHEMISTRY

### 3478 AECD-3807

Knolls Atomic Power Lab., Schenectady, N. Y.

GAMMA-INDUCED LIGHT PRODUCTION IN WATER. J. A. Rich and R. E. Slovacek. Sept. 19, 1952. Decl. with deletions Dec. 5, 1955. 32p. Contract W-31-109-Eng-52. \$6.30(ph OTS); \$3.00(mf OTS).

The mechanism of light production in H<sub>2</sub>O is shown to be due predominantly to the Cherenkov process. Measurement of the radiant flux was carried out for "infinite volume" and for spherical volumes of H<sub>2</sub>O of different radii. (auth)

## RADIATION EFFECTS

### 3479 AECD-3810

North American Aviation, Inc., Downey, Calif.

RADIATION EFFECTS QUARTERLY PROGRESS REPORT [FOR] APRIL-JUNE 1954. Frank E. Faris, ed. Nov. 1, 1954. Decl. with deletions Dec. 6, 1955. 52p. Contract AT-11-1-GEN-8. \$9.30(ph OTS); \$3.60(mf OTS).

Two theories on the anomalous low temperature thermal conductivity of graphite were tested by measurements with a single graphite crystal. It was concluded that the conductivity has a T<sup>2</sup> dependence at low temperature, and that the T<sup>3</sup> dependence is explained by a two-medium theory involving intergranular C. The theoretical treatment of the two-medium theory is extended from previous studies to



include the effect of neutron damage on several artificial graphites, as well as the effect of bromination. An apparatus was constructed for measuring the magnetic susceptibility of solids at liquid- $N_2$  temperatures. Results for graphite are presented. Another device was designed for measuring the temperature dependence of thermal conductivity, electrical resistivity, and thermoelectric power for cyclotron-irradiated graphite. Graphical results for a temperature range of 5 to 300°K are given. Previously determined power and electrical resistivity of graphite at -180°C and -190°C, respectively, are compared for irradiations made at +35, -94, and -170°C. Several determinations were made of the activation energy for the room-temperature annealing state of cyclotron-irradiated iodide-processed Th. The tensile properties of this material were measured at 77 and 295°K. Potassium chloride crystals colored in Na vapor were analyzed, and it was found that no Na was present in the interior of the crystal. The absorption spectrum, however, showed a new band that is found only in KCl colored by Na. The nature of this band is not clear, although it occurs in a region in which N-band structure in radiation-damaged crystals occurs. (K.S.)

#### 3480 CC-1321

Chicago. Univ. Metallurgical Lab.  
THE EFFECT OF RADIATION ON WATER AND AQUEOUS SOLUTIONS OF INORGANIC SUBSTANCES. A. O. Allen. Feb. 22, 1944. Decl. Dec. 15, 1955. 29p. (A-1874) \$4.80 (ph OTS); \$2.70(mf OTS).

Electrons and x rays dissociate water through ionization into oxidizing and reducing fragments, which probably have the formulas OH and H. In the absence of any solute, the fragments recombine and no net reaction occurs. If any oxidizable or reducible substance is dissolved in the water, it will react with the fragments, becoming oxidized or reduced. Thus, oxygen dissolved in the water is reduced to hydrogen peroxide, and ferrous, arsenite and other reducing ions are oxidized with the formation of an equivalent amount of hydrogen gas. Iodide and bromide ions sensitize the decomposition of water to hydrogen peroxide and hydrogen; bicarbonate ion and  $CO_2$  also yield a peroxide, which may be percarbonic acid. The amount of reaction occurring for a particular exposure is (in the absence of complicating chain reactions) independent of the concentration of solute, at least above  $10^{-4}$  M, and probably also independent of the nature of the solute, being fixed only by the number of ionizations produced by the radiation. To produce one chemically effective ionization in liquid water appears to require the absorption of about 80 ev of energy from the radiation. Heavy ionizing particles, including protons (recoils produced by action of neutrons passing through the water), deuterons, alpha particles and fission recoils, act on water directly to form hydrogen and hydrogen peroxide, which in turn decomposes to yield oxygen. If anything is dissolved in the water, the decomposition reaction is superimposed on the oxidation-reduction reactions of the solute. The kinetics and the mechanism of the decomposition are rather obscure; the back-reaction of the dissolved products, hydrogen and oxygen, to re-form water appears to play an important role. Corrosion of aluminum and of other metals is not greatly affected by radiation, at least in all experiments made to date. (auth)

#### SEPARATION PROCEDURES

##### 3481 AECD-3859

[Tennessee Eastman Corp., Oak Ridge, Tenn.]  
THE EFFECT OF TEMPERATURE ON THE DISTRIBUTION OR NITRIC ACID BETWEEN DIBUTYL CARBITOL AND AQUEOUS SOLUTIONS OF COPPER NITRATE. C. D. Shacklett and W. J. Wilcox, Jr. Jan. 17, 1946. Decl. Dec. 3, 1955. 12p. (CD-954-14). \$3.30(ph OTS); \$2.40 (mf OTS).

At a constant acidity in the aqueous phase, the distribution coefficient  $K_d$  (where  $K_d = [\text{acid}]_{\text{carbitol}} / [\text{acid}]_{\text{aqueous}}$   $Cu(NO_3)_2$  decreases as the temperature is increased; at a constant temperature  $K_d$  increases as the density of the aqueous phase is increased. (C.W.H.)

##### 3482 AECD-3905

Massachusetts Inst. of Tech., Oak Ridge, Tenn. Engineering Practice School.  
ANALYSIS OF ZIRCONIUM PURIFICATION COLUMNS. E. I. Goodman, R. F. Abbanat, A. G. Bates, and D. C. Lea. Dec. 16, 1950. 42p. Decl. Dec. 7, 1955. (KT-104). \$7.80(ph OTS); \$3.30(mf OTS).

Operating characteristics of three spray columns, the extractor, stripper, and scrubber, in the zirconium solvent-extraction pilot plant are given. Variables affecting the Hf-Zr separation are discussed. (C.W.H.)

##### 3483 CC-264

[Clinton Labs., Oak Ridge, Tenn.]  
THE EXTRACTION METHOD OF PURIFICATION OF URANYL NITRATE. L. S. Myers, Jr., E. C. Anderson, Sol Wexler, and G. E. Boyd. Aug. 28, 1942. Decl. Dec. 13, 1955. 9p. (A-295). \$1.80(ph OTS); \$1.80(mf OTS).

Three extractions of a diethyl ether solution of uranyl nitrate with small portions of water are effective in removing rare earths, as is shown by radio-gadolinium and radio-europium tracer experiments. A study of representative ethers, alcohols, ketones, and esters showed that diethyl ether and a mixture of 85% ethyl methyl ketone with 15% xylene are the best solvents for the extractions. At 25°C a saturated diethyl ether solution is 1.8 molar, and a similar solution in the ketone-xylene mixture is 2.0 molar. An empirical relation for the distribution ratio between ether and water is  $K = C_s / C_w^{0.3} = 0.20$  where  $C_s$  is the equilibrium concentration in the ether layer of the uranyl nitrate, and  $C_w$  that in water. A similar equation for the ketone-xylene mixture is  $K = C_s / C_w^{1.24} = 0.60$ . Di-ethyl ether gives the better extraction. Sodium chloride, sodium nitrate, and uranyl chloride have no deleterious effect on the extraction. However, more than four ml of nitric acid per hundred ml of saturated ether solution reduce the efficiency of the extraction in removing UX. (auth)

##### 3484 CC-2401

[Ames Lab., Ames, Iowa].  
A METHOD OF RECOVERING THORIUM FROM SLAG MATERIALS. Problem Assignment No. 16. Oliver Johnson and R. W. Fisher. Mar. 23, 1945. Decl. Dec. 13, 1955. 7p. Contract W-7405-eng-82. \$1.80(ph OTS); \$1.80(mf OTS).

A method of recovering thorium from slag from the bomb process of producing thorium has been developed. HCl and NaOH are the only chemicals required in quantity. Materials required for a representative slag are given. (auth)



**3485** CC-2962

[Ames Lab., Ames, Iowa].

PRECIPITATION OF THORIUM OXALATE FROM NITRIC ACID SOLUTIONS. Problem No. 117. A. S. Ayers. Oct. 5, 1945. Decl. Dec. 15, 1955. 5p. Contract W-7405-eng-82. \$1.80(ph OTS); \$1.80(mf OTS).

Data are reported from a study of factors affecting the precipitation of Th oxalate from nitric acid solutions. (C.H.)

**3486** CF-51-7-120

[Oak Ridge National Lab., Tenn.]

PERFORMANCE OF HOT COPPER WHEN USED FOR THE REMOVAL OF OXYGEN AND OXIDES OF NITROGEN FROM A GAS STREAM. H. O. Weeren. July 18, 1951. Decl. Dec. 16, 1955. 35p. Contract [W-7405-eng-26]. \$6.30(ph OTS); \$3.00(mf OTS).

An investigation was made of the efficiency with which a heated Cu bed will remove oxygen and the oxides of nitrogen from gas mixtures at various temperatures and flow rates. Mixtures of NO and N, N<sub>2</sub>O and N, and O and N were fed to chemical reactor at various flow rates and at different reactor temperatures. The effectiveness with which hot Cu removed the O and oxides of N was measured. Calculations based on the findings indicated that 1500 lb of Cu would be required to remove the O and N oxides from the gases passing during one day through the dissolver off-gas system of the Arco Chemical Processing Plant. Consideration of this method for removal of nitrogen oxides at the Arco plant was abandoned. (C.H.)

**3487** CF-51-10-28

[Oak Ridge National Lab., Tenn.]

PUREX PROCESS. VAPOR PRESSURE OF AMSCO 123-15 AND OF 30% TBP IN AMSCO 123-15. L. E. Line, Jr. Oct. 3, 1951. Decl. Dec. 15, 1955. 5p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Since Amsco 123-15 diluent is a potential industrial hazard, the vapor pressures of 100% Amsco 123-15 and 30% tributyl phosphate - 70% Amsco 123-15 were determined over the range 20 to 185°C. Data are tabulated and graphed. (C.H.)

**3488** CF-52-2-164

Oak Ridge National Lab., Tenn.

ADSORPTION OF FISSION PRODUCTS ON STAINLESS STEEL IN IAW SOLUTION AND SUBSEQUENT DESORPTION. Quarterly Report for Period November 10, 1951 - February 10, 1952. M. R. Bennett. Feb. 18, 1952. Decl. Dec. 15, 1955. \$1.80(ph OTS); \$1.80(mf OTS).

The adsorption equilibrium on stainless surfaces for all fission products other than niobium was established within six hr with a specific adsorption activity of approximately  $7.0 \times 10^4$  c/m/in.<sup>2</sup> gross  $\beta^-$ . Approximately 75% of the total  $\beta$  activity adsorbed within the first 12 hr was due to Zr-Nb; 15% was due to TRE, and 6% was due to Ru, Cs, and Zr. The adsorption equilibrium for fission products on Type 347 stainless steel appears to be slightly higher than for Type 309, by a factor of 1.05 to 1.08. Results are tabulated. (auth)

**3489** CF-53-1-283

Oak Ridge National Lab., Tenn.

DEVELOPMENT OF DECONTAMINATION REAGENT. Quarterly Report for Period November 1, 1952 to February 1, 1953. M. L. Feldman and R. F. Rogers.

Jan. 26, 1953. Decl. Dec. 16, 1955. 15p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

Procedures were evaluated for the decontamination of stainless steel. One criterion was that the pH of the final waste solutions must be high or neutral. Results are tabulated which were obtained by decontamination with 15 solution treatments. Solutions and procedures are also tabulated. The method of choice consists of 6.1M NaOH - 1M Na<sub>2</sub>C<sub>4</sub>H<sub>4</sub>O<sub>6</sub> used at 85°C for 0.5 hr with vigorous agitation followed by 1M H<sub>2</sub>C<sub>2</sub>O<sub>4</sub> - 0.1M NaF under the same conditions. This procedure should be repeated. (C.H.)

**3490** CNL-41

Clinton National Lab., Oak Ridge, Tenn.

THE BEHAVIOR OF RUTHENIUM UNDER SOLVENT EXTRACTION. G. R. B. Elliott and F. T. Miles. Feb. 27, 1948. Decl. Dec. 20, 1955. 30p. Contract W-35-058-eng-71). \$4.80(ph OTS); \$2.70(mf OTS).

Studies were carried out to help understand the two-phase distribution behavior of ruthenium. Distribution data are presented. It was found that the distribution behavior could be explained by four forms of ruthenium and various equilibrium constants and reaction rates. Estimates of these values are given and a possible assignment of states is suggested. (auth)

**3491** K-447

Carbide and Carbon Chemicals Co. K-25 Plant, Oak Ridge, Tenn.

SEPARATION OF COPPER, IRON, NICKEL AND URANYL IONS BY ION EXCHANGE COLUMNS. H. L. Bench, R. H. Capps, M. R. Skidmore, H. B. Weisblatt, and R. H. Winget. July 20, 1949. Decl. Dec. 27, 1955. 32p. (KLO-127). \$6.30(ph OTS); \$3.00(mf OTS).

The adsorption and elution characteristics of Cu, Fe, Ni, and uranyl ions on Dowex 50 synthetic exchange resin were studied with small columns. It was found possible to separate Cu and Ni from U adsorbed on a column of the Na form of Nalcite high capacity exchange resin (Dowex 50) using 5% ammonium citrate as an elutriant at pH 7, followed by the same elutriant at pH 3. Of the total U in the mixture, 83% was recovered in 160 ml of eluate. Sixty-six % was recovered free of contamination in 70 ml, 60% being concentrated in a 20 ml fraction of eluate. (auth)

**3492** M-2327

Purdue Univ., Lafayette, Ind.

REMOVAL OF ETHER PEROXIDES FROM DIETHYL ETHER BY EXTRACTION WITH CERTAIN AQUEOUS SOLUTIONS. A. A. Alberts. Mar. 21, 1946. Decl. Dec. 5, 1955. 9p. Contract W-7405-eng-74. \$1.80(ph OTS); \$1.80(mf OTS).

An investigation was made to determine the effect produced upon the concentration of other peroxides in diethyl ether by extraction with various solvents. These data can be used to show the probability of ether peroxide formation during a continuous extraction process involving diethyl ether. (J.E.D.)

**3493** M-4241(Pt.III)

Princeton Univ., N. J. Frick Chemical Lab.

A METHOD FOR THE DETERMINATION OF TRACES OF METALS. III. STUDIES OF THE DISTILLATION OF AMALGAMS. C. E. Bricker, N. H. Furman, and Bruce McDuffie. 1946. Revised Oct. 1947. Decl. Dec. 5, 1955. 9p. \$1.80(ph OTS); \$1.80(mf OTS).



Successful recovery of milligram quantities of Cd, Co, Fe, Ni, Cu, and Zn from amalgams was achieved by distillation in a  $N_2$  atmosphere. (K.S.)

#### 3494 M-4483

[National Bureau of Standards, Washington, D.C.]  
PROGRESS REPORT NO. 4 ON THE SEPARATION OF ZIRCONIUM FROM HAFNIUM. [194?]. Decl. Nov. 29, 1955. 4p. \$1.80(ph OTS); \$1.80(mf OTS).

Preliminary investigations indicate that a freshly prepared precipitate of  $Zr_3(PO_4)_4$ , when agitated in an entirely different solution from which it was formed had the property of removing Hf to a certain extent. (auth)

#### 3495 RL-4.6.151

[California. Univ., Berkeley. Radiation Lab.]  
THE HYPOSULFITE-pH CONTROL METHOD OF TUBALLOY [U]-IRON SEPARATION. E. L. Wagner. June 3, 1943. Decl. Jan. 5, 1956. 9p. \$1.80(ph OTS); \$1.80(mf OTS).

The procedure consists of the following steps: reduction of  $UO_2^{2+}$  and  $Fe^{3+}$  with  $(NH_4)_2SO_4$  to  $U^{4+}$  and  $Fe^{2+}$ ; precipitation with  $NH_4OH$  of  $U(OH)_4-U(SO_3)_2$  at pH 4.5, leaving the  $Fe^{2+}$  in solution. (K.S.)

#### 3496 UCRL-861

California. Univ., Berkeley. Radiation Lab.  
ALKYL PHOSPHORIC ACID EXTRACTIONS. D. C. Stewart and T. E. Hicks. Aug. 9, 1950. Decl. Dec. 7, 1955. 40p. Contract W-7405-eng-48. \$6.30(ph OTS); \$3.00(mf OTS).

Organic solvent extraction techniques were used to separate the mono- and di-alkyl substituted commercial phosphoric acid mixtures. Extraction coefficients and titration curves for several systems are presented. Tracer quantities of  $U^{233}$  were extracted by the separated acids. The equilibrium extraction reaction for the moderate-to-high initial-acid systems is proposed. Tracer  $U^{233}$  extractions by TBP seemed to verify previous studies of the same system by other laboratories. Tracer  $Pu^{239}$  extraction by dibutyl phosphoric acid from  $HNO_3$  solutions are presented. Some preliminary experiments on the separability of  $U^{233}$  and  $Pu^{239}$ , by alkyl phosphoric acid extraction, were undertaken and the data presented. (auth)

Refer also to abstract 3566.

### SORPTION PHENOMENA

#### 3497 K-372

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

ABSORPTION OF SILICON TETRAFLUORIDE BY ACTIVATED ALUMINA. A. D. Horton and S. S. Kirsliis. Mar. 23, 1949. Decl. Dec. 5, 1955. 14p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

The absorption of  $SiF_4$  on activated alumina was determined in the temperature range from 22.5 to 575°C. At each temperature, a mixture of 1%  $SiF_4$  and 99% N was passed through two Pregl absorption tubes, each containing 2 g of alumina, for 2 hr at a flow rate of 40 ml/min. Absorption of  $SiF_4$  was complete at each temperature when 4 g of absorbent were used. Absorption with 2 g of absorbent was found to be incomplete, but it became more complete at higher temperatures. Rapid, complete condi-

tioning of activated alumina was achieved by heating in a Pt container at 750°C for three hr. (auth)

### SYNTHESES

#### 3498 A-796

Columbia Univ., New York. Div. of War Research.  
PREPARATIVE METHODS. H. I. Schlesinger. Feb. 1943. Decl. Dec. 8, 1955. 12p. Contract OEMsr-368. (100XR-158). \$3.30(ph OTS); \$2.40(mf OTS).

Procedures are summarized for the preparation of uranium borohydride; aluminum borohydride; methyl borate; sodium trimethoxyborohydride; diborane; lithium borohydride; and sodium borohydride. Apparatus used is illustrated. (C.H.)

### TRANSURANIC ELEMENTS AND COMPOUNDS

#### 3499 ANL-4654

Argonne National Lab., Lemont, Ill.  
AN INTERIM REPORT ON STUDIES OF THE THERMIONIC PROPERTIES OF SURFACES CONSISTING OF PLUTONIUM ATOMS ADSORBED ON OXYGENATED TUNGSTEN. T. E. Phipps, E. G. Rauh, and O. C. Simpson. Aug. 27, 1951. Decl. Jan. 6, 1956. 38p. Contract W-31-109-eng-38. \$6.30(ph OTS); \$3.00(mf OTS)

Attempts were made to ionize Pu on the surface of a tungsten filament exposed to an atomic beam of Pu atoms. No evidence of surface ionization was found under several experimental conditions, from which fact it was concluded that the ionization potential is greater than 6.2 volts. Electron emission from the filament was followed as Pu atoms were deposited on the surface at a constant rate. A  $\log i$ ,  $\log t$  plot exhibited the same characteristics as similar plots for the adsorption of other metal atoms: a linear portion, a maximum, and a decrease toward a constant value. Adsorbed oxygen atoms were shown to increase the slope of the linear portion from about 4 for small oxygen coverage to 8.5 for complete oxygen coverage. By following the evaporation of the adsorbed Pu atoms thermionically the heat of evaporation of Pu from tungsten was determined to be 140 to 145 kcal mole<sup>-1</sup> at low concentrations of adsorbed Pu atoms and was shown to decrease with increasing concentration. The evidence indicates that Pu is adsorbed as ions among adatoms of oxygen in a mixed film rather than as a second layer on top of the adsorbed oxygen atoms. It is concluded that there are no known experimental conditions under which Pu may be ionized by the method of surface ionization. (A.G.)

#### 3500 CK-942

California. Univ., Berkeley. Radiation Lab.  
THE DISTRIBUTION OF PLUTONIUM TRACER BETWEEN METALS AND THEIR MOLTEN HALIDES. I. THE URANIUM-URANIUM BROMIDE SYSTEM. R. A. Webster. II. THE LEAD-LEAD CHLORIDE SYSTEM. B. J. Fontana. [194?]. Decl. Dec. 13, 1955. 12p. \$3.30(ph OTS); \$2.40(mf OTS).

Studies were initiated on the high-temperature oxidation-reduction relations of Pu in  $U-UBr_3$  and  $Pb-PbCl_2$  systems. Plutonium appears to be more electropositive than U or Pb. (C.W.H.)



**3501 CK-1359**

California. Univ., Berkeley. Radiation Lab.  
THE DISTRIBUTION OF PLUTONIUM TRACER BETWEEN METALS AND THEIR MOLTEN HALIDES. III. FURTHER EXPERIMENTS IN THE URANIUM - URANIUM BROMIDE SYSTEM INCLUDING EXPERIMENTS WITH THORIUM TRACER. IV. THE MANGANESE - MANGANOUS CHLORIDE SYSTEM. V. THE CALCIUM - CALCIUM CHLORIDE SYSTEM. R. A. Webster. Feb. 1, 1944. Decl. Dec. 12, 1955. 17p. Contract [W-7405-eng-48]. (A-2004). \$3.30(ph OTS); \$2.40(mf OTS).

Additional studies on the electrochemical properties of Pu in U- $\text{UBr}_3$ , Mn-Mn $\text{Cl}_2$ , and Ca-Ca $\text{Cl}_2$  systems indicate that Pu is more electropositive than U and Mn and less electropositive than Ca. (See also CK-942). (C.W.H.)

**3502 CK-1529**

Chicago. Univ. Metallurgical Lab.  
THE DISTRIBUTION OF PLUTONIUM TRACER BETWEEN METALS AND THEIR MOLTEN HALIDES. VI. DISTRIBUTION OF PLUTONIUM AND URANIUM TRACERS IN THE MAGNESIUM METAL-HALIDE SYSTEM. B. J. Fontana. Feb. 21, 1944. Decl. Dec. 13, 1955. 15p. (A-2207). \$3.30(ph OTS); \$2.40(mf OTS).

Additional studies on the electrochemical behavior of Pu and U in Mg-Mg $\text{X}_2$  (where X = halide) suggest that Pu is more electropositive than U or Mg. (See also CK-942). (C.W.H.)

**3503 CK-1712**

[California. Univ., Berkeley. Radiation Lab.]  
THE DISTRIBUTION OF PLUTONIUM TRACER BETWEEN METALS AND THEIR MOLTEN HALIDES. VII. DISTRIBUTION OF PLUTONIUM TRACER IN THE STRONTIUM-STROMTIUM BROMIDE AND THE BARIUM-BARIUM BROMIDE SYSTEMS. B. J. Fontana. May 16, 1944. Decl. Dec. 15, 1955. 11p. (A-2437). \$3.30(ph OTS); \$2.40(mf OTS).

Investigations on the high-temperature oxidation-reduction relations of Pu in Sr-Sr $\text{Br}_2$  and Ba-Ba $\text{Br}_2$  systems indicate that Sr and Ba are more electropositive than Pu. (See also CK-942.) (C.W.H.)

**3504 CN-1702**

[Chicago. Univ.] Metallurgical Lab.  
CHEMICAL RESEARCH—BASIC CHEMISTRY OF PLUTONIUM REPORT FOR MONTH ENDING JUNE 1, 1944. June 26, 1946. Decl. Dec. 13, 1955. 35p. (A-2431) \$6.30(ph OTS); \$3.00(mf OTS).

Progress is reported in the following studies: measurements of oxidation potentials of Pu(III)-Pu(IV) couples; measurements of the solubilities of Pu(III) and Pu(IV) phosphates and Pu(III) and Pu(IV) oxalates in HCl or  $\text{HNO}_3$  at various temperatures; the co-separation of Pu with various carriers; the crystal structure of Pu(IV) phosphate and oxalate; the ether extraction of Pu; the hydrolysis of Pu(III) and Pu(IV); the precipitation of Pu(OH) $_4$  from nitrate and from sulfate solution; the rate of oxidation of Pu(IV) by  $\text{HNO}_3$  in various concentrations of  $\text{H}_2\text{SO}_4$ ; the rate of reduction of Pu(IV) by  $\text{SO}_2$ ; the rate of oxidation of Pu(IV) by ceric nitrate and by dichromate in nitric acid; variations in the optical density of the Pu(III) absorption bands with concentration of Pu; basic chemical studies on the Bi $\text{PO}_4$  extraction of Pu; and the purification of Pu following recovery from a large variety of materials. (C.H.)

**3505 LA-112**

Los Alamos Scientific Lab., N. Mex.  
THE PREPARATION OF PLUTONIUM TRICHLORIDE. C. S. Garner, S. E. Bakes, I. B. Johns, G. H. Moulton, and B. Weinstock. July 24, 1944. Decl. Dec. 13, 1955. 14p. Contract [W-7405-eng-36]. \$3.30(ph OTS); \$2.40(mf OTS).

The preparation of Pu $\text{Cl}_3$  by the chlorination of Pu $\text{O}_2$  in the presence of CCl $_4$  vapor and by other methods are described. Several physical properties of Pu $\text{Cl}_3$  are reported. (C.W.H.)

**3506 LA-172**

[Los Alamos Scientific Lab., N. Mex.]  
DECOMPOSITION PRODUCTS OF PLUTONYL NITRATE AND PLUTONIUM OXALATE. G. H. Moulton. Nov. 14, 1944. Decl. Dec. 13, 1955. 10p. Contract [W-7405-eng-36]. \$1.80(ph OTS); \$1.80(mf OTS).

Results show that both of these compounds decompose directly to the dioxide with no evidence of formation of any intermediate compounds. (auth)

**3507 LA-381**

Los Alamos Scientific Lab., N. Mex.  
EQUILIBRIUM CONSTANTS AND HEATS OF REACTION FOR THE HYDROFLUORINATION OF URANIUM DIOXIDE AND PLUTONIUM DIOXIDE. I. B. Johns. Aug. 30, 1945. Decl. Dec. 10, 1955. 10p. \$1.80(ph OTS); \$1.80(mf OTS).

Direct determinations were made of the equilibrium conditions for the reactions of HF with  $\text{UO}_2$  at 600°C, 705°C and 800°C and with Pu $\text{O}_2$  at 400°C and 600°C. From these data, the equilibrium constants at these temperatures were calculated. From the change of equilibrium constant with temperature, the heats of reaction were calculated. The heat of reaction of HF on  $\text{UO}_2$  to yield  $\text{UF}_4$  was found to be  $-\Delta H = 42080$  cal/mol. This is in fair agreement with the value 45800 cal/mol calculated from the known heats of formation of the compounds involved in the reaction. The heat of reaction of HF on Pu $\text{O}_2$  calculated from the equilibrium constants at 400° and 600°C is 10220 cal/mol. (auth)

**URANIUM AND URANIUM COMPOUNDS****3508 A-28**

Iowa State Coll., Ames.  
ORGANO URANIUM COMPOUNDS. I. [Report for Period January 21, 1941 to May 20, 1941]. Henry Gilman. Decl. Dec. 6, 1955. 8p. \$1.80(ph OTS); \$1.80(mf OTS).

Attempts to prepare compounds containing C-U linkages by direct reaction of U metal and of a U-Ni alloy with methyl iodide were unsuccessful. The displacement of Hg or Pb from the ethyl compounds of these metals by U did not take place under the conditions tried. Reactions of uranous chloride and of uranyl chloride with various organometallic compounds in several solvents resulted either in reduction of the salts with the formation of hydrocarbons or in no change. These results are quite comparable to those obtained with other transition elements and particularly reactions with Ti salts. The reaction of  $\text{UCl}_3$  with methylmagnesium iodide resulted in very little gas formation. This may have been due to traces of moisture or of uranous chloride. The reactions of this salt ( $\text{UCl}_3$ ) with other organometallic compounds in inert solvents (like benzene or petroleum ether) appear worthy of



further study. Reactions of uranium chlorides with less reactive organometallic compounds in alcoholic solutions result in secondary products due to solvolysis of the metal salts. This may also be true of long time reactions in ether. (auth)

### 3509 A-30

Iowa State Coll., Ames.

ORGANO URANIUM COMPOUNDS. III. [Report for Period] June 16, 1941 to August 9, 1941. Henry Gilman. Decl. Dec. 6, 1955. 5p. \$1.80(ph OTS); \$1.80(mf OTS).

Attempts are reported to prepare compounds containing C-U linkages. Reactions between p-tolyl diazonium chloride and U tetrachloride and between p-tolyl diazonium chloride and uranyl chloride yielded materials which contained both U and C. Other reactions reported were unsuccessful. (C.H.)

### 3510 A-523

Ames Lab., Ames, Iowa.

DIRECTIONS FOR THE PREPARATION OF  $X(OC_2H_5)_5$  [AND]  $X(OC_2H_5)_6$ . Henry Gilman. Feb. 6, 1943. Decl. Dec. 8, 1955. 15p. OSRD Project No. 346. (100XR-150). \$3.30(ph OTS); \$2.40(mf OTS).

Uranium pentaethoxide,  $U(OC_2H_5)_5$ , may be prepared by the reaction of  $UCl_4$  with sodium ethoxide followed by direct oxidation of the ethyl-alcohol solution of the intermediate product. Yields (~65%) were obtained. (C.W.H.)

### 3511 A-728

Du Pont de Nemours (E. I.) & Co. Jackson Lab., Wilmington, Del.

THE REACTION OF TUBEALLOY TETRAFLUORIDE WITH ANTIMONY PENTAFLUORIDE. Progress Report [covering period] October 15, 1942 to October 28, 1942. A. L. Linch. May 17, 1943. Decl. Dec. 8, 1955. 3p. (100XR-1216). \$1.80(ph OTS); \$1.80(mf OTS).

An attempt was made to synthesize  $UF_6$  by fluoride exchange between  $SbF_5$  and  $UF_4$ . Antimony pentafluoride with  $UF_4$  formed an equimolecular complex thermally stable to 200°C, decomposed by water to  $UF_4$ , and soluble in antimony salts. Heating to 650°C did not produce noticeable quantities of volatile U salts, but gave 15 to 20% yield of water soluble U derivatives in the residue. (C.H.)

### 3512 A-1008

Harshaw Chemical Co., Cleveland.

TENTATIVE METHODS FOR ANALYZING WE-22 ( $UF_4$ ). July 28, 1953. Decl. Dec. 8, 1955. 6p. \$1.80(ph OTS); \$1.80(mf OTS).

Procedures are described for the gravimetric determination of U and the volumetric determinations of  $UO_2F_2$ ,  $UF_4$ , and Fe in  $UF_4$  samples. (C.W.H.)

### 3513 A-1025

Mallinckrodt Chemical Works, St. Louis.

CONCENTRATION OF  $UX_1 [Th^{234}]$  FROM  $UO_2$ . H. Yeager and J. A. Kyger. Feb. 2, 1944. Decl. Dec. 2, 1955. 3p. Contract [W-14-108-eng-8]. \$1.80(ph OTS); \$1.80(mf OTS).

Thorium<sup>234</sup> was concentrated from nitrate solutions of  $UO_2$  by repeated ether- $H_2O$  extractions. The  $Th^{234}$  was then precipitated by addition of excess NaOH. A concentration factor of  $\sim 10^3$  was obtained. (C.W.H.)

### 3514 A-1058

Du Pont de Nemours (E. I.) and Co. Jackson Lab. [Wilmington, Del.]

PRELIMINARY PLANT PROCESS FOR THE MANU-

FACTURE OF SODIUM URANATE FROM URANIUM HEXAFLUORIDE CONTAINING  $\phi$ -DIMETHYLCYCLOHEXANE ( $C_8F_{18}$ ). D. X. Klein. Sept. 16, 1944. Decl. Dec. 8, 1955. 12p. \$1.80(ph OTS); \$1.80(mf OTS).

Uranium hexafluoride containing up to 40%  $\phi$ -dimethylcyclohexane is vaporized from its container into an aqueous caustic solution in a closed system. The resulting solution, at a pH of 7.0 to 7.5 is steam-distilled to recover the fluorocarbon. Sodium hydroxide solution is added to the hot solution to precipitate sodium uranate at a pH of 10.0 to 10.5. The soda salt is filtered, washed practically free of sodium fluoride and dried. (auth)

### 3515 A-1083

Mallinckrodt Chemical Works, St. Louis.

A SHORTER ASSAY METHOD FOR URANIUM MATERIALS AND SOME INTERFERENCES IN THE TITRATION. T. R. Barddack, C. L. French, G. L. Martin, and J. R. McCoy. May 14, 1945. Decl. Dec. 5, 1955. 11p. \$1.80(ph OTS); \$1.80(mf OTS).

A volumetric determination of U is described which makes use of cupron for the precipitation of molybdenum, followed by extraction with chloroform, and the usual cupferron separation. Interfering ions ( $NO_3^-$ ,  $V^{5+}$ ,  $U^{4+}$ , and Mo) are removed by this method. (C.W.H.)

### 3516 A-1277

Columbia Univ., New York. Div. of War Research.

THE THERMAL STABILITY OF URANIUM OXIDES AND URANIUM OXIDE HYDRATES IN WATER. D. Vier. May 26, 1944. Decl. Dec. 8, 1955. 55p. Contract W-7405-eng-50. (100K-R-654). \$9.30(ph OTS); \$3.60(mf OTS).

Data are presented from an investigation of the thermal stability of U oxide slurries. Most of the data presented deal with U trioxide hydrates. (C.H.)

### 3517 A-2702

Purdue Univ., LaFayette, Ind.

DETERMINATION OF TUBALLOY [URANIUM] WITH THE X-RAY SPECTROGRAPH. Summary Report. Oct. 25, 1945. Decl. Dec. 14, 1955. 9p. Contract W-7405-eng-74. \$1.80(ph OTS); \$1.80(mf OTS).

The applicability of the x-ray spectrograph to the problem of detecting small amounts of U in the presence of large amounts of other elements such as Cu, Fe, Cr, and Mn has been studied. The effects produced by the variation of several experimental conditions on the sensitivity of the instrument to the  $U L_{\alpha 1}$  line have been investigated. These experimental conditions include the potential applied on the x-ray tube, the time of exposure, the size of the angle of oscillation, the crystal used for the reflection grating, the type of film and the use of an intensifying screen in connection with the film. Using optimum conditions, namely 60 kv peak tube voltage, 10 ma. tube emission, sodium chloride crystal, Eastman No-Screen x-ray film and an exposure time of about 72 min per degree of oscillation, it was possible to detect the presence of one part of U in 2,000 parts of Fe by weight in a mixture of the oxides. (auth)

### 3518 A-2709

Purdue Univ., Lafayette, Ind.

TITRIMETRIC DETERMINATION OF URANIUM WITH POTASSIUM DICHROMATE. M. M. Kruder, W. S. Barnhart, H. Hunt, E. S. Gantz, and M. G. Mellon. Mar. 8, 1946. Decl. Dec. 8, 1955. 6p. Contract W-7405-eng-74. \$1.80(ph OTS); \$1.80(mf OTS).

A rapid titrimetric procedure is described for the



determination of U in presence of moderate amounts of Cr, Cu, Ni, Cl, and Fe. After correcting for Fe, a precision of about 1 part in 1000 was obtained under routine conditions. (auth)

**3519** A-3387

[Wisconsin Alumni Research Foundation].

FURTHER EXPERIMENTS ON THE PREPARATION OF  $UF_6$ . William Krasny Ergen. July 29, 1942. Decl. Dec. 13, 1955. 4p. (100RD-152). \$1.80(ph OTS); \$1.80(mf OTS).

The attempted preparations of  $UF_6$  by the reactions of  $UF_4$  with  $HgF$  and  $Cl_2$  or with  $HgF_2$  as fluorinating agent are described. Uranium(VI) fluoride was obtained in small yield. (auth)

**3520** A-3505

Du Pont De Nemours (E. I.) & Co. Jackson Lab.,  
Wilmington, Del.

METHODS OF CONTROLLING BULK DENSITY OF C-108 [ $UO_3$ ] PRODUCED FROM NON-ETHER-EXTRACTED C-106. [ $UO_2(NO_3)_2 \cdot 6H_2O$ ] C. W. Maynard, Jr. Dec. 3, 1945. Decl. Dec. 8, 1955. 6p. Contract W-7412-eng-151. \$1.80(ph OTS); \$1.80(mf OTS).

The bulk density of  $UO_3$  produced from non-ether extracted  $UO_2(NO_3)_2$  was lower than that produced from ether-extracted nitrate. The sulfate impurities appeared to affect the bulk density of the  $UO_3$  produced. (C.W.H.)

**3521** A-3506

Du Pont de Nemours (E. I.) and Co. Jackson Lab.,  
[Wilmington, Del.],

RAPID ANALYSIS FOR SMALL AMOUNTS OF URANIUM IN GYP CAKES. Problem Report [for] Period November 2, 1944–December 3, 1945. Alvan Donnan. Dec. 12, 1945. Decl. Dec. 7, 1955. 17p. Contract W-7412-eng-151. (JWD-69). \$3.30(ph OTS); \$2.40(mf OTS).

A colorimetric method for the determination of U in "gyp" is described. The method consists of acid digestion,  $Na_2CO_3$  digestion, filtration,  $H_2O_2$  addition, and color measurement. (C.W.H.)

**3522** A-3507

Du Pont de Nemours (E. I.) and Co. Jackson Lab.,  
[Wilmington, Del.]

MINIMIZING THE URANIUM CONTENT OF GYP CAKES. Problem Report [for] Period March 9, 1945 to September 25, 1945. Alvan Donnan. Dec. 17, 1945. Decl. Dec. 8, 1955. 8p. Contract W-7412-eng-151. (JWD-70). \$1.80(ph OTS); \$1.80(mf OTS).

The uranium content of gyp cakes can be decreased by substituting  $Na_2CO_3$  for  $CaCO_3$  during lime out and by extracting off-quality gyp with aqueous  $Na_2CO_3$ . (auth)

**3523** A-3550

Du Pont de Nemours (E. I.) & Co. Wilmington, Del.  
CHAMBERS WORKS PROCESS FOR THE MANUFACTURE OF SODIUM URANATE FROM N. G. SOLUTIONS OF URANYL NITRATE HEXAHYDRATE. J. A. Alexander. Jan. 24, 1945. Decl. Dec. 2, 1955. 4p. Contract W-7412-eng-3. \$1.80(ph OTS); \$1.80(mf OTS).

Sodium uranate is produced by adding excess soda caustic solution to N.G. solutions of uranyl nitrate. The solution is then filtered and the press cake is put into barrels. (C.W.H.)

**3524** A-3554

Du Pont de Nemours (E.I.) & Co. Engineering Dept.,  
Wilmington, Del.  
CHAMBERS WORKS PROCESS FOR THE MANUFACTURE

OF SODIUM URANATE FROM SUMP DRAININGS. (M. W. 348.06). James A. Alexander. Jan. 29, 1945. Decl. Dec. 2, 1955. 3p. Contract W-7412-Eng-3. \$1.80(ph OTS); \$1.80(mf OTS).

Sodium uranate may be precipitated by adding NaOH in excess to the sump drainings (uranyl nitrate solutions). (C.W.H.)

**3525** A-4024

Kellex Corp., New York.

SOME REACTIONS OF URANYL ION IN ALKALINE SOLUTION. (Research Paper No. E-12A). Robert H. Lafferty, Jr., S. C. Schuman, K. J. Radimer, and S. H. Smiley. Apr. 12, 1946. Decl. Dec. 2, 1955. 10p. \$1.80(ph OTS); \$1.80(mf OTS).

The absorption of  $UF_6$  in alkaline media was studied. In relation to the design of a suitable tower for absorption of the former, sodium bicarbonate was found to be the best alkaline reagent for the absorption in aqueous solution, ethanolamine the best non-aqueous reagent. The chemistry of each absorption has been examined insofar as it has related to design of an absorption tower for gaseous mixtures of  $F_2$ ,  $UF_6$ , and  $N_2$ . The formation of soluble U compounds formed when  $UF_6$  and  $F_2$  are discharged into a NaOH solution is discussed. (auth)

**3526** AECD-3851

Massachusetts Inst. of Tech., Cambridge.

URANIUM–ZIRCONIUM EXPLOSIONS IN NITRIC ACID. R. B. Russell. May 11, 1953. 5p. Decl. Dec. 5, 1955. Contract [W-7405-eng-175]. (MIT-RBR-4). \$1.80(ph OTS); \$1.80(mf OTS).

An investigation of explosions between a U–Zr alloy (80 wt. % U) and  $HNO_3$  indicates that the explosion is a result of surface shock. The mechanism of the explosion is unknown. (C.W.H.)

**3527** AECD-3854

Tennessee Eastman Corp., Oak Ridge, Tenn.

VAPOR PHASE CHLORINATION OF  $TO_3$  [ $UO_3$ ]. Progress Report. George S. Parsons, Charles L. McCabe, G. F. Engle, and C. E. Larson. Apr. 2, 1945. Decl. Jan. 4, 1956. 14p. Project 31. Contract W-7401-eng-23. (CD-564-CEL-A). \$3.30(ph OTS); \$2.40(mf OTS).

Progress is reported in a study of various laboratory methods for the gas phase chlorination of  $UO_3$ . The use of vertical tube chlorinators with a bore up to 3 in. with  $CCl_4$  as a chlorinating agent at temperatures not exceeding 500°C was shown to be possible. The high temperature chlorination of  $UO_3$  and C by  $Cl_2$ , and the chlorination of  $UO_3$  by  $CCl_4$  at high temperatures appeared to be a practical method for the preparation of  $UCl_4$ . Thionyl chloride used as a chlorinating agent at temperatures not exceeding 300°C was shown to be a very efficient chlorinating agent. (C.H.)

**3528** AECD-3867

Brown Univ., Providence.

PROGRESS REPORT [ON] CONTRACT OEMsr-290. SUPPLEMENT 2. Charles A. Kraus. Oct. 8, 1942. Decl. Dec. 12, 1955. 8p. (BT-8). \$1.80(ph OTS); \$1.80(mf OTS).

The solubility of uranyl nitrate in ethyl acetate was redetermined. Distribution coefficients of  $UO_2(NO_3)_2$  in several solvent pairs are given. The thermal decomposition of uranium peroxide was investigated. Gravimetric, volumetric, and conductance methods for the analysis of  $UO_2(NO_3)_2$  solutions were compared. (C.W.H.)



**3529** AECD-3875

Tennessee Eastman Corp., Oak Ridge, Tenn.

TUBALLOY TETRACHLORIDE [UCl<sub>4</sub>]. E. L. Wagner. Feb. 6, 1946. Decl. Dec. 2, 1955. 1p. [Contract W-7401-eng-23]. (C-2.381.4). \$1.80(ph OTS); \$1.80(mf OTS).

The properties, preparation, and chemical reactions of UCl<sub>4</sub> are graphically presented. (C.W.H.)

**3530** AECD-3897

Tennessee Eastman Corp., Oak Ridge, Tenn.

A SPECTROPHOTOMETRIC DETERMINATION OF MIXTURES OF HEXAVALENT AND TETRAVALENT [URANIUM]. L. J. Andrews, Ward B. Schaap, and J. W. Gates, Jr. Preliminary Report. Feb. 17, 1945. Decl. Dec. 15, 1955. 6p. Contract W-7401-eng-23. (CD-4003). \$1.80(ph OTS); \$1.80(mf OTS).

A spectrophotometric method for the analysis of solutions, containing U<sup>4+</sup> and U<sup>6+</sup>, has been developed. Optical densities of the solution are measured at 630 and 410 mμ from which the respective concentrations of U<sup>4+</sup> and U<sup>6+</sup> can be determined. The method is accurate to within 3%. (C.W.H.)

**3531** AECD-3908

Tennessee Eastman Corp., Oak Ridge, Tenn.

A DETERMINATION OF THE U-235 CONTENT IN HIGHLY IMPOVERISHED MATERIAL. A. E. Cameron and Roger F. Hibbs. May 9, 1946. Decl. Dec. 12, 1955. 6p. (B-6.460.14). \$1.80(ph OTS); \$1.80(mf OTS).

Mass spectrometric analyses of highly impoverished material for residual U<sup>235</sup> content are reported. A value of 25,000 for the ratio U<sup>238</sup>/U<sup>235</sup> was obtained. (C.W.H.)

**3532** AECD-3910

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

APPLICATION OF ASCORBIC ACID METHOD TO URANIUM IN SALVAGE SOLUTIONS. C. D. Rothenberger and W. R. Grimes. June 11, 1947. Decl. Dec. 7, 1955. 23p. [Contract W-7405-eng-26]. (H-4.360.14). \$4.80(ph OTS); \$2.70(mf OTS).

The ether extraction-ascorbic acid procedure for the determination of U content in plant salvage solutions is described. Pre-treatment of the solution with HClO<sub>4</sub> or activated carbon is necessary to remove interfering trace organic material. (C.W.H.)

**3533** AECD-3911

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

TENTATIVE PROCEDURES FOR ANALYSIS OF HCP PROCESS MATERIALS. H. J. Belknap, G. J. Nessel, and W. R. Grimes. May 28, 1947. Decl. Dec. 8, 1955. 49p. (H-4.360.12). \$7.80(ph OTS); \$3.30(mf OTS).

Procedures are presented for the potentiometric, spectrophotometric, and fluorimetric determinations of U in process materials; also, procedures are presented for the determination of Cl<sup>-</sup>, Cu, and Fe in process solutions. Analyses of UO<sub>2</sub>(NO<sub>3</sub>)<sub>2</sub>, UCl<sub>4</sub>, machine wash solution, rinse solution, reactor condensates, organic wastes, extracted gunk, and carbon bowl residue are outlined. (C.W.H.)

**3534** AECD-3917

Tennessee Eastman Corp., Oak Ridge, Tenn.

PREPARATION AND STABILITY OF COBALT TRIFLUORIDE. J. Whitney, F. Smith, and A. J. Miller. Oct. 15,

1945. Decl. Dec. 21, 1955. 4p. Contract W-7401-eng-23. (C-2.355.1). \$1.80(ph OTS); \$1.80(mf OTS).

Cobalt trifluoride CoF<sub>3</sub> was prepared by heating anhydrous CoCl<sub>2</sub> with F<sub>2</sub> at 300 to 400°C. It remains stable when kept in sealed glass tubes but absorbs H<sub>2</sub>O on exposure to air. (auth)

**3535** AECD-3932

Tennessee Eastman Corp., Oak Ridge, Tenn.

THE USE OF SODIUM DIETHYL DITHIOCARBAMATE AS A REAGENT FOR THE DETERMINATION OF T [U]. A. G. Jones. Apr. 1942. Decl. Dec. 22, 1955. 10p. Contract [W-7401-eng-23]. (C-4.360.9).

A rapid colorimetric method is presented for the determination of U in plant solutions. The absorbance of the uranium diethyl dithiocarbamate in CCl<sub>4</sub> is measured at 380μ. (C.W.H.)

**3536** AECD-3935

Tennessee Eastman Corp., Oak Ridge, Tenn.

THE DETERMINATION OF SMALL AMOUNTS OF THORIUM IN SOME URANIUM MATERIALS. E. W. Christopherson, R. W. Woodard, and C. E. Larson. Sept. 11, 1946. Decl. Dec. 21, 1955. 13p. Contract W-7401-eng-23. (C-0.380.8). \$3.30(ph OTS); \$2.40(mf OTS).

A method for the determination of small quantities of Th in the presence of large quantities of U is presented. Solid samples are dissolved in an appropriate acid. Reducible metals are removed by means of a Hg cathode. Excess acid is removed by fuming to dryness. The residue is dissolved in water and made alkaline with saturated (NH<sub>4</sub>)<sub>2</sub>CO<sub>3</sub> solution, thus complexing the U and permitting the precipitation of Th(OH)<sub>4</sub> with the aid of an Al(OH)<sub>3</sub> carrier. Thorium is determined colorimetrically with thoron. (auth)

**3537** AECD-3937

Tennessee Eastman Corp., Oak Ridge, Tenn.

DIRECT CONVERSION OF TF<sub>6</sub> [UF<sub>6</sub>] TO TCl<sub>4</sub> [UCl<sub>4</sub>]. Vincent P. Calkins. Sept. 25, 1945. Decl. Dec. 21, 1955. 6p. Contract W-7401-eng-23. (C-0.350.4). \$1.80(ph OTS); \$1.80(mf OTS).

Results indicate that the conversion of UF<sub>6</sub> to UCl<sub>4</sub> proceeds through a two-step process involving UF<sub>4</sub>. Uranium (IV) chloride can be prepared by the direct reaction of UF<sub>4</sub> with AlCl<sub>3</sub> or BCl<sub>3</sub>. (C.W.H.)

**3538** AECD-3945

Tennessee Eastman Corp., Oak Ridge, Tenn.

QUANTITATIVE RECOVERY OF TUBALLOY FROM TUBALLOY TETRAFLUORIDE. J. W. Gates, Jr., L. J. Andrews, and W. B. Schaap. Feb. 22, 1945. Decl. Dec. 22, 1955. 4p. Contract W-7401-eng-23. (CD-4005). \$1.80(ph OTS); \$1.80(mf OTS).

Uranium(IV) fluoride can be quantitatively converted to ammonium uranate by the following procedures: reaction of UF<sub>4</sub> with NH<sub>4</sub>OH, then H<sub>2</sub>O<sub>2</sub>, acidification with HNO<sub>3</sub>, and precipitation with NH<sub>4</sub>OH; reaction of UF<sub>4</sub> with H<sub>2</sub>SO<sub>4</sub>, then (NH<sub>4</sub>)<sub>2</sub>S<sub>2</sub>O<sub>8</sub>, and precipitation with NH<sub>4</sub>OH. Recoveries (~99%) of U were obtained. (C.W.H.)

**3539** AECD-3947

Tennessee Eastman Corp., Oak Ridge, Tenn.

THE PREPARATION OF TUBALLOY TETRACHLORIDE BY FLUIDIZATION. J. V. Hubbard, H. A. Perlmutter, H. L. Goren, and G. H. Clewett. Aug. 28, 1945. Decl. Dec. 21, 1955. 10p. Contract W-7401-eng-23. (C-5.350.3). \$3.30(ph OTS); \$2.40(mf OTS).



Preliminary investigation of the application of fluidization to  $\text{UF}_4$  production indicated this was a very promising method of contacting a chlorinating gas with  $\text{UO}_3$ . A procedure was developed wherein reaction time with unactivated Mallinckrodt oxide was only twenty minutes at 240 to 280°C, and the product was of high quality and uniform texture. Both  $\text{CCl}_4$  and thionyl chloride vapors were employed. With  $\text{CCl}_4$  an average yield of 94% was obtained from the somewhat crude apparatus. (auth)

### 3540 AECD-3952

Tennessee Eastman Corp., Oak Ridge, Tenn.  
THE CHLORINATION OF  $\text{TO}_3$  [ $\text{UO}_3$ ]. G. Gavlin and G. H. Clewett. Dec. 28, 1945. 12p. Decl. Dec. 19, 1955. Contract W-7401-eng-23. (C-5.350.5). \$3.30(ph OTS); \$2.40(mf OTS).

The applicability of specific mixtures and organic chlorocarbons in general toward the chlorination of  $\text{UO}_3$  has been tested by means of reactions in sealed glass tubes. The results show that thionyl chloride mixed with tetrachloroethylene or a bromomethane of the type  $\text{CHBrCl}_2$  will produce  $\text{UCl}_4$  directly. This same result is produced by  $\text{CBrCl}_3$  or  $\text{CBr}_2\text{Cl}_2$  alone. (auth)

### 3541 AECD-3953

Tennessee Eastman Corp., Oak Ridge, Tenn.  
SUMMARY OF INTERFERENCES IN THE FLUORESCENT DETERMINATION OF T. C. F. Coleman and A. A. Smales. [July 1945]. Decl. Dec. 19, 1955. 6p. Contract W-7401-eng-23. (C-4.360.2). \$1.80(ph OTS); \$1.80(mf OTS).

A study was made on the effects of the presence of 26 other ions on the fluorescence of a given amount of U. The fluorescent method used for the determination of U is described. Data are tabulated on the empirical quenching properties of the ions when 1  $\mu\text{g}$  of U is present in the sample. (C.H.)

### 3542 AECD-3954

Tennessee Eastman Corp., Oak Ridge, Tenn.  
THE AMMONIA REDUCTION AND ITS APPLICATION TO THE PREPARATION OF GREEN SALT. Dec. 29, 1945. 11p. Decl. Dec. 19, 1955. Contract W-7401-eng-23. (C-2.355.2). \$3.30(ph OTS); \$2.40(mf OTS).

Ammonia reacts readily with  $\text{TO}_3[\text{UO}_3]$  and  $\text{T}_3\text{O}_8[\text{U}_3\text{O}_8]$  at temperatures of 450° and above with the formation of  $\text{TO}_2[\text{UO}_2]$ . The reaction is applicable to the preparation of  $\text{TO}_2[\text{UO}_2]$  where it is desired as either a reaction intermediate or as final product. The ammonia reduction is directly applicable to the preparation of  $\text{TF}_4[\text{UF}_4]$ . When  $\text{NH}_3$  and HF as gases or from distillation of  $\text{NH}_4\text{F}$  or  $\text{NH}_4\text{HF}_2$  are simultaneously passed over  $\text{TO}_3[\text{UO}_3]$  at 500° or above, a simultaneous reduction and hydrofluorination produces  $\text{TF}_4$ . This reaction goes to completion, whereas the analogous reaction with  $\text{H}_2$  and HF introduced simultaneously produces  $\text{TF}_4[\text{UF}_4]$  only in partial yields. The  $\text{NF}_3\text{HF}$  method for preparation of  $\text{TF}_4[\text{UF}_4]$  can apparently be carried out very rapidly. It gives products of adequate density, and has so far been employed on batches of up to 60 g in half-inch depth with satisfactory results. (auth)

### 3543 AECD-3955

Tennessee Eastman Corp., Oak Ridge, Tenn.  
THE DIBUTYL CARBITOL-TUBANYL [URANYL] NITRATE ETHERATE. H. R. Grady, G. M. Armstrong, and J. W. Gates, Jr. Sept. 5, 1945. Decl. Dec. 19, 1955. 5p. Contract W-7401-eng-23. (C-1.365.5). \$1.80(ph OTS); \$1.80(mf OTS).

Uranyl nitrate etherate is formed during the solvent ex-

traction of aqueous uranyl nitrate solutions with dibutyl carbitol. Molecular constitution, physical properties, and chemical properties of the etherate are discussed. (C.W.H.)

### 3544 AECD-3959

Tennessee Eastman Corp., Oak Ridge, Tenn.  
TUBALLOY PEROXIDE [ $\text{UO}_4$ ]. PART II. THE INFLUENCE OF SULPHATE ON THE SOLUBILITY AND RATE OF PRECIPITATION OF TUBALLOY PEROXIDE [ $\text{UO}_4$ ]. P. F. Grieger, E. W. Christopherson, Roy Oringer, and J. W. Gates, Jr. April 19, 1945. Decl. Dec. 22, 1955. 32p. Contract W-7401-eng-23. (CD-4016). \$6.30 (ph OTS); \$3.00(mf OTS).

The solubility of  $\text{UO}_4$  has been determined over a fairly wide range of  $\text{SO}_4^{2-}$ ,  $\text{H}^+$  and  $\text{H}_2\text{O}_2$  concentrations. Sulfate decreases the rate of precipitation of  $\text{UO}_4$ . The equilibrium solubility of  $\text{UO}_4$  varies inversely with  $\text{H}_2\text{O}_2$  concentration. The solubility increases with the first power of  $\text{SO}_4^{2-}$  at low concentrations but in the neighborhood of 1.0M  $\text{SO}_4^{2-}$  the solubility is roughly proportional to the square of sulfate concentration. The solubility increases with a power of hydrogen ion slightly greater than one. The regions of quantitative precipitation have been plotted. (auth)

### 3545 AECD-3960

Tennessee Eastman Corp., Oak Ridge, Tenn.  
 $\text{TO}_3$  [ $\text{UO}_3$ ] REDUCTION AND CHLORINATION IN THE EXPERIMENTAL GLASS FLUIDIZER. R. S. Lowrie and J. V. Hubbard. Dec. 20, 1945. Decl. Dec. 20, 1955. 10p. Contract W-7401-eng-23. (C-5.350.6). \$3.30(ph OTS); \$2.40(mf OTS).

Uranium(VI) oxide was reduced to  $\text{UO}_2$  by reaction with  $\text{NH}_3$  at temperatures above 400°C. The  $\text{CCl}_4$  chlorination which was carried out in the temperature range, 350 to 400°C gave ~99% conversion. (C.W.H.)

### 3546 AECD-3965

Tennessee Eastman Corp., Oak Ridge, Tenn.  
THE REACTION OF HEXACHLOROPROPYLENE WITH METALLIC OXIDES. B. M. Pitt, E. L. Wagner, and A. J. Miller. Jan. 14, 1946. Decl. Dec. 21, 1955. 6p. Contract W-7401-eng-23. (C-2.355.3). \$1.80(ph OTS); \$1.80(mf OTS).

The action of refluxing hexachloropropylene was determined on 22 metallic oxides. It was found that anhydrous chlorides can be prepared with exceptional ease from the higher valent oxides of the V and VI group elements. (auth)

### 3547 ANL-4181

Argonne National Lab., Lemont, Ill.  
PREPARATION OF  $\text{UO}_3$ . Irving Sheft and Sherman Fried. July 13, 1948. Decl. Dec. 14, 1955. 8p. Contract W-31-109-eng-38. \$1.80(ph OTS); \$1.80(mf OTS).

The preparation of anhydrous  $\text{UO}_3$  by the oxidation of  $\text{U}_3\text{O}_8$  or amorphous  $\text{UO}_3$  in an oxygen atmosphere under high pressures is described. (C.W.H.)

### 3548 CC-3302

Chicago. Univ. Metallurgical Lab.  
RECOVERY OF  $\text{D}_2\text{O}$  AND  $\text{UO}_2\text{F}_2$  BY DISTILLATION. R. Fischer and A. Wattenberg. Oct. 10, 1945. Decl. Dec. 22, 1955. 9p. Contract W-7401-eng-37. \$1.80(ph OTS); \$1.80(mf OTS).

The purification and separation by distillation of  $\text{UO}_2\text{F}_2$  from  $\text{D}_2\text{O}$  is described. In the experiment which is discussed 2,129.6 lbs of  $\text{UO}_2\text{F}_2$  were dissolved in 6,605 lbs of  $\text{D}_2\text{O}$ . The apparent losses were 2.3 lbs of  $\text{UO}_2\text{F}_2$  and



64 lbs of  $D_2O$ . The average isotopic purity of the  $D_2O$  decreased during the distillation from 99.77% to 99.73%. The dissolved impurities were less than those present originally in the heavy water. (C.H.)

### 3549 CC-3336

Chicago, Univ. Metallurgical Lab.  
THE DETERMINATION OF THORIUM IN THORIUM-URANIUM ALLOYS, USING CUPFERRON. A. C. Eckert and R. W. Bane. DETERMINATION OF THORIUM IN URANIUM-THORIUM ALLOYS USING ION EXCHANGE. R. W. Bane. Nov. 23, 1945. Decl. Dec. 20, 1955. 12p. Contract W-7401-eng-37. \$3.30(ph OTS); \$2.40(mf OTS).

Two methods are described for the determination of Th in Th-U alloys low in Th. One method involves a cupferron precipitation in the presence of carbonate, used as buffer and complexing agent. The precipitate is weighed as thorium oxide after ignition. The second method involves an ion exchange separation of Th from U. The Th is then precipitated, ignited, and weighed in the conventional manner. (C.H.)

### 3550 CF-51-2-102

Oak Ridge National Lab., Tenn.  
THE RECOVERY OF URANIUM FROM NATURAL WATERS OF THE UNITED STATES. F. R. Bruce and D. E. Ferguson. Feb. 17, 1951. Decl. Dec. 19, 1955. 14p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

This report proposes that the natural waters of the United States be considered as an important potential source of U. It is believed that U can be economically recovered, by an anion exchange process, from fresh water containing as little as 10 parts of U per billion parts water. (auth)

### 3551 CF-51-11-44

Oak Ridge National Lab., Tenn.  
SOME OBSERVATIONS ON  $UO_3$  SLURRIES. Quarterly Report for Period August 10-November 10, 1951. J. O. Blomeke. Nov. 7, 1951. Decl. Dec. 19, 1955. 7p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Progress is reported in the development of aqueous  $UO_3$  slurries suitable for use at temperatures near 250°C and containing 100 to 300 g/l of U. Observation on the preparation of  $\alpha UO_3 \cdot H_2O$ ,  $\beta UO_3 \cdot H_2O$ ,  $\gamma UO_3 \cdot H_2O$ , and  $\delta UO_3 \cdot H_2O$  slurries are summarized. (C.H.)

### 3552 CF-51-12-67

Oak Ridge National Lab., Tenn.  
THE PREPARATION OF  $\gamma-UO_3 \cdot H_2O$  FROM URANYL NITRATE. J. O. Blomeke and J. L. Bamberg. Dec. 12, 1951. Decl. Dec. 15, 1955. 6p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

The preparation of  $\gamma-UO_3 \cdot H_2O$  crystals by precipitation of  $UO_4 \cdot 2H_2O$ , thermal decomposition of the peroxide in air to  $UO_3$ , and hydration of the trioxide was investigated. A flowsheet is presented for the production of 1-kg quantities of  $\gamma-UO_3 \cdot H_2O$ . (C.H.)

### 3553 CN-795

Ames Lab., Ames, Iowa.  
CHEMICAL RESEARCH—CHEMISTRY OF 94 (PLUTONIUM). Report for Month Ending July 15, 1943. Decl. Dec. 13, 1955. 5p. Contract [W-7405-eng-82]. (A-988). \$1.80(ph OTS); \$1.80(mf OTS).

The metallurgical separation of Pu from U metal was studied. In the process, the U is alloyed with Sn, the Sn-U alloy converted to hydride, the hydride dissolved in acid,

and the Pu separated from this solution. Removal of 93% of the Pu from 90% of the U has been achieved. (C.W.H.)

### 3554 K-315

Massachusetts Inst. of Tech., Oak Ridge, Tenn. Engineering Practice School.

USE OF ZINC NITRATE IN DECONTAMINATION SOLUTIONS. R. G. Stirling, T. A. Kirkham, and T. Cantwell. Sept. 25, 1948. Decl. Dec. 5, 1955. 26p. For Carbide and Carbon Chemicals Corp. K-25 Plant. Contract [W-7405-eng-26], Subcontract 70. \$4.80(ph OTS); \$2.70(mf OTS).

Investigation into the use of zinc nitrate in decontamination solutions showed that the replacement of calcium nitrate by zinc nitrate had no appreciable effect on decontamination properties, and that distribution coefficients obtained were satisfactory. Results from extraction column operation were inconclusive. (auth)

### 3555 K-421

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

STUDY OF THE SOLUBILITY OF URANYL AMMONIUM PHOSPHATE IN WATER AT 25°C. H. A. Bernhardt, J. H. Junkins, and S. S. Kirsliis. June 15, 1949. Decl. Dec. 27, 1955. 6p. Contract [W-7405-eng-26]. (KLO-112). \$1.80(ph OTS); \$1.80(mf OTS).

The solubility of uranyl ammonium phosphate tetrahydrate in water was determined at 25°C. The solubility was found to be 0.2  $\mu g/U/ml$ . (auth)

### 3556 K-482

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

THE ELECTRICAL RESISTIVITY AND DIELECTRIC CONSTANT OF LIQUID URANIUM HEXAFLUORIDE. J. F. Burns, H. S. McKown, and I. Asbury. Aug. 10, 1949. Decl. Dec. 27, 1955. 14p. Contract [W-7405-eng-26]. (KLO-138). \$3.30(ph OTS); \$2.40(mf OTS).

The value of the coefficient of electrical resistivity of liquid U hexafluoride has been found to be of the order of  $10^{14}$  ohm c. This value is not appreciably altered by the presence of hydrogen fluoride in amounts normally encountered in plant operations. The dielectric constant of liquid U hexafluoride has been found to be 2.57 at 500, 1000 and 2000 cycles per sec. (auth)

### 3557 K-719

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

X-RAY INSTRUMENT FOR MEASUREMENT OF URANIUM DEPOSITS IN PLANT EQUIPMENT. W. C. Taylor. Jan. 31, 1951. Decl. Dec. 27, 1955. 14p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

An x-ray instrument for transmission measurements was adapted for plant use in measuring small deposits of U in closed containers. It was found that with careful monitoring of all affecting variables, a change of 0.1 g/cm<sup>2</sup> of solid uranium could be detected in a closed container 8 ft in diameter with 7/16 in. steel walls. The backscatter radiation method of measuring deposits in closed containers was also investigated but the required sensitivity was not attainable because of the thickness of the container walls which would be encountered. (auth)

### 3558 KLX-35

Kellex Corp., New York

REPORT OF SHARPLES CENTRIFUGE TESTS. Job. 11.



Feb. 15, 1949. Decl. Dec. 7, 1955. 11p. Contract AT-30-1-GEN-169. \$1.80(ph OTS); \$1.80(mf OTS).

Results are presented of tests of two commercial centrifuges for the separation of precipitated U soda-salts from a representative sodium diuranate slurry sample. (C.H.)

### 3559 KLX-37

Kellex Corp., New York.

STUDIES OF ALKALINE PRECIPITATION OF URANIUM.

R. O. Hill and W. R. Peterson. Feb. 21, 1949. Decl.

Dec. 7, 1955. 28p. Contract AT-30-1-Gen-169. \$4.80 (ph OTS); \$2.70(mf OTS).

Results of a program of experimental work on the precipitation of U from nitrate solutions by means of sodium hydroxide, are presented. A study was made of the effect of various anions on the precipitation reaction and the extent to which phosphate and sulfate ions may be removed from the precipitates by water washing. Probable reactions occurring during precipitation are proposed and pH curves illustrating the various titrations are presented. (auth)

### 3560 M-2142

Du Pont de Nemours (E. I.) & Co. Jackson Lab.,  
Wilmington, Del.

CHAMBERS WORKS PROCESS FOR THE MANUFACTURE OF PERURANIC ACID (338.20). G. M. Richardson. Nov. 15, 1944. Decl. Dec. 5, 1955. 6p. Contract [W-7412-eng-2]. (BP-13). \$1.80(ph OTS); \$1.80(mf OTS).

Uranyl sulfate solution was clarified by filtration and precipitated as peruranic acid by means of hydrogen peroxide under controlled pH conditions. The precipitated peruranic acid was isolated in a filter press or centrifuge. The reaction is indicated by the equation:  $\text{UO}_2\text{SO}_4 + \text{H}_2\text{O}_2 \rightarrow \text{UO}_4 \cdot 2\text{H}_2\text{O} + \text{H}_2\text{SO}_4$ . The yield in this operation is about 99.0% of theory. About 1,911 lb of U were obtained per charge as a 45% paste of peruranic acid. (C.H.)

### 3561 MCW-103

Mallinckrodt Chemical Works, St. Louis.

TREATMENT OF URANIUM DIOXIDE WITH WATER

VAPOR AT HIGH TEMPERATURES. C. W. Kuhlman.

Aug. 13, 1948. Decl. Dec. 5, 1955. 5p. \$1.80(ph OTS); \$1.80(mf OTS).

Uranium tetrafluoride prepared by the 1948 Mallinckrodt plant process consistently contains a larger water soluble fraction than can be attributed to a reaction of the hydrogen fluoride with the amount of hexavalent U present in the dioxide. In experimental equipment this tendency has been even more marked, both here and at other plants. A possible explanation is the reaction  $\text{U}_3\text{O}_8 + 8 \text{HF} \rightarrow 2 \text{UO}_2\text{F}_2 + \text{UF}_4 + 4 \text{H}_2\text{O}$ . Evidence is presented to show that this increase in hexavalent U is not due to an oxidation reaction between  $\text{UO}_2$  and water. That is, the reaction  $3 \text{UO}_2 + 2 \text{H}_2\text{O} \rightarrow \text{U}_3\text{O}_8 + 2 \text{H}_2$  does not take place under the conditions studied. (auth)

### 3562 MCW-136

Mallinckrodt Chemical Works, St. Louis.

AN INVESTIGATION OF THE SAMPLING PROCEDURES

OF THE ORE ASSAY PROCEDURE. S. H. Houston and

J. R. Simmler. Sept. 1948. Decl. Dec. 5, 1955. 5p. \$1.80(ph OTS); \$1.80(mf OTS).

In contrast to regular sampling procedure, the entire sample was rolled 50 times and spread out as thin as possible. Small samples, from the surface of the ore to

the paper, were taken at evenly distributed points throughout the ore until a 50-g amount was collected. The whole 50-g sample was digested and a suitable aliquot taken for analysis. No essential difference was noted from the results of assays sampled by the 50-g procedure and the regular MCW sampling procedure. (L.M.T.)

### 3563 MITG-244

Massachusetts Inst. of Tech., Cambridge. Mineral Engineering Lab.

A SEARCH FOR SELECTIVE SOLVENTS OF URANIUM

NITRATE FROM OTHER NITRATES. William V. Ward.

Jan. 17, 1951. Decl. Dec. 6, 1955. 37p. Contract AT-30-1-gen-211. \$6.30(ph OTS); \$3.00(mf OTS).

The extractive properties of several organic solvents for the nitrates of U and its common impurities have been studied, employing a liquid-solid extraction technique. The effects of dilute  $\text{HNO}_3$  and  $\text{CCl}_4$  on the solvent properties were investigated. Physical properties of the solvents tested are tabulated. (C.W.H.)

### 3564 NYO-5164

Mallinckrodt Chemical Works, St. Louis.

A COMPARISON OF THE NITRIC ACID CONSUMPTION AND INSOLUBLE VALUES REPORTED BY THE LABORATORY WITH THOSE OBTAINED IN PILOT PLANT

OPERATION. Preliminary Report. S. H. Brown, A. J.

Cook, E. I. Miller, D. Smith, A. Tomoufoik, and J. H.

Yeager. Feb. 15, 1946. Decl. Dec. 2, 1955. 7p. Contract W-14-108-eng-8. \$1.80(ph OTS); \$1.80(mf OTS).

The present process for removing U from pitchblende involves the digesting of ore with  $\text{HNO}_3$  to dissolve the uranium compounds present. The resultant slurry is filtered on a rotary drum type filter. To obtain a high yield, it is necessary to add enough  $\text{HNO}_3$  to react with the oxides and other compounds present and have about a 1N excess of  $\text{HNO}_3$  after the reaction has been completed. In order to have a resultant slurry which is capable of being filtered on a rotary drum filter, the amount of solids in the slurry should be at least 250 g/l. In addition, slurries are unfilterable if no excess  $\text{HNO}_3$  is present. A test was devised in which a measured amount of  $\text{HNO}_3$  was allowed to react with a small quantity of ore and the excess  $\text{HNO}_3$  present after the reaction was titrated back with caustic to determine the quantity of acid consumed. The amount of 38° Baume  $\text{HNO}_3$  consumed per gram of ore was called  $\text{HNO}_3$  consumption and reported as such. A test was also devised in which a small amount of ore was tested with  $\text{HNO}_3$ , the resultant slurry filtered, and the dry cake weighed. The percentage of the ore found as dried cake was termed percent  $\text{HNO}_3$  insoluble. A comparison is made of the values obtained by the laboratory with those obtained in pilot-plant operation. (J.E.D.)

### 3565 RL-4.6.231

California. Univ., Berkeley. Radiation Lab.

ABSORPTION SPECTRA OF  $\text{TiCl}_4$  [ $\text{UCl}_4$ ] VAPOR. F. L.

Reynolds and P. H. Davidson. Nov. 30, 1943. Decl. Dec. 7, 1955. 6p. Contract W-7405-eng-48. (Chem.-S-231).

\$1.80(ph OTS); \$1.80(mf OTS).

The absorption spectrum of  $\text{TiCl}_4$  ( $\text{UCl}_4$ ) vapor was determined between wave lengths of 5000 and 2200 Å and at temperatures from 250 to 520°C in steps of 10° intervals for the principal purpose of ascertaining the proper wave length of light to use in a suggested method of measuring and controlling the vapor pressure of  $\text{TiCl}_4$  by optical instrumentation. (auth)



**3566 UCRL-196**

California. Univ., Berkeley. Radiation Lab.  
SPECIES OF URANIUM(VI) WITH TTA IN BENZENE AND  
PERCHLORIC ACID. THE CHARGE ON URANYL ION.  
William C. Orr. Sept. 1948. Decl. Dec. 8, 1955. 82p.  
Contract W-7405-eng-48. \$12.30(ph OTS); \$4.50(mf OTS).

The distribution coefficient of  $U^{6+}$  between dilute  $HClO_4$  and benzene solutions of TTA was determined. The data are interpreted to show that the principal species in the acid phase is a doubly charged ion,  $UO_2^{++}$ . Two previously unreported species of  $U^{6+}$  in the presence of TTA,  $UO_2K_2 \cdot HK$  in benzene and  $UO_2K^+$  in dilute acid, were found. The absorption spectra of all principal species are reported. (auth)

**3567 Y-63**

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.  
8-HYDROXYQUINOLINE COLORIMETRIC METHOD FOR THE DETERMINATION OF MICROGRAM QUANTITIES OF URANIUM. D. A. Lee and R. W. Woodard. Nov. 19, 1947. Decl. Dec. 7, 1955. 8p. \$1.80(ph OTS); \$1.80(mf OTS).

Microgram amounts of U can be determined quantitatively by measuring the absorbance of the chloroform extract of uranyl 8-hydroxyquinolate from neutral uranyl solutions at 380 m $\mu$ . (auth)

**3568 Y-87**

Carbide and Carbon Chemicals Co. Y-12 Plant, Oak Ridge, Tenn.  
R [ $U^{235}$ ] RECOVERY BY SCRAPING AND VACUUMING TECHNIQUES. J. M. Googin and M. C. Wiest. Dec. 19, 1947. Decl. Dec. 6, 1955. 8p. Contract [W-7405-eng-26.] \$1.80(ph OTS); \$1.80(mf OTS).

The feasibility of recovering  $U^{235}$  material by manually scraping and vacuuming the  $U^{235}$  carbons was investigated. Experimental results indicate that the overall recovery attainable by this method is about 5% higher as compared to the carbon-burning process. (auth)

**3569 Y-112**

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.  
CHLORINE ( $_{17}Cl^{36}$ ) TRACER STUDIES. PART I. URANIUM TRIOXIDE-HEXACHLOROPROPENE REACTION MECHANISM. PART II. EXCHANGE REACTIONS OF SEVERAL ORGANIC CHLORIDE-INORGANIC CHLORIDE SYSTEMS. D. A. Lee and R. W. Woodard. Jan. 12, 1948. Decl. Dec. 7, 1955. 18p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

Investigations of the reaction of  $UO_3$  with hexachloropropene indicate that the reaction product  $UCl_5$  undergoes rapid chlorine exchange with hexachloropropene. Several reactions involving the exchange of  $Cl_2$  between chloroform and inorganic chlorides are described. The synthesis of  $Cl^{36}$ -labeled  $CHCl_3$  is outlined. (C.W.H.)

**3570 Y-161**

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.  
PREPARATION AND PROPERTIES OF MOLTEN AND FUSED URANIUM TETRACHLORIDE. R. H. Adams and J. S. Reece. March 29, 1948. Decl. Dec. 6, 1955. 48p. Contract W-7405-eng-26. \$7.80(ph OTS); \$3.30(mf OTS).

Research and development studies involving the preparation of molten and fused  $UCl_4$  are reported. Methods of preparation of fused charges for track operation, and the

operating characteristics of these charges were examined. The corrosion effect of molten  $UCl_4$  was studied and the ability of various materials of construction to withstand attack are compared. Methods of melting  $UCl_4$  in carbon and glass containers for loading H-bottles with molten charge were studied. The application of a carbon-resistance heater for melting  $UCl_4$  was examined. Determinations of the specific gravity of fused  $UCl_4$  and of the electrical conductivity of molten  $UCl_4$  are discussed. An explanation of the development of stick-feed production methods and plans for further work are included. (auth)

**3571 Y-184**

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.  
EXCHANGE OF URANIUM BETWEEN  $U^{+2}$  AND  $UO_2^{+2}$  IN DILUTE ACID SOLUTION. R. W. Woodard, D. A. Lee, and J. S. Drury. June 21, 1948. Decl. Dec. 6, 1955. 25p. Contract W-7405-eng-26. \$4.80(ph OTS); \$2.70(mf OTS).

By the use of tracer technique it was found that under certain conditions an interchange of U atoms takes place between uranous,  $U^{+4}$ , and uranyl,  $UO_2^{+2}$ , ions. Quantitative experiments were carried out to find the effect of various factors on the rate of U interchange. The factors investigated were H ion concentration, temperature, and light. A mathematical treatment of the exchange process was made which conforms with experimental results. (auth)

**3572 Y-286**

Carbide and Carbon Chemicals Co. Y-12 Plant, Oak Ridge, Tenn.  
THE STUDY OF EVAPORATION OF ACID MACHINE WASH AND EXTRACTION OF URANIUM FROM THE CONCENTRATE WITH DIETHYL ETHER. A. D. Ryon and E. J. Lord. Nov. 12, 1948. Decl. Dec. 6, 1955. 11p. Contract W-7405-eng-26. \$3.30(ph OTS); \$2.40(mf OTS).

Acid machine wash can be evaporated to  $\frac{1}{10}$  of the original volume and, under proper conditions, the chloride and acid content of the concentrate are favorable for subsequent extraction of the U with ether. This permits a reduction in the size of extraction equipment and a saving in the amount of aluminum nitrate consumed. (auth)

**3573 Y-315**

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.  
SOLUBILITY OF URANYL AMMONIUM PHOSPHATE IN NITRIC ACID AND AMMONIUM NITRATE SOLUTIONS AS A FUNCTION OF TEMPERATURE. A. D. Ryon and D. W. Kuhn. Jan. 10, 1949. Decl. Dec. 6, 1955. 25p. Contract W-7405-Eng-26. \$4.80(ph OTS); \$2.70(mf OTS).

The solubility of  $UO_2NH_4PO_4 \cdot 3H_2O$  in 0.8M to 1.6M nitric acid increases rapidly as the temperature is increased from 0°C to about 80°C, at which point a transition to  $(UO_2)_3(P_2O_7)_2 \cdot 4H_2O$  occurs. The latter compound exhibits retrograde solubility as the temperature is increased above 80°C. The solubility of  $UO_2NH_4PO_4 \cdot 3H_2O$  was found to be linearly dependent upon the concentration of nitric acid. The presence of ammonium ion greatly represses the solubility at temperatures below the transition point. (auth)

**3574 Y-381**

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.  
SOLUBILITY OF URANYL AMMONIUM PHOSPHATE. A. D. Ryon and D. W. Kuhn. Apr. 1, 1949. Decl. Dec. 6,

1955. 22p. Contract W-7405-eng-26. \$3.30(ph OTS); \$2.40(mf OTS).

The solubility of uranyl ammonium phosphate,  $\text{UO}_2\text{NH}_4\text{PO}_4 \cdot 3\text{H}_2\text{O}$  in  $\text{NH}_4\text{NO}_3$ - $\text{HNO}_3$  solutions at 25 and 70°C was determined. The effects of excess  $\text{PO}_4^{3-}$  and  $\text{UO}_2^{2+}$  on the solubility were investigated. The solubility of uranyl phosphate  $(\text{UO}_2)_3(\text{PO}_4)_2 \cdot 4\text{H}_2\text{O}$  was determined at 96°C in various solvents. (C.W.H.)

**3575 Y-409**

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

DIRECT REDUCTION OF URANIUM HEXAFLUORIDE TO METALLIC URANIUM. D. E. Carpenter, C. P. Johnston, and C. D. Susano. May 16, 1949. Decl. Dec. 8, 1955.

5p. Contract W-7405-eng-26. \$1.80(ph OTS); \$1.80(mf OTS).

Exploratory tests are reported which indicate the feasibility of a one-step reduction process for the preparation of uranium metal from the hexafluoride by the action of calcium metal and iodine. (auth)

**3576 Y-478**

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

RATE OF EXCHANGE OF URANIUM BETWEEN URANOUS AND URANYL IONS IN AQUEOUS SOLUTION. D. G. Hill. Sept. 2, 1949. Decl. Dec. 6, 1955. 16p. Contract W-7405-Eng-26. \$3.30(ph OTS); \$2.40(mf OTS).

A mechanism is proposed for the reaction on the assumption that the rate measured is the rate of combination of  $\text{U}^{4+}$  and  $\text{UO}_2^{2+}$  to form  $\text{UO}_2^+$ . The measured dependence of the reaction rate upon acidity is that predicted by this mechanism. The reaction rate constant is calculated from the equilibrium constant and from the rate constant for the reverse reaction. Mathematical expressions are derived for comparing the results of other workers with those obtained here. It is suggested that an error resulting from the neglect of oxidation may explain some discrepancies in published results for the order of the reaction. (auth)

Refer also to abstracts 3444, 3446, 3496, and 3612.

## WASTE DISPOSAL

**3577 K-273**

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

A PROPOSAL FOR TAKING SAMPLE OF UNNEUTRALIZED WASTE. A. A. Abbatiello. Sept. 17, 1948. Decl. Dec. 27, 1955. 10p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

A method for taking a 100 ml sample of high-activity waste from a sampling station is proposed. Special precautions are necessary because of the high level of radiation. Equipment has been designed, built, and tested as far as practical. (auth)

**3578 K-316**

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

SLUDGE SAMPLING SYSTEM. A. A. Abbatiello. Dec. 9, 1948. Decl. Dec. 27, 1955. 16p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

A clamshell-type sludge sampler was designed and built at K-25 and used at Hanford to obtain specimens of radio-

active materials at predetermined depths from the metal waste tanks T-101, T-102 and T-103. Construction of the device and experience in its use at Hanford are described. Data on some of the physical and radiochemical properties of the samples obtained are tabulated. (auth)

**3579 K-416**

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

RECOVERY OF URANIUM FROM HANFORD WASTE BY PRECIPITATION AS URANIUM TETRAFLUORIDE AND SUBSEQUENT FLUORINATION. H. A. Bernhardt, S. Bernstein, and F. D. Rosen. June 10, 1949. Decl. Dec. 27, 1955. 16p. (KLO-107). \$3.30(ph OTS); \$2.40(mf OTS).

Uranium may be recovered from Hanford waste by precipitation as  $\text{UF}_4$  and subsequent fluorination to  $\text{UF}_6$ . This treatment has been used to obtain separation of all the fission products, except  $\text{Ru}^{106}$ , from the U. Activity due to the Ru was reduced to a value of 1 mc/kg of U. (auth)

**3580 Y-471**

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

URANIUM CONTENT OF SEWAGE SLUDGE; OAK RIDGE DISPOSAL PLANTS. L. J. Brady and C. D. Susano. Aug. 10, 1949. Decl. Dec. 6, 1955. 10p. Contract W-7405-Eng-26. \$1.80(ph OTS); \$1.80(mf OTS).

Results of tests are given on the U content of sludge which is produced at the Oak Ridge sewage disposal plants. The sludge produced at the West Plant is reported to contain 25 to 50 ppm of U, and that produced at the East Plant is reported to be of the order of 5 to 10 ppm. (auth)

## ENGINEERING

**3581 AECD-3901**

[Oak Ridge National Lab., Y-12 Area, Tenn.]

[OPERATING PROCESS FOR CANNING OF X-10 SLUGS.] [nd]. Decl. Dec. 8, 1955. 33p. Contract [W-7405-eng-26]. (Y-B58-1). \$6.30(ph OTS); \$3.00(mf OTS).

**3582 M-3845**

General Cable Corp., Bayonne, N. J.

DESIGN, PRODUCTION, AND TERMINATION OF POWER SUPPLY CABLE. E. Richman. [194?]. Decl. Nov. 28, 1955. 11p. \$3.30(ph OTS); \$2.40(mf OTS).

The power supply cables were designed with all elements having a concentric configuration. A varnished cambric insulation was used. The requirements, selection of insulation walls, and other design features are discussed. (J.E.D.)

**3583 M-3846**

Kerite Co., New York.

HIGH VOLTAGE KERITE CABLES FOR ELECTROMAGNETIC PLANT. Alan Standish Dana. [194?]. Decl. Nov. 28, 1955. 22p. \$4.80(ph OTS); \$2.70(mf OTS).

Many novel types of high voltage d-c cables were designed and manufactured in a very short period of time and an improved type of open terminals was developed. Considering the severity of the voltage stresses to which the cables were subjected, and the lack of information during the cable manufacturing period, the performance of both cables and terminals was quite satisfactory. When the ex-



traneous oscillations were reduced by suitable methods, the performance of cable and terminal was improved. (auth)

## HEAT TRANSFER AND FLUID FLOW

### 3584 A-381

National Bureau of Standards, [Washington, D. C.]  
HEAT TRANSFER COEFFICIENT FOR HYDROGEN  
FLOWING THROUGH A TUBE AT LOW TEMPERATURES.  
H. W. Woolley and F. G. Brickwedde. [194?]. Decl. Dec.  
8, 1955. 8p. \$1.80(ph OTS); \$1.80(mf OTS).

A study was made to determine the coefficient  $h$  in the equation  $dQ/dt = h\Delta\theta$  for the rate of flow,  $dQ/dt$ , of heat  $Q$  from the surface of a smooth, straight, cylindrical, metal tube to gaseous hydrogen at a different temperature  $\theta$  flowing through the tube at low temperatures under conditions of turbulent flow. (auth)

## MATERIALS TESTING

### 3585 M-4168

[Clinton Labs., Oak Ridge, Tenn.]  
PROCESS SOLUTION TRANSFER—TESTING OF STEAM  
AND AIR JETS. M. D. Peterson. Jan. 30, 1945. Decl.  
Nov. 29, 1955. 93p. \$15.30(ph OTS); \$5.40(mf OTS).

Seven steam and air jets of different designs were tested for performance in the transfer of process solutions. Data are presented on the design, test set-up, and characteristic curves of the jets tested. (C.H.)

## PUMPS

### 3586 K-101

Carbide and Carbon Chemicals Corp. [K-25 Plant], Oak Ridge, Tenn.

KINNEY PUMP OILS. C. B. Clifford, M. I. Lundin, and T. Shapiro. Dec. 4, 1947. Decl. Nov. 29, 1955. 8p.  
Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Performance tests were run in order to determine the relative costs and efficiency of Hi-Vac #3 (Vacuum Oil) and NS-2075 (Lube Oil) in the process area Kinney vacuum pumps. As a result of these tests it has been proven that the reclaimed Hi-Vac #3 now being used is directly responsible for a high percentage of the carbonization taking place in the pumps and materially contributes to their failure. Test data is presented to show that NS-2075 oil meets all operating requirements without carbonizing in the Kinney pumps. (auth)

### 3587 KAPL-130

Knolls Atomic Power Lab., Schenectady, N. Y.  
THEORY OF THE PUMP-MIX MIXER SETTLER. Chemical Engineering Laboratory Report No. 5. J. K. Davidson. Mar. 11, 1949. Decl. Dec. 5, 1955. 12p. Contract W-31-109-Eng-52. \$3.30(ph OTS); \$2.40(mf OTS).

Equations are derived which describe the hydraulic relations, the impeller characteristics, and the settling relations of the pump-mix mixer settler. (auth)

### 3588 KLX-1036

Kellex Corp., New York  
REPORT OF THE INSTRUMENT AND MECHANICAL DEVELOPMENT DEPARTMENT ON "CANNED" MOTORS

AND "CANNED" MAGNETIC COUPLINGS. Job 15. June 30, 1949. Decl. Dec. 6, 1955. 41p. Contract W-31-109-eng-52, Subcontract G-148. \$7.80(ph OTS); \$3.30(mf OTS).

The development of canned fractional-horsepower motors suitable for application to rotating pumps is reported. The development of these motors was part of a program to develop leakproof rotating pumps for transfer service in Redox plants. Such a motor consists of a stainless-steel-encased rotor running in a stainless-steel tube, separating the stator laminations and windings from the area about the rotor. Process fluids may be pumped through the rotor gap and the hollow rotor shaft. An integral unit of motor and pump may thus be obtained in which the pumped fluid flows through the pump. Four models of canned motors were fabricated and tested. Drawings and performance data are presented. Canned magnetic couplings suitable for driving rotary pumps or agitators were developed. Magnetic couplings consist of driven and driving members mounted on separate shafts and bearings. The driving member is coupled to a prime-mover and the driven member to the equipment. The two members are linked magnetically but not physically. A coupling that has a high starting and slipping torque in addition to good synchronous or near synchronous torque is required. Specifications, drawings, and test results are included for several models of induction couplings. (C.H.)

## MINERALOGY, METALLURGY, AND CERAMICS

### CERAMICS AND REFRACTORIES

#### 3589 AECD-3847

California Research and Development Co., Livermore, Calif.

CERAMIC-BASED MATERIALS FOR HIGH TEMPERATURE SERVICE. W. A. Bates. June 11, 1951. Decl. Dec. 3, 1955. 12p. (CRD-T2B-20). \$3.30(ph OTS); \$2.40(mf OTS).

The properties and fabrication of high-temperature refractory ceramics are discussed. Physical, chemical, and tensile properties of several ceramic materials are tabulated. (auth)

#### 3590 AECD-3951

Tennessee Eastman Corp., Oak Ridge, Tenn.

THE PREPARATION AND ANALYSIS OF THE CARBIDES OF Ta, Be, Zr, AND Th. E. W. Boulger, J. W. Sausville, and C. E. Larson. Sept. 19, 1945. Decl. Dec. 22, 1955. Contract W-7401-eng-23. (C-0.380.1). \$1.80(ph OTS); \$1.80(mf OTS).

Carbides of Th, Ta, Be, and Zr were prepared from the oxides of these metals by reaction with graphite in the induction furnace. Methods for the analysis of these compounds are given. (auth)

#### 3591 ANL-4177

Argonne National Lab., Lemont, Ill.

THE VOLATILIZATION OF BERYLLIA IN WATER VAPOR. M. G. Berkman and S. L. Simon. July 15,

1948. Decl. Dec. 14, 1955. 23p. Contract W-31-109-eng-38. \$4.80(ph OTS); \$2.70(mf OTS).

The effects of variation of temperature, steam pressure, mass flow rate and volume flow rate, BeO sample area, and vapor composition on the reaction rate of BeO with steam are summarized. (C.W.H.)

## CORROSION

### 3592 AECD-3896

[Tennessee Eastman Corp., Oak Ridge, Tenn.]

CORROSION TESTS ON AL ALLOYS. H. W. Winkler. Mar. 8, 1946. 8p. Decl. Dec. 15, 1955. Contract [W-7401-eng-23]. (CD-5560). \$3.30(ph OTS); \$2.40(mf OTS).

Results of corrosion tests on Al alloys in H<sub>2</sub>O containing Cl<sup>-</sup> indicate that the initial high corrosion rate decreases with time due to formation of a protective coating and that the Al corrosion rate is independent of the Cl<sup>-</sup> concentration. (C.W.H.)

### 3593 CN-2834

[Chicago. Univ. Metallurgical Lab.]

CORROSION TESTS. Progress Report for the Period November 15, 1944 to April 15, 1945. N. R. Glarum and W. H. Baldwin. June 20, 1945. Decl. Dec. 22, 1955. 11p. Contract W-7406-eng-39. \$3.30(ph OTS); \$2.40(mf OTS).

### 3594 HW-12552

[Hanford Works, Richland, Wash.]

CORROSION TESTS ON TANTALUM, HASTELLOY C AND DURIRON IN 234-5 PROJECT SOLUTIONS. J. B. Work and W. W. Koenig. Feb. 25, 1949. Decl. Dec. 12, 1955. 9p. [Contract W-31-109-eng-52]. \$3.30(ph OTS); \$2.40(mf OTS).

Static immersion and vapor suspension corrosion tests were conducted with Duriron, Hastelloy C, and Ta in hydriodic acid and synthetic 234-5 project process supernatant solution at room and elevated temperatures. Data are tabulated on the physical and mechanical characteristics of the metal and alloys, and on the composition and corrosive effects of the liquids. The 234-5 project process supernatant solution contained, among other things, 103 g/l of HI. (C.H.)

### 3595 HW-15829

Hanford Works, Richland, Wash.

CORROSION OF CONSTRUCTION MATERIALS IN 234-5 PROJECT SOLUTIONS. W. W. Koenig. Jan. 31, 1950. Decl. Dec. 7, 1955. 21p. Contract W-31-109-eng-52. \$3.30(ph OTS); \$2.40(mf OTS).

Laboratory corrosion studies of a number of materials to determine their suitability for use in construction equipment were made. Tantalum was the only metallic material completely satisfactory. Of the non-metallic materials, fluorothene and teflon showed satisfactory resistance. Laboratory tests are described and the results tabulated. (J.E.D.)

### 3596 HW-20765

Hanford Works, Richland, Wash.

CORROSION TESTS ON STAINLESS STEEL PLATE-WASTE METAL RECOVERY PROCESS. Kenneth L. Sanborn. Apr. 9, 1951. Decl. Dec. 7, 1955. 5p. Contract [W-31-109-Eng-52]. \$1.80(ph OTS); \$1.80(mc).

Significant improvement in the resistance of 347 stainless steel to boiling 65% HNO<sub>3</sub> was obtained by annealing for 4 hr at 1650°F, followed by a water quench. Less im-

provement was noted when the plate was annealed for ½ hr at 1975°F followed by air cooling. (K.S.)

### 3597 K-373

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

CORROSION OF VARIOUS METALS IN HYDROFLUORIC SULFURIC ACID SOLUTIONS OF SYNTHETIC HANFORD WASTE. H. A. Bernhardt, W. Davis, Jr., and J. R. Flanary. Mar. 18, 1949. Decl. Dec. 23, 1955. 20p. Contract [W-7405-eng-26]. (KLO-87). \$3.30(ph OTS); \$2.40(mf OTS).

The precipitation of uranium as uranium tetrafluoride from hydrofluoric-sulfuric acid solutions of Hanford waste as a method of uranium recovery has imposed the problem of determining the type of metal that can be used for reactors. Nickel, monel metal and four stainless steels have been tested for their resistance to corrosion by such acid solutions. Nickel and monel corrode at rates of 0.019 and 0.062 in./year. The former shows extensive flaking after about 20 days exposure. The stainless steels are quite corrosion resistant, varying in the ranges of 0.0032 in./year for 302 stainless, about 0.001 in./year for 304 and 316 stainless steels, and 0.00007 in./year for 25-12 (Nb stabilized) stainless steel. A comparison of observed corrosion rates with an estimated maximum allowable corrosion rate of 0.01 to 0.05 in./year suggests that all the stainless steels tested would meet this requirement while monel and Ni would not. Welding has little effect on the corrosion rates of 304 and 316 stainless steels, the only welded steels tested. (auth)

### 3598 M-4585

[Ames Lab., Ames, Iowa.]

CORROSION OF THORIUM AND RELATED MATERIALS. J. G. Feibig. [194?] Decl. Dec. 8, 1955. 28p. Contract [W-7405-eng-82]. Based on CC-2400 and CC-2715. \$4.80(ph OTS); \$2.70(mf OTS).

A study of the corrosion of Th and related materials in both air and water at various temperatures was made. By varying the method of treating the sample after exposure to water, it was found that values obtained by polishing the sample with either a non-metal-cutting cloth or an abrasive wheel were more reliable than those obtained by other methods. The effects of coupling, acid and salt solutions, and temperature were investigated. The coupling of Al and Th had little effect on the corrosion rate of Th but elevation of the temperature caused an increase in the rate of corrosion. Partial disintegration of the samples occurred in solutions containing acid and dissolved salts. Alloys of Th were found to be less resistant to corrosion than was the unalloyed metal. All alloys of uranium partially disintegrated during the tests. By exposing Th and a Th-Be alloy to air at various temperatures it was observed that both metals corroded appreciably, but the alloy was corroded to a lesser extent than was the unalloyed Th. A preferential corrosion of one phase of the alloy took place, but the phase most seriously attacked could not be identified. (auth)

### 3599 NYO-5129

Mallinckrodt Chemical Works, St. Louis.

CORROSION TESTS ON STEELS IN AAA [PITCHBLENDE] LIQUORS. E. T. Furnas. June 26, 1945. Decl. Dec. 7, 1955. 4p. \$1.80(ph OTS); \$1.80(mf OTS).

Samples of 304, 316, 317, and 347 stainless steel were immersed in acid leach precipitate solutions of pitchblende



ore. The four steels tested showed little difference in corrosion resistance to the liquor. (L.M.T.)

Refer also to abstract 3611.

## GEOLOGY AND MINERALOGY

### 3600 Y-414

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

A STATISTICAL ANALYSIS OF FACTORS AFFECTING THE FLUORIMETRIC DETERMINATION OF URANIUM IN OIL SHALE. Roberta L. McCutchen and C. D. Susano. May 26, 1949. Decl. Dec. 6, 1955. 19p. Contract W-7405-eng-26. \$3.30(ph OTS); \$2.40(mf OTS).

A statistical evaluation of the oil shale data indicated that neither particle size nor preliminary treatment of the sample was critical. A close control of the fluorimetric method of analysis by means of quality control charts is recommended to improve the precision and reliability of the test results. (auth)

## METALS AND METALLURGY

### 3601 A-2950

[Columbia Univ., New York].

HEAT TREATMENT OF A URANIUM-2% MOLYBDENUM ALLOY. J. E. Chaffey. May 1947. Decl. Dec. 3, 1955. 59p. Contract W-28-094-eng-10. \$7.80(ph OTS); \$3.30(mf OTS).

Experiments and data on the heat treatment of a U-2% Mo alloy are summarized. It is concluded that a eutectoid reaction exists at 600°C, that the fineness of the lamellar structure is affected by the cooling rate, that the  $\gamma$  phase may be retained at room temperatures by relatively slow quenches, that increased hardness and strength are due to precipitation from the supersaturated  $\gamma$  phase, that tempering treatments cause transformation from the  $\gamma$  to the  $\alpha$  phase, and that isothermal treatments did not produce any great change in microstructure except for very long times. (B.J.H.)

### 3602 AECD-3891

Oak Ridge National Lab., Tenn.

THE PROPERTIES OF ZIRCONIUM AND ITS POSSIBILITIES FOR THERMAL REACTORS. Harold B. Fairchild. Jan. 7, 1949. Decl. with deletions Jan. 5, 1956. 106p. Contract W-7405-eng-26. \$16.80(ph OTS); \$5.70(mf OTS).

Included are general discussions of the nuclear, physical, mechanical, and chemical properties of Zr, the production and fabrication of Zr, methods of analysis of Zr, and its corrosion resistance. (B.J.H.)

### 3603 AECD-3903

National Bureau of Standards, Washington, D. C.

QUARTERLY PROGRESS REPORT TO THE ATOMIC ENERGY COMMISSION FOR OCTOBER, NOVEMBER, AND DECEMBER 1954. April 1955. Decl. Dec. 7, 1955. 104p. (NBS-D-131). \$15.30(ph OTS); \$5.40(mf OTS).

Data or results are presented for the following studies: electrodeposition of Be-Mg alloys from ethereal solutions of MgAl hydride and Be borohydride; electrodeposition of Al-Mg alloys using tetrahydrofuran and diethyl ether as solvents; preparation of Be borohydride; synthe-

sis of phenylene sulfides, perfluoroaromatic compounds, and meta-linked polyphenyls; phase studies on Pt-U and Ru-U alloys of various compositions; preparation and testing of urania and thoria ceramics; physical properties of  $\text{UO}_2$  and  $\text{ThO}_2$ ; and elastic properties of Ni-bonded Te carbide specimens. (L.M.T.)

### 3604 AECD-3916

California Research and Development Co., Livermore, Calif.

MATERIALS HANDBOOK. PART III-LOW TIN ZIRCONIUM ALLOYS. H. Majors, Jr., R. T. Webster, G. E. Wendell, and R. H. Wallace. Jan. 29, 1953. Decl. Dec. 20, 1955. 33p. (CRD-A19-27(pt. 3)). \$6.30(ph OTS); \$3.00(mf OTS).

The mechanical and physical properties of low Sn-Zr alloys are outlined. (C.H.)

### 3605 AECD-3949

California Research and Development Co., Livermore, Calif.

MATERIALS HANDBOOK. PART V. PROPERTIES OF THORIUM. George E. Wendell, Harry Majors, Jr., R. H. Wallace, and R. T. Webster. May 6, 1953. Decl. Dec. 19, 1955. 78p. (CRD-A19-27(pt. 5); LWS-22514(pt. 5)). \$12.30(ph OTS); \$4.50(mf OTS).

Data are summarized on many mechanical and physical properties of Th. Most of the material in this report is also contained in Vol. 3 of the Reactor Handbook. (B.J.H.)

### 3606 CF-52-6-33

Oak Ridge National Lab., Tenn.

COLUMBIUM. H. Inouye. June 4, 1952. Decl. Dec. 16, 1955. 6p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Information obtained from a literature survey on the physical properties and gaseous reactions of Nb and the properties of Nb alloys is summarized. (B.J.H.)

### 3607 CF-54-3-171

Oak Ridge National Lab., Tenn.

THE DECONTAMINATION OF STAINLESS STEEL. Progress Report. D. O. Campbell. Mar. 16, 1954. Decl. Dec. 20, 1955. 30p. \$4.80(ph OTS); \$2.70(ph OTS).

The contamination on stainless steel exposed to Purex process solutions is predominantly Nb. Besides being the predominant initial contaminant, Nb appears to be the most difficult to remove. The rate of decontamination with time of treatment is reported for nitric acid, oxalic acid, Na hydroxide, Na tartrate in Na hydroxide, and a solution of Na tartrate, hydrogen peroxide, and Na hydroxide. Nitric acid is the least effective; alkaline tartrate peroxide is the most effective. The reagents decontaminate rapidly at first, but the rate drops to about 6% removal per day after several days. Contamination from dilutions of the Purex process waste solution follows the Freundlich adsorption isotherm relationship between the amount of radioactivity adsorbed and its concentration in the contamination solution. The addition of a fluoride solution of stable Nb and Zr to the contamination solution decreases the gamma contamination by decreasing that of Nb and Zr. Ruthenium then becomes relatively important. However, it is difficult to get Nb into solution with nitric acid alone. Hydrofluoric acid (3%) in nitric acid (20%) is the most effective decontamination reagent tested. It is also severely corrosive to stainless steel, although it does not produce intergranular corrosion or serious pitting.

Ultrasonic radiation of high enough intensity increases the rate of decontamination. (auth)

### 3608 CP-1837

[Chicago. Univ.] Metallurgical Lab.

SEALING OF HOLES IN ALUMINUM SHEET BY OXIDATION. S. Anderson and N. Goldowski. July 15, 1944.

Decl. Jan. 5, 1956. 30p. Contract W-7401-eng-37.

(A-2661). \$4.80(ph OTS); \$2.70(mf OTS).

An investigation is made of the conditions under which holes in Al may be expected to close by oxidation while in use in reactors. A brief theoretical discussion is given of the mechanism of oxidation of Al. Preliminary experimental results on plugging by chemical oxidation and by corrosion are summarized. It is concluded that under the most favorable conditions, only small holes may be sealed by oxidation processes. (B.J.H.)

### 3609 CT-1571

Battelle Memorial Inst., Columbus, Ohio.

METALLURGY OF TUBALLOY. Progress Report. Apr. 1, 1944. Decl. Dec. 13, 1955. 78p. Contract [W-7405-eng-92]. (A-2239) \$9.30(ph OTS); \$3.60(mf OTS).

Thermal expansion measurements between room temperature and 750°C were made on longitudinal specimens of  $\gamma$ - and  $\alpha$ -extruded metal, on transverse specimens of  $\gamma$ -extruded metal, and on biscuit metal. The inherent anisotropy of the metal and of the specimens is probably the cause of the peculiar dilatation behavior that is observed in the  $\alpha$  region and in the  $\alpha$ - $\beta$  transformation. The metal is characterized by a tendency for slow isothermal dilatation in the medium and high  $\alpha$  region and in the  $\alpha$ - $\beta$  transformation. Anisotropic properties of specimens account for much of the discordant expansion coefficient data. In a sample of commercially extruded and outgassed metal, the transverse expansion coefficient in the  $\alpha$  was initially high, while the longitudinal coefficient was low. Cycling through the lower transformation tended to bring the coefficients in the two directions together. A single heating-cooling cycle with this sample of extruded metal results in a permanent transverse expansion and longitudinal contraction. Nickel plate on Al has been found adequate to prevent alloying when hot Zn-dipping, 0.0005-in. thickness being resistant up to five minutes in the Zn bath at 450°C. When Cr is plated over Ni, the Cr apparently dissolves, but prevents alloying with the Ni. Anodizing in a  $H_3PO_4$  solution with HCl produces a surface which can be plated with adherent Ni deposits. Smoother deposits are obtained than with trichloroacetic acid. The production of Be reinforcements for end caps appears favorable using powder metal processes. Machining results in a high metal loss, and a rolled 50-50 Be-Al alloy does not appear promising. Measurements were made of the elastic constants of U at stresses up to 18,000 psi. Beyond this stress, yielding was too pronounced to warrant attempts to measure elasticity. It was found that Young's modulus varied from  $23.8 \times 10^6$  to  $13.9 \times 10^6$  psi and Poisson's ratio from 0.38 to 0.39 in one sample, while in another Young's modulus varied from  $27 \times 10^6$  to  $17.8 \times 10^6$  psi and Poisson's ratio from 0.38 to 0.43. Cracked bars occurring in extrusion are believed to be caused by high impurity content, particularly Fe, as a result of a study of samples obtained from Revere. Spun Al closures have been made for development work on welding for the final seal. (auth)

### 3610 LA-44

Los Alamos Scientific Lab., N. Mex.

URANIUM ALLOY DEVELOPMENT. PART II. A. U. Seybolt, C. S. Smith, L. B. Stark, and J. Koehl. Dec. 14, 1943. Decl. Dec. 13, 1955. 26p. Contract [W-7405-eng-36]. \$4.80(ph OTS); \$2.70(mf OTS).

The work on U-Mo alloys has been extended to cover a few more compositions. Maximum hardness is obtained with a molybdenum content of about 3%. A suitably heat-treated 3% alloy has a yield strength in compression of the order of 200,000 lb/in<sup>2</sup>. The carbon impurity (Ca 0.1%) has a pronounced hardening effect on uranium. Minimum hardness is obtained by furnace cooling, and maximum hardness on reheating for about 2 hr at 250 to 300°C, following a water quench from 900°C. (auth)

### 3611 MIT-1090

Massachusetts Inst. of Tech., Cambridge. Metallurgical Project.

CORROSION TESTING OF ZIRCONIUM IN WATER AT TEMPERATURES BELOW 600°F. D. S. Kneppel. Apr. 22, 1952. Decl. Dec. 8, 1955. 9p. Contract AT(30-1)-981. \$1.80(ph OTS); \$1.80(mf OTS).

Unalloyed graphite-melted zirconium has not corroded after seven to ten months in 350°F water. At this temperature higher amounts of impurities (e.g., N<sub>2</sub>, C, Ti, Al) can be tolerated than at 600°F. However, at 450°F it appears necessary to add a small amount of tin (e.g., 1 wt.%) or other alloying agent to guarantee corrosion resistance of graphite-melted zirconium. (auth)

### 3612 NYO-5225

Mallinckrodt Chemical Works, St. Louis.

THE RETENTION OF COPPER AND NICKEL IN THE PRECIPITATION OF URANYL AMMONIUM PHOSPHATE. Joseph R. Simmler. Apr. 6, 1948. Decl. Dec. 2, 1955. 6p. \$1.80(ph OTS); \$1.80(mf OTS).

As part of the systematic examination of the U assay procedure for ores used at the Mallinckrodt Chemical Works, it was desired to know how much Cu and Ni were retained by the U as it is precipitated as uranyl ammonium phosphate. The U is precipitated as the phosphate to separate it from most of the Ni and the bulk of the other constituents that are soluble as phosphates at a pH between 4 and 5. Colorimetric procedures are described for the determination of Cu and Ni retained by the U when precipitated as uranyl ammonium phosphate from ore samples. (C.H.)

### 3613 SO-3003

Rensselaer Polytechnic Inst., Troy, N. Y. Powder Metallurgy Lab.

ELECTRIC RESISTANCE SINTERING. A. B. Backensto, Jr., N. F. Hopson, and F. V. Lenel. Apr. 30, 1951. Decl. Dec. 6, 1955. 22p. Contract AT(30-3)-37. \$4.80(ph OTS); \$2.70(mf OTS).

Fe-Al compacts consisting of a core containing a mixture of Fe shot and Al powder surrounded by a case of pure Al powder have been extruded. Results are indicated by tabular extrusion data and photomicrographs. Sintered Zr compacts have been extruded in a resistance sintering machine using a tungsten wafer as an extrusion die. The resistance sintering technique has been applied to graphite in an attempt to produce graphite of a high density for use in nuclear reactors. (B.J.H.)



**3614** SO-3005

Rensselaer Polytechnic Inst., Troy, N. Y. Powder Metallurgy Lab.

## POWDER METALLURGY OF BERYLLIUM. A. B.

Backensto, Jr., N. F. Hopson, and F. V. Lenel. Dec. 31, 1951. Decl. Nov. 29, 1955. 29p. Contract AT(30-3)-53. \$4.80(ph OTS); \$2.70(mf OTS).

The production of composite bodies consisting of Be and another substance having greater ductility than Be is discussed. The KAPL method for copper plating metallic Be is outlined; it was found to be successful in plating Al powder (as a stand-in for Be) with coatings of Zn and Cu, but it is not applicable to Be powder when it is immersed in a zincate solution. Cu can be deposited on Be powder by electroplating in a Cu cyanide bath. It is also possible to deposit Cu on Be powder by displacement when the Be powder is immersed in a solution of Cu sulfate. No prior solvent cleaning or acid etching of the Be powder is necessary. The amount of Cu deposited can be controlled by controlling the concentration of the sulfate solution. Cu-coated Be powder containing 31% by weight of Cu was compacted and sintered by electrical resistance sintering. The compacts were quite strong but did not show any appreciable ductility in a transverse rupture test. The installation of equipment for safe handling of Be powder and also the health physics tests which were conducted to demonstrate its efficient functioning are described in an appendix. (J.E.D.)

**3615** WAPD-84

Westinghouse Electric Corp. Atomic Power Div., Pittsburgh.

EXPLOSIONS INVOLVING PICKLING OF ZIRCONIUM AND URANIUM ALLOYS. W. J. Hurford. May 28, 1953. Decl. Jan. 6, 1956. 18p. Contract AT-11-1-GEN-14. \$3.30(ph OTS); \$2.40(mf OTS).

Reports are submitted in a consolidated form by individual laboratories on explosion hazards involved in etching and pickling Zr and U and their alloys. (J.A.G.)

**PHYSICS****3616** AECD-3864

Westinghouse Electric Corp. Atomic Power Div., Pittsburgh.

THERMAL CONDUCTIVITY OF REACTOR FUEL ELEMENT MATERIALS. R. C. Westphal. June 23, 1954. Decl. Dec. 6, 1955. 4p. (WAPD-MM-538). \$1.80(ph OTS); \$1.80(mf OTS).

Thermal conductivities are presented for the following reactor fuel element materials: BeO-UO<sub>2</sub>, Cr-U, Mo-U, Th-U, Sn-Zr, U, UO<sub>2</sub>, U-Zr, and Zr. (C.W.H.)

**AEROSOLS****3617** MLM-188

Mound Lab., Miamisburg, Ohio.

THE APPLICATION OF TYPE 6 FILTER PAPER FOR THE REMOVAL OF AIRBORNE ALPHA EMITTING CONTAMINATION. R. Endebrook. Apr. 18, 1947. Decl. Dec. 7, 1955. 35p. Contract AT-33-1-GEN-53. \$6.30(ph OTS); \$3.00(mf OTS).

A determination was made of the efficiency of paper

filters in removing airborne  $\alpha$ -emitting contamination at various levels of contamination and of the operational pressure differentials of Type 6 filter paper. Other pertinent data were also collected. Results give the average efficiency of Type 6, single-thickness paper, for 21 runs as 94.5% and for 12 runs on double thickness paper as 96.6%. (B.J.H.)

**CRYSTALLOGRAPHY AND CRYSTAL STRUCTURE****3618** CC-2123

Chicago. Univ. Metallurgical Lab.

THIRD FORM OF BISMUTH PHOSPHATE—X-RAY STUDY. Rose C. L. Mooney. Sept. 7, 1944. Decl. Dec. 15, 1955. 9p. Contract [W-7401-eng-37]. \$1.80(ph OTS); \$1.80(mf OTS).

In addition to the hexagonal and the monoclinic bismuth phosphate precipitates, whose structures are now known, a third crystalline phase has been found to appear in BiPO<sub>4</sub> precipitates after extremely long digestion in concentrated nitric acid and oven drying at 800 to 1000°. Though very small single crystals of this component have been isolated, no crushed sample contained less than 30% of the  $\beta$  form. The cell size and symmetry of the crystal indicates that there are two bismuth atoms in the cell, and there is no evidence that the compound is not BiPO<sub>4</sub>. It is suggested that this may be a third form of BiPO<sub>4</sub>, stable over a short range of conditions, and tending to revert to the  $\beta$  form. (auth)

Refer also to abstract 3745.

**ELECTRICAL DISCHARGE****3619** AECD-3966

Tennessee Eastman Corp., Oak Ridge, Tenn.

THE METAL-DIELECTRIC JUNCTION OF HIGH-VOLTAGE INSULATORS IN VACUUM AND MAGNETIC FIELD. M. J. Kofoed, R. S. Alger, and D. Graves. Aug. 8, 1945. Decl. Dec. 20, 1955. 84p. (D-4,250,13). \$13.80(ph OTS); \$4.80(mf OTS).

The metal-dielectric junction of high-voltage insulators has been investigated in vacuum, with an applied magnetic field of 3400 gauss and with transient and steady state voltages. The junction at the negative end of the insulator is the source of electrical discharges which are associated with insulator failure. The positive junction has no evident role in insulator failure. The phenomena at the negative junction appear to be caused by the extremely high electric fields produced in the small gaps of the metal-dielectric contact. The phenomena do not depend upon gas pressure in the range of 0.1 to 1.0 $\mu$ , upon electrode material, or upon contact surface roughness. Metallizing the ceramic to reduce the contact gap serves only to move the discharge to the edge of the metallized region. The threshold voltage for the appearance of the discharge is raised by an increase in the uniformity of the electric field at the contact, or by a large decrease in the dielectric constant of the insulating ceramic. The negative junction phenomena were markedly reduced in intensity by shaping the electrode so that the edge of the metal-dielectric contact was in a region of very weak electric field. Practical electrode design, based upon these results, is discussed and will be the subject of future study. The threshold

voltage for the junction discharge increases with increasing over-all length of the insulator. However, the factors involved in this relationship are not as yet understood. (auth)

### 3620 BP-29

California. Univ., Berkeley. Radiation Lab.  
HIGH FREQUENCY INSULATOR AND VACUUM CAP  
BREAKDOWN TESTS. Fred Schmidt. Aug. 13, 1946.  
Decl. Nov. 28, 1955. 20p. Contract W-7405-eng-48.  
\$3.30(ph OTS); \$2.40(mf OTS).

The Zircon porcelain insulators used to support the 184-in. cyclotron dee and the stator ring of the rotary capacitor were tested at 13 Mc r-f voltage. The tests indicate that, with the insulator water and air cooling called for in the present capacitor designs, the maximum permissible continuous peak voltage appearing at the capacitor will lie between 55 and 65 kilovolts. R-f voltages greater than this will probably result in considerable heating of the insulators. It seems likely, however that gap breakdowns between the blades of the capacitor will present a lower limitation to the voltage than the insulators. (B.J.H.)

## INSTRUMENTS

### 3621 EAH-87

General Electric Co. General Engineering and Consulting Lab., Schenectady, N. Y.  
DESIGN PROPOSAL FOR ONE BINOCULAR AND ONE MONOCULAR PERISCOPE FOR HANFORD WORKS.  
G. R. Rede. Feb. 10, 1949. Decl. Nov. 28, 1955. With this is bound: BINOCULAR PERISCOPE DEVELOPMENT REPORT. Projects C-187 C and D. Norman F. Barnes. Oct. 29, 1948. (EAH-69). 78p. \$12.30 (ph OTS); \$4.50(mf OTS).

### 3622 MLM-291

Mound Lab., Miamisburg, Ohio.  
ELECTRONICS PROGRESS REPORT [FOR] FEBRUARY 1-28, 1949. Josef W. Heyd and Philip E. Ohmart. Apr. 25, 1949. Decl. Nov. 28, 1955. 36p. Contract AT-33-1-GEN-53. \$6.30(ph OTS); \$3.00(mf OTS).

A detailed study was made of the frequency response of the linear amplifier used with a boron-wall tube. Detailed views are given of the cathode follower circuit used for coupling the boron-wall tube to its linear amplifier. (B.J.H.)

## ISOTOPES

### 3623 ORNL-388

Oak Ridge National Lab., Tenn.  
PRODUCTION OF CARBON 14 FROM AMMONIUM NITRATE SOLUTION IN THE CHAIN REACTOR. A. H. Snell and L. D. Norris. Oct. 19, 1949. Decl. Dec. 7, 1955. 24p. Contract W-7405-eng-26. (deleted version: MDDC-726). \$4.80(ph OTS); \$2.70(mf OTS).

An apparatus is described for producing useable quantities of  $C^{14}$  by circulating  $NH_4NO_3$  solutions through the slow neutron flux of ORNL Graphite Reactor. The radioactive carbon, resulting from the  $N^{14}(n,p)C^{14}$  reaction, appears largely as CO and  $CO_2$  which are vented off and ultimately precipitated as  $BaCO_3$ . (K.S.)

## ISOTOPE SEPARATION

### 3624 A-3957

California. Univ., Berkeley. Radiation Lab.  
THE IONIC CENTRIFUGE. [Report for Period] January 1, 1942 to December 31, 1942. J. Slepian. Decl. Dec. 8, 1955. 45p. \$7.80(ph OTS); \$3.30(mf OTS).

Topics discussed include: an evaluation of the electromagnetic method of isotope separation; the production of ions at electrodes of a vacuum arc; the 1942 theory of the ionic centrifuge; the expected superiority of the ionic centrifuge over other electromagnetic devices; the experimental development of the arc ion source; experiments with the ionic centrifuge; isotope analyses made at Berkeley; results of thirty-three collection runs with the ionic centrifuge; and results from analyses of Berkeley samples made at Columbia. (C.H.)

### 3625 Y-164

Carbide and Carbon Chemicals Co. Y-12 Plant, Oak Ridge, Tenn.  
THE SEPARATION OF THE STABLE ISOTOPES OF THALLIUM. J. R. Patton and C. P. Keim. Apr. 14, 1948. Decl. Dec. 6, 1955. 35p. Contract W-7405-eng-26. \$6.30(ph OTS); \$3.00(mf OTS).

Thallium halides were used as a charge material for the calutron concentration of  $Th^{203}$  and  $Th^{206}$ . Preparation of the halides and calutron operations are described and illustrated. Data are presented on the chemical analysis, isotopic assays, and inventory quantities following the separation. (C.H.)

### 3626 Y-228

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.  
AN EVALUATION OF THE INTERNAL THERMAL FLOW METER FOR MEASURING  $UCl_4$  VAPOR IN THE BETA SOURCE UNIT. Donald Ross, Frank Neill, J. W. Morfitt, and Raymond Murray. Sept. 24, 1947. Decl. Dec. 7, 1955. 20p. Contract W-7405-eng-26. \$3.30 (ph OTS); \$2.40(mf OTS).

Because the mean free path of the gas particles is so large at the low operating pressures in a calutron beta source unit, no detectible flow of  $UCl_4$  vapor can be observed with the internal thermal flow meter. (auth)

### 3627 Y-287

Carbide and Carbon Chemicals Co. Y-12 Plant, Oak Ridge, Tenn.  
PREPARATION AND PROPERTIES OF URANIUM TETRACHLORIDE STICKS. Herbert S. Clinton and John S. Reece. Nov. 18, 1948. Decl. Dec. 6, 1955. 35p. Contract W-7405-eng-26. \$6.30(ph OTS); \$3.00(mf OTS).

Steps in development of a method of producing sticks of  $UCl_4$  suitable for experimental work on process efficiency are described, and a procedure which will produce satisfactory sticks in large enough numbers to be used for Beta Process experimental work is presented. The charge consumption rate of a calutron unit can not be determined until the unit is terminated. The average charge consumption rate can only be determined after termination, and it can not be determined for any specific period of operation. The Chemical Development Department accepted the responsibility to develop sticks of uranium tetrachloride (stick feed), for the purpose of determining the charge consumption rate for all periods of operation. Extruding



uranium tetrachloride through a small orifice, and casting were tried; casting proved to be a workable method. Casting was improved, and satisfactory sticks can now be produced by that method. (auth)

### 3628 Y-299

Carbide and Carbon Chemicals Co. Y-12 Plant, Oak Ridge, Tenn.

THE 100 KILOVOLT "G" SUPPLY. A. L. Boch. Mar. 4, 1948. Decl. Dec. 7, 1955. 11p. Contract W-7405-eng-26. \$1.80(ph OTS); \$1.80(mf OTS).

An experimental "G" supply of 100 kv was constructed for use in investigating high accelerating fields in the calutron. The system consists essentially of two "G" rectifiers operated in series with appropriate auxiliary equipment. Operation of the supply was entirely satisfactory under test conditions with a load of 0.4 amp at 100 kv. The regulation of the supply is 14%. (auth)

### 3629 Y-352

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

COMPARISON OF VARIOUS METHODS FOR THE REMOVAL OF URANIUM FROM CARBON SALVAGE. L. P. Twichell, P. B. Petretsky, R. D. Williams, and F. B. Waldrop. Feb. 11, 1949. Decl. Dec. 8, 1955. 21p. Contract W-7405-eng-26. \$4.80(ph OTS); \$2.70(mf OTS).

Experiments were conducted in which the removal of U by nitric acid leaching of ground C salvage was compared with the removal by similar leaching of residues. These residues were the resultant products of four types of pretreatment of C: muffling, burning in continuous carbon burner, heating in an insufficiency of air (coking), and reacting with steam at high temperature. Each sample was subjected to five stages of leaching after pretreatment. Results are presented to show the removal of U at each stage of leaching for the various methods of pretreatment and for different acid concentrations. Results are also given to show the portion of U from each calutron batch remaining in the final leached residue. (auth)

### 3630 Y-353

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

THE DEVELOPMENT OF EQUIPMENT FOR THE CONTINUOUS BURNING AND LEACHING OF GROUND CARBON. P. B. Petretsky, L. P. Twichell, R. D. Williams, and F. B. Waldrop. Apr. 14, 1949. Decl. Dec. 8, 1955. 20p. Contract W-7405-eng-26. \$3.30(ph OTS); \$2.40(mf OTS).

Equipment was developed for the continuous burning and leaching of ground C in order to recover U for the proposed cyclotron closed cycle beta process. The burning apparatus consisted of a vertical tube with a grate to support the C. An updraft of air was used to support combustion. The burning rate of the apparatus was 500 g of C per hr; combustion averaged over 98% complete. The leacher consisted of a heated nitric acid bath divided into four compartments through which ground C was pushed by rotating paddles. The acid flowed, by gravity, counter-current to the C. (auth)

### 3631 Y-544

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

ALTERNATE URANIUM CHARGES. Donald Ross and Raymond Murray. Sept. 20, 1948. Decl. Dec. 8, 1955.

14p. Contract W-7405-eng-26. \$3.30(ph OTS); \$2.40(mf OTS).

The performance characteristics of several U compounds as charge material for use in the calutron ion source explored included  $UCl_3$ ,  $UO_2Cl_2$ ,  $UBr_3$ ,  $UH_3$ , and  $UI_3$ . None of these was found to be any better than  $UCl_4$ . (auth)

### 3632 Y-652

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

THE EFFECT OF HIGH MAGNETIC FIELD ON ARC PHENOMENA AND CALUTRON PERFORMANCE. R. L. Murray and M. Wallis. Apr. 1, 1948. Decl. Dec. 8, 1955. 18p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

A calutron unit was operated at magnetic fields between 5000 and 15,000 oersteds. The effect of the field on a number of calutron parameters and performance characteristics was observed for a variety of charge materials. In particular, arc stability and calutron production efficiencies increased with increased magnetic fields, whereas total ion production and optimum slot widths decreased. (auth)

### 3633 Y-655

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

AN INDIRECTLY HEATED CATHODE FOR THE CALUTRON ION SOURCE. John J. Murphy and Raymond Murray. Dec. 15, 1948. Decl. Dec. 6, 1955. 11p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

An indirectly heated cathode for use in the calutron ion source has been successfully developed. Both Ta and W serve well as cathodes, and each has been tested with several charge materials. With a method of replacing cathodes during operation, extremely long runs may be possible, as filament life is no longer a problem. (auth)

Refer also to abstract 3568.

## MASS SPECTROGRAPHY

### 3634 AECD-3787

Tennessee Eastman Corp., Oak Ridge, Tenn.

DIAGNOSIS OF INSTABILITY OF AN ASSAY MASS SPECTROMETER. A. E. Cameron and G. P. Happ. Mar. 6, 1946. Decl. Nov. 28, 1955. 9p. Contract [W-7401-eng-23]. (B-6.460.11). \$1.80(ph OTS); \$1.80(mf OTS).

The type of trouble most frequently encountered in maintaining an assay mass spectrometer falls into the general classification of instability. A systematic procedure for locating the causes of instability is offered. (D.E.B.)

### 3635 KLX-1384

Vitro Corp. of America, New York.

PROJECT STATUS REPORT MASS SPECTROMETER DEVELOPMENT. Job 24-B2. P. A. Stowell. Dec. 30, 1952. Decl. Dec. 12, 1955. 22p. Contract AT(30-1)-850. \$4.80(ph OTS); \$2.70(mf OTS).

The program of modifying a commercial isotope ratio mass spectrometer to adapt it to rapid analysis of solid materials has been continued. Modification and improvements have resulted in an instrument which has successfully demonstrated rapid isotopic analyses of a variety of solid materials. (auth)

## MATHEMATICS

**3636** CP-2541

[Chicago, Univ. Metallurgical Lab.]

ON THE STATISTICS OF ROD WARPING. A. V. Martin and G. Young. Dec. 28, 1944. Decl. Dec. 13, 1955. 19p. Contract W-7401-eng-37. \$3.30(ph OTS); \$2.40(mf OTS).

The probability of exceeding assigned values of displacements or forces in simple rod models assembled from slugs picked at random is discussed, and some estimate for the statistical gain resulting from the use of shorter slugs is obtained. The probability that a rod with self-warping will touch the top of the tube appears great enough to justify a recommendation of the use of top ribs. (auth)

## MEASURING INSTRUMENTS AND TECHNIQUES

**3637** HW-27090

Hanford Works, Richland, Wash.

A METHOD FOR THE ANALYSIS OF RADIONUCLIDE MIXTURES USING A GAMMA-BETA SCINTILLATION SPECTROMETER. M. B. Leboeuf and R. E. Connally. Feb. 27, 1953. Decl. Dec. 7, 1955. 37p. Contract W-31-109-eng-52. \$6.30(ph OTS); \$3.00(mf OTS).

Beta and gamma scintillation detectors have been designed for use with an automatic recording, energy spectrometer. The application of this instrument to the analysis of mixtures of radionuclides which decay by gamma emission has been investigated. Integration of the area under the photoelectric peak of a differential pulse height scan obtained with the gamma energy spectrometer permits quantitative determination of each gamma emitter present. The substances present in three component mixtures have been identified, and, using the photopeak area method, the compositions of the mixtures have been determined with a precision of  $\pm 2.6\%$  (Std. Dev.) of the total gamma activity. A simplified method for the quantitative interpretation of scans is given, and its use for the determination of fission products in Redox and Metal Recovery plant streams is explained. Scans obtained on individual fission products and on a variety of such process samples are shown, and these illustrate the simplicity and wide range of applicability of the method. Analyses of solutions containing mixed gamma emitters were performed directly, without preliminary separations, in less than 40 minutes. It is believed that this instrumental method for the analysis of radionuclide mixtures will be of particular value to radiochemical process control because of its speed and reliability; in addition, it is expected to find application in any studies where mixed gamma emitters are used. (auth)

**3638** K-497

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

PROPORTIONAL FISSION NEUTRON COUNTERS. R. C. Rohr, E. R. Rohrer, and R. L. Macklin. Aug. 1, 1949. Decl. Dec. 27, 1955. 10p. Contract [W-7405-eng-26]. (KLO-143). \$1.80(ph OTS); \$1.80(mf OTS).

Some proportional fission neutron counters are described with information on methods of preparation and details of a circuit for a portable model. The portable instrument has an efficiency of .01% for neutrons from Po-Bc sources. (auth)

**3639** K-757

Carbide and Carbon Chemicals Co. K-25 Plant, Oak Ridge, Tenn.

PRELIMINARY REPORT ON A HIGH SENSITIVITY GAMMA PROBE FOR USE WITH THE SAMSON SURVEY METER. R. W. Schede. May 1, 1951. Decl. Dec. 27, 1955. 14p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

A high sensitivity gamma extension probe has been developed for use with the Samson survey meter. It has a sensitivity of 0.02 mr/hr full scale. The probe weighs 4.5 lb. and is 19 in. long by 2.5 in. in diameter. The primary function of this probe is to locate deposits of  $U^{235}$  in process equipment. (auth)

**3640** RL-4.6.271

[California, Univ., Berkeley. Radiation Lab.]

THE TECHNIQUE OF  $^{27}$  MEASUREMENT. M. B. Allen. July 17, 1944. Decl. Dec. 7, 1955. 5p. \$1.80(ph OTS); \$1.80(mf OTS).

Problems arising in the accurate measurement of the  $U^{237}$   $\beta$  radiation are considered in connection with the use of this isotope as a tracer. Preparation of samples with low self-absorption is outlined, as well as factors affected by the build-up of decay products. A satisfactory procedure is outlined for getting the  $U^{237}$  into solution, evaporating the solution on fine-grained filter paper, and counting with a thin-window bell jar counter. (K.S.)

## MOLECULAR PROPERTIES

**3641** MonT-164

[Clinton Labs., Oak Ridge, Tenn.]

THERMAL CONDUCTIVITIES OF PRESSED POWDERS. Final Report. B. Manowitz. Sept. 5, 1946. Decl. Nov. 28, 1955. 15p. Contract W-35-058-eng-71. \$3.30(ph OTS); \$2.40(mf OTS).

The thermal conductivities of lucite,  $Ca(NO_3)_2$ ,  $MgO$ , and  $Be_3N_2$  at 80°C have been measured. (C.W.H.)

## NEUTRONS

**3642** AECD-3848

California Research and Development Co., Livermore, Calif.

FUNDAMENTAL EQUATIONS DESCRIBING NEUTRON BEHAVIOR IN A CAVITY. D. B. Willmer and D. H. Imhoff. May 22, 1951. Decl. Dec. 5, 1955. 6p. (CRD-T4A-18). \$1.80(ph OTS); \$1.80(mf OTS).

**3643** AECD 3849

California Research and Development Co., Livermore, Calif.

ANGULAR DISTRIBUTION OF NEUTRONS FROM A PLANE SURFACE. W. H. Harker. May 24, 1951. Decl. Dec. 5, 1955. 8p. (CRD-T4A-23; LWS-23014). \$1.80(ph OTS); \$1.80(mf OTS).

In connection with the problem of neutron losses in reactor matrices, a theoretical determination is made of the angular distribution of the neutrons emitted from the interior faces of the lattice and the exterior faces of the target. The problem is investigated by considering the dimensions of the faces to be large compared to the total mean free path. (B.J.H.)

**3644** ANL-4475

Argonne National Lab., Lemont, Ill.

ESTIMATION OF NEUTRON SELF ABSORPTION IN  $RaCO_3$



SAMPLES. Robert Keyes. June 26, 1950. Decl. Jan. 5, 1956. 11p. Contract W-31-109-eng-38. \$1.80(ph OTS); \$1.80(mf OTS).

Approximate solutions of neutron self absorption for spherically and cylindrically symmetric geometries are obtained and evaluated numerically for the case of  $\text{RaCO}_3$  surrounded by Be. The results are given in both tabular and graphical form. (B.J.H.)

**3645** CF-52-2-55

Oak Ridge National Lab., Tenn.

NEUTRON SPECTRUM AND DOSE BUILDUP FACTOR IN WATER. H. P. Sleeper. Feb. 7, 1952. Decl. Dec. 15, 1955. 4p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Calculations of the neutron dose buildup factor in  $\text{H}_2\text{O}$  had previously been made assuming an energy-independent O removal cross section. The spectrum and buildup factor for fission neutrons in  $\text{H}_2\text{O}$  were also determined using an accurate cross section and angular dependence for H, and a smoothed-out O cross section, averaged over the narrow resonances and extrapolated to high energies by theory. The buildup factors obtained by the two methods are compared graphically as a function of distance from the source. Results show the neutron buildup factor calculated by the latter method to be about three times that calculated by the former. (B.J.H.)

**3646** CF-863

Chicago. Univ. Metallurgical Lab.

ACTIVATION OF FAST NEUTRON DETECTORS BY CYCLOTRON AND BY FISSION NEUTRONS. J. Ashkin and B. Feld. Apr. 1, 1943. Decl. Dec. 13, 1955. 6p. \$1.80(ph OTS); \$1.80(mf OTS).

The  $(n,\alpha)$ ,  $(n,p)$  and  $(n,\gamma)$  reactions in Al, P and I have been studied as fast neutron detectors, by investigating their activation in a pile of U metal. The cyclotron was used as a source of fast neutrons. Two categories of neutrons were considered: "fast," or those capable of exciting  $(n,\alpha)$  and  $(n,p)$  reactions, and "slow," or those exciting  $(n,\gamma)$  activities. The relative activations of these reactions were studied in different parts of the pile. For "fission" neutrons, the ratio of activities was found to be:  $\text{Al}(n,\alpha)/\text{Al}(n,p) \approx 0.4$ ;  $\text{Al}(n,p)/\text{P}(n,p) \approx 0.2$ ;  $\text{I}(n,\gamma)/\text{Al}(n,\alpha) \approx 7$ . These results suggest a method of comparing the fission spectrum with the energy spectrum of other sources by comparing activations of fast neutron detectors. Information on the way in which cyclotron neutrons come into equilibrium in the metal is gained by considering the variation in relative activation for different positions in the pile. Experimental "slow" to "fast" ratios are directly compared with the capture-to-fission ratios observed earlier. It is shown that the  $\text{P}(n,\gamma)/\text{P}(n,p)$  ratio behaves in somewhat the same fashion as uranium capture/fission. (auth)

**3647** CP-597

Chicago. Univ. Metallurgical Lab.

EFFECT OF TEMPERATURE ON THE RESONANCE ABSORPTION OF NEUTRONS BY URANIUM. Allan C. G. Mitchell, Louis Slotin, John Marshall, V. A. Nedzel, L. J. Brown, and John R. Pruett. Apr. 22, 1943. Decl. Dec. 14, 1955. 19p. Contract [W-7401-eng-37]. \$3.30(ph OTS); \$2.40(mf OTS).

The resonance absorption of uranium for neutrons has been investigated between 20 and 1000°C. Experiments

were carried out on both  $\text{UO}_2$ , density 4.63, and metal. The resonance activity was measured with respect to that of an iodine monitor at several different temperatures and the ratio of activity at temperature T to that at 20°C was determined. The increase in activity is 0.9% per 100°C for the oxide and 1.1% per 100°C for the metal. (auth)

**3648** LAMS-121

[Los Alamos Scientific Lab., N. Mex.]

NEUTRON EMISSION BY POLONIUM OXIDE LAYERS.

M. Argo and E. Teller. Aug. 8, 1944. Decl. Dec. 13, 1955. 7p. Contract [W-7405-eng-36]. \$1.80(ph OTS); \$1.80(mf OTS).

The number of neutrons produced by the  $\text{O}^{16}(\alpha,n)$  reaction in a thin and uniform polonium oxide layer is calculated. Factors due to oblique transmission and "effective"  $\alpha$ -particle range have been taken into account. Calculations for layer thicknesses between .01c/cm<sup>2</sup> and 1c/cm<sup>2</sup> indicate the number of neutrons emitted per curie of polonium alpha particles is approximately given by  $140 \times \text{C}^{.8}$  where C is the number of curies per square centimeter. (auth)

Refer also to abstracts 3725 and 3748.

NUCLEAR PHYSICS

**3649** AECD-3846

Argonne National Lab., Lemont, Ill.

PHYSICS DIVISION QUARTERLY REPORT FOR APRIL, MAY AND JUNE 1950. A. Wattenberg, F. C. Hoyt, and Louis A. Turner, eds. July 5, 1950. Decl. with deletions Dec. 12, 1955. 110p. Contract W-31-109-eng-38. \$16.80(ph OTS); \$5.70(mf OTS).

**3650** ANL-4076

Argonne National Lab., Lemont, Ill.

EXPERIMENTAL NUCLEAR PHYSICS DIVISION AND THEORETICAL NUCLEAR PHYSICS DIVISION REPORT FOR JULY, AUGUST AND SEPTEMBER. Oct. 13, 1947. Decl. Dec. 15, 1955. 105p. Contract W-31-109-eng-38. \$16.80(ph OTS); \$5.70(mf OTS).

**3651** ANL-4174

Argonne National Lab., Lemont, Ill.

EXPERIMENTAL NUCLEAR PHYSICS DIVISION REPORT FOR APRIL, MAY AND JUNE. July 6, 1948. Decl. Dec. 15, 1955. 74p. Contract W-31-109-eng-38. \$12.30(ph OTS); \$4.50(mf OTS).

Half life and energy measurements for  $\text{Hg}^{203,205}$   $\beta$  activity were made. The  $\gamma$  spectrum of  $\text{Au}^{198}$  was investigated and the results compared with previous findings. Yields of delayed neutrons from Pu fission were found to be independent of incident neutron energy. The low capture cross section for isotopes having 82 neutrons is explained on the basis of filled nuclear shells. Empirical data for the standard pile are given. Techniques and results of small angle neutron scattering measurements on crystalline substances are given. Circuitry for a new pile oscillator system is presented and its operation explained. Results of neutron absorption cross section measurements on C, Mg, Al, and La are summarized. Progress is reported on  $\gamma$ -ray cross-over transitions, neutron diffraction in liquids, and absolute thermal neutron flux measurements. Investigations of internal conversion in Br radiative capture are discussed. The existence of the 5.5-second W activity was verified. (D.E.B.)

**3652 ANL-4208**

Argonne National Lab., Lemont, Ill.

EXPERIMENTAL NUCLEAR PHYSICS DIVISION REPORT FOR JULY, AUGUST AND SEPTEMBER; THEORETICAL NUCLEAR PHYSICS DIVISION SUMMARY REPORT FOR APRIL THROUGH SEPTEMBER. Oct. 4, 1948. Decl. Dec. 14, 1955. 105p. Contract W-31-109-eng-38. \$16.80(ph OTS); \$5.70(mf OTS).

An end point of  $570 \pm 10$  kev and a half life of  $2.7 \pm 0.4 \times 10^6$  years was established for  $\text{Be}^{10}$ . Differences in  $\text{Be}^{10}$  and  $\text{C}^{10}$  decay are explained on the basis of a  $\text{C}^{10}$  decay to an excited state of  $\text{B}^{10}$ . A technique for making thin nylon film is given. Theoretical and experimental considerations of small-angle neutron scattering are reviewed. Results indicate that the hypothesis that scattering is caused by multiple refraction at domain boundaries is adequate, and may be useful in domain structure investigations. A single crystal of Pb was used in plotting the effect of crystal structure on neutron cross sections. Results of small-angle neutron scattering measurements indicate a definite correlation between particle size and scattering at low energies. The neutron scattering cross section for Co was determined using pile, epi-Cd, and sub-Cd neutrons. Studies in coincidence measurements, cross over transitions in  $\text{Br}^{82}$ ,  $\text{Sb}^{124}$ ,  $\text{Co}^{60}$ ,  $\text{Mn}^{56}$ ,  $\text{Cl}^{36}$ ; and internal conversions in Br were continued. A 29-sec activity for Pt and 5 and 40 sec. activities for Yb are reported. Eighteen isotopes are added to the list having no short life activities. The 19 sec. isomeric transition in Hf is shown as a means of determining the presence of this impurity in Zr. Statistical studies of the Monte Carlo procedure are reported. Expressions for the paramagnetic effects in neutron polarization in Fe are given, and methods for neutron polarization are reviewed. (D.E.B.)

**3653 ANL-4277**

Argonne National Lab., Lemont, Ill.

EXPERIMENTAL NUCLEAR PHYSICS DIVISION REPORT FOR JANUARY, FEBRUARY AND MARCH 1949. Apr. 4, 1949. Decl. Dec. 13, 1955. 82p. Contract W-31-109-eng-38. \$13.80(ph OTS); \$4.80(mf OTS).

The two indices of refraction for neutrons in iron were shown experimentally. These were in agreement with theoretical predictions. Tests of the Mayer theory of closed neutron shells were continued to 48- and 50-neutron nuclei. The design and operating characteristics of a fast neutron chopper are given. The  $\beta$  spectra of  $\text{Tl}^{204}$  and  $\text{Tb}^{160}$  are discussed. The Br recoil energy spectrum was plotted as a function of applied voltage. Measurements by the soap film technique will be made for comparison. The method of neutron activation analysis of meteorites is outlined and results of analyses for Au and Rh are reported. A neutron velocity selector design is described. A table of total neutron cross sections prepared from Co and Mn resonance scattering analysis is presented. Results of neutron absorption cross section measurements for 46 elements are reported. Equations for the relationship of the epi-Cd scattering cross section and the resonance scattering integral are given, and computed resonance integrals tabulated. The technique and results of a Cd capture  $\gamma$ -ray spectrum study with photographic plates are discussed. Results of  $\text{D}_2\text{O}$  slow neutron diffraction experiments are given, and the angular distribution of Be photoneutrons are plotted. (D.E.B.)

**3654 ANL-4323**

Argonne National Lab., Lemont, Ill.

EXPERIMENTAL NUCLEAR PHYSICS DIVISION AND THEORETICAL NUCLEAR PHYSICS DIVISION REPORT FOR APRIL, MAY AND JUNE 1949. July 5, 1949. Decl. Dec. 14, 1955. 71p. Contract W-31-109-eng-38. \$10.80(ph OTS); \$3.90(mf OTS).

The study of neutron polarization by reflection from magnetized mirrors was continued. Properties of Co which led to its substitution for Fe as the reflecting surface are discussed. The reaction  $e^- + \text{H}^1 \rightarrow n + \nu$  was employed in an attempt to estimate the contribution of neutrinos to the earth's heat. Results indicate a maximum of 4% of the earth's heat can be attributed to the sun's neutrinos. Chemical dissociation of compounds containing nuclei undergoing isomeric transition was investigated. The transition of 4.4-hour  $\text{Br}^{80}$  to -18 min  $\text{Br}^{80}$  in ethyl bromide is specifically treated.  $\text{U}^{238}$  effective neutron resonance integrals were found to be linear with the ratio of surface area to mass in normal U metal rods. Values of "a" and "b" in  $\Sigma = a + b s/m$  were 9.25 and 24.7 where  $\Sigma$  is the effective absorption integral, S the surface area ( $\text{cm}^2$ ), and m the mass (gm.). Results of neutron absorption cross section measurements on Na and Cr by Co and Mn detection are given. The method and results of neutron resonance width measurements on  $\text{Co}^{60}$ ,  $\text{Mn}^{56}$ , and  $\text{W}^{187}$  are discussed. Additional Cd-ratio measurements of activation integrals were made in the rabbit flux of CP-3. The data obtained from 26 isotopes are listed. Photographic plate studies of neutron capture gamma spectra were extended to Cl; results are graphed. Results of coincidence measurements with  $\text{Hf}^{181}$  are reviewed. The fast group equation for a two-group model is derived assuming that diffusion theory holds for neutrons of all energies. The integral equation for monochromatic neutron scattering is developed for machine evaluation. Laplace transforms are used to derive exact expressions for the Doppler effect when the capture cross section follows a Breit-Wigner one level formula, and in the case of several resonances. The cross section for self-indication is also evaluated. Isotope shifts in the He atomic spectrum are calculated. (D.E.B.)

**3655 ANL-4350**

Argonne National Lab., Lemont, Ill.

EXPERIMENTAL NUCLEAR PHYSICS DIVISION AND THEORETICAL NUCLEAR PHYSICS DIVISION. Quarterly Report [for] July, August, and September 1949. Oct. 10, 1949. Decl. Dec. 10, 1955. 97p. Contract W-31-109-eng-38. \$15.30(ph OTS); \$5.40(mf OTS).

Neutron cross sections for various elements at 115 and 300 ev are listed. A more thorough investigation was made of neutron resonances in Na, Cr, and V. Equations are given for resonance absorption using flat and resonance scattering detectors. Recently obtained Cd-ratio measurements are summarized. Resonance scattering data for inert gases and rare earths are also given. Preliminary results of the operation of the Van de Graaff are discussed. Work on the fast chopper is also reported. The neutron capture  $\gamma$  ray spectra of Fe and Al are shown. Data on the angular distribution of photoneutrons from deuterium at 2.76 Mev are given. A determination was made of slow and fast fluxes inside a U annulus bombarded by pile neutrons. Work was continued on the reflection of neutrons from ferromagnetic



mirrors. Neutron scattering curves for soda-lime-silica glass and fused quartz are given. The change in reactivity of the Argonne Heavy Water Reactor caused by placing various sizes of natural U inside a central Cd-covered thimble is reported. A general discussion is given on the nuclear shell model based on jj coupling, including discussions of spins, magnetic moments, excited states,  $\beta$  decay, and the magnitude of the spin-orbit coupling. Progress is reported on the solution of reactor problems by numerical methods. (B.J.H.)

### 3656 ANL-4437

Argonne National Lab., Lemont, Ill.

EXPERIMENTAL NUCLEAR PHYSICS DIVISION AND THEORETICAL NUCLEAR PHYSICS DIVISION REPORT FOR JANUARY, FEBRUARY AND MARCH 1950. A. Wattenberg and W. H. McCorkle, eds. Apr. 5, 1950. Decl. Dec. 13, 1955. 130p. Contract W-31-109-eng-38. \$19.80(ph OTS); \$6.30(mf OTS).

Neutron cross sections of Ru, Pd, and La<sup>139</sup> at 120 ev and 345 ev are reported. Evidence for the existence of a negative energy neutron resonance in Cl<sup>35</sup> is discussed. Measurements were made of the number of  $\gamma$  rays emitted in a neutron capture process for various nuclei and the dependence of this number on atomic number is discussed. Neutron scattering cross sections of the noble gases were measured. Measurements were made of the  $\beta$  radiation from Ho<sup>166</sup>, Er<sup>171</sup>, and In<sup>116</sup>, and the results are summarized. Total neutron cross sections of Co and Mn are given. Designs are given for the target assembly to be used for determining photodisintegration thresholds, and the  $(\gamma, n)$  thresholds of deuterium and Be are reported. Designs of a neutron beam collimator are also given. Coherent n-p scattering is discussed. Neutron capture  $\gamma$ -ray spectra for W and Hg are given, and these results are discussed. The neutron groups from the reaction Li<sup>7</sup> (p,n) Be<sup>7</sup> were studied. An experimental determination was made of the neutron flux depression in the neighborhood of a foil inside a standard graphite pile. Neutron activation cross sections are reported for various substances. Total neutron cross sections of tungsten isotopes are given. Circuit designs for a low noise preamplifier are given. The  $\beta$  spectrum of Hf<sup>181</sup> was investigated. Experiments on the conversion coefficients of 4.4-hr Br<sup>80m</sup> in isomeric transitions are described. The determination of charged 17-min Rb<sup>88</sup> ions resulting from the  $\beta$ -decay of 3-hr Kr<sup>88</sup> is discussed. The feasibility of neutron fuses for a nuclear reactor is studied. The numerical determination of fundamental modes is discussed in detail. The theory of spin-spin doublets in N<sup>15</sup> and O<sup>16</sup> is also discussed. A three-group method for obtaining the critical properties of heavy-water moderated reactors is also given. (B.J.H.)

### 3657 ANL-4602

Argonne National Lab., Lemont, Ill.

PHYSICS DIVISION REPORT FOR DECEMBER 1950, JANUARY AND FEBRUARY 1951. Mar. 5, 1951. Decl. Dec. 10, 1955. 62p. Contract W-31-109-eng-38. \$10.80 (ph OTS); \$3.90(mf OTS).

Neutron cross sections for various elements are tabulated. Data are given on the internal conversion of capture  $\gamma$  rays in Gd and Sm. Improvements are described for the CP-3 pile oscillator circuit. The coherent neutron scattering cross section of Hg was measured. Results of a study of the internal conversion electron spectra of Se and Sm isotopes are tabulated. Improvements made on the Van de

Graaff accelerator are discussed. The isomeric transition of Br<sup>80</sup> is also discussed. A procedure is described for the preparation of metallic Na<sup>24</sup> after pile irradiation of aluminum nitrate. Studies were made on the organic retention of I following radiative neutron capture. The condensation of Na<sup>24</sup> molecular beams on various metals was studied. Techniques are outlined for the determination of atmospheric krypton content. Preliminary results of x-ray studies of Zr fluorides are reported. A mathematical analysis was made of the field of the lens system of the linear accelerator. Axial asymmetry in the linear accelerator is also discussed. (B.J.H.)

### 3658 CP-1729

Chicago. Univ. Metallurgical Lab.

NUCLEAR PHYSICS DIVISION REPORT FOR MONTH ENDING MAY 25, 1944. PART I. June 2, 1944. Decl. Dec. 15, 1955. 49p. (A-2443). \$7.80(ph OTS); \$3.30 (mf OTS).

### 3659 CP-2568

[Clinton Labs., Oak Ridge, Tenn.]

PHYSICS SECTION MONTHLY REPORT FOR THE PERIOD ENDING JANUARY 31, 1945. Feb. 1, 1945. Decl. Dec. 14, 1955. 31p. Contract W-7405-eng-39. \$6.30(ph OTS); \$3.00(mf OTS).

### 3660 LWS-12019

California Research and Development Co., Livermore, Calif.

CROSS SECTIONS FOR THE FORMATION OF Na<sup>22</sup> FROM ALUMINUM BOMBARDED WITH PROTONS (0 TO 32.5 MEV). R. E. Batzel. July 18, 1951. Decl. Dec. 6, 1955. 5p. Contract AT(11-1)-74. \$1.80(ph OTS); \$1.80(mf OTS).

The variation of the cross section for the formation of Na<sup>22</sup> from Al with the energy of the bombarding proton was determined from 32.5 to 25 Mev, the apparent threshold of the reaction. Results are given in graphical form. (B.J.H.)

### 3661 MonP-356

Clinton Labs., Oak Ridge, Tenn.

FISSION RECOILS IN A VARIABLE DENSITY BODY. G. Young. Aug. 6, 1947. Decl. Dec. 9, 1955. 13p. Contract W-35-058-eng-71. \$3.30(ph OTS); \$2.40 (mf OTS).

Calculations are made for the distribution of heat production in a fissioning slab of variable density, and for the escape of recoil particles and energy from the slab. A result is also given for the heat production in the inner part of a not-too-small fissioning body of any shape. (auth)

### 3662 RL-28.5.117

[California. Univ., Berkeley. Radiation Lab.]

SUMMARY OF THE RESEARCH PROGRESS MEETING. R. K. Wakerling. Aug. 1, 1946. Decl. Nov. 28, 1955. 6p. Contract W-7405-eng-48. \$1.80(ph OTS); \$1.80(mf OTS).

Preliminary tests of the r-f system for the 184-in. cyclotron were made on a 1/4-scale model. The status of proton-proton scattering experiments at 15 Mev were reviewed. (B.J.H.)

### 3663 UCRL-116

California. Univ., Berkeley. Radiation Lab.

PHYSICS DIVISION QUARTERLY REPORT [FOR] FEBRUARY 1, 1948 TO MAY 1, 1948. June 30, 1948. Decl. Nov. 28, 1955. 78p. Contract W-7405-eng-48. \$12.30(ph OTS); \$4.50(mf OTS).

A determination was made of the angular distribution of

the protons scattered when 90-Mev neutrons impinge on a H-filled cloud chamber. Methods for the detection of mesons are discussed. Meson tracks initiating stars are shown. Mass distributions of mesons were found from ranges in emulsion. The status of n-p scattering calculations is reviewed. The cross section for the production of mesons by  $\alpha$  particles is also calculated. Measurements of the total n-p cross section, made at 90 and 38 Mev, are summarized. Designs are given for a refrigerated photo-multiplier unit used for the investigation of the characteristics of the scintillation counter. Voltage-gain characteristics of the 1P21 photomultiplier are included. The arrangement of a complete "counting unit" using anthracene scintillation counters is shown. Operation and development of the 184- and 60-in. cyclotrons are discussed. Operation of the synchrotron is briefly discussed. (B.J.H.)

### 3664 UCRL-130

California. Univ., Berkeley. Radiation Lab.  
RESEARCH PROGRESS MEETING, JUNE 3, 1948.  
Margaret Foss Folden. Decl. Nov. 28, 1953. 8p. Contract W-7405-eng-48. \$1.80(ph OTS); \$1.80(mf OTS).

Evidence for the existence of the heavy meson is discussed. Improvements in the background of the 184-inch cyclotron are also described. (B.J.H.)

## NUCLEAR PROPERTIES

### 3665 AECD-3994

Carbide and Carbon Chemicals Co., Y-12 Area, Oak Ridge, Tenn.

THE TEMPERATURE DEPENDENCE OF A CROSS-SECTION EXHIBITING A RESONANCE. R. K. Osborn. Nov. 17, 1952. Decl. Jan. 6, 1956. 5p. Contract W-7405-eng-26. (Y-F10-112). \$1.80(ph OTS); \$1.80(mf OTS).

The explicit energy and temperature dependence of a macroscopic cross section exhibiting a resonance is calculated, assuming a particular form for the microscopic cross section and that particles in the absorbing system are in a Maxwell-Boltzmann velocity distribution. (B.J.H.)

### 3666 CF-54-2-159

Oak Ridge National Lab., Tenn.

NUCLEAR CONSTANTS FOR  $\text{Pu}^{239}$  AT 250°C AND 300°C. P. N. Haubenreich. Feb. 16, 1954. Decl. Dec. 6, 1955. 8p. Contract W-7405-eng-26. \$1.80(ph OTS); \$1.80(mf OTS).

Information from BNL-170, BNL-170B, and BNL-221 were used to evaluate the nuclear constants for  $\text{Pu}^{239}$  at 250 and 300°C. Data are tabulated. (C.H.)

### 3667 LA-266

[Los Alamos Scientific Lab., N. Mex.]

ABSORPTION AND FISSION CROSS SECTIONS OF  $^{49}\text{Pu}^{239}$  IN THE NEUTRON ENERGY RANGE 0.01 ev TO 100 ev. E. E. Anderson, B. D. McDaniel, R. B. Sutton, and L. S. Lavatelli. Apr. 23, 1945. Decl. Dec. 14, 1955. 20p. Contract [W-7405-eng-36]. \$3.30(ph OTS); \$2.40(mf OTS).

Measurements have been made of the variation of the fission cross section of  $\text{Pu}^{239}$ ,  $\sigma_f$  with neutron energy for the region from 0.02 ev to 450 ev and of the variation of the absorption cross section,  $\sigma_a$ , in the region 0.01 ev to 50 ev. Neutron energies were determined by use of the slow-neutron velocity spectrometer. The fission and absorption cross section curves appear qualitatively to be quite similar. Three resonances were observed. One,

which has been previously reported is at 0.295 ev, a second at about 12 ev and a third at about 60 ev. The first two were observed both in fission and absorption, the third in fission only since the absorption data do not extend to high enough energy. The quantity  $1 + \alpha = \sigma_a / \sigma_f$  in the region between 0.0250 ev and 1 ev was computed from the measurements. It deviates from its value at 0.0250 ev by an amount between one and two times the estimated probable value. Since the estimation of the probable error is rather difficult it is not possible to say whether  $\alpha$  does or does not vary in this region. It was found impossible to fit the resonance at 0.295 ev with a Breit-Wigner one-level formula. The possible significance of this fact and of the behavior of  $1 + \alpha$  is discussed. (auth)

### 3668 M-2273

Columbia Univ., New York.

NEUTRON BEAM SPECTROMETER STUDIES OF NITROGEN. E. Melkonian, W. W. Havens, Jr., L. J. Rainwater. Aug. 8, 1947. Decl. Nov. 28, 1955. 7p. Contract AT-30-1-Gen-72. (DR-971). \$1.80(ph OTS); \$1.80(mf OTS).

Neutron cross sections for nitrogen at energies greater than 0.025 ev were estimated to be  $9.60 + 0.48 E^{-1/2}$  barns. The capture cross section for thermal neutrons is calculated to be 3.04 barns. (C.W.H.)

### 3669 M-2554

Columbia Univ., New York.

NEUTRON BEAM SPECTROMETER STUDIES OF OXYGEN. E. Melkonian, L. J. Rainwater, and W. W. Havens, Jr. Aug. 8, 1947. Decl. Nov. 28, 1955. 7p. Contract AT-30-1-GEN-72. (DR-972) \$1.80(ph OTS); \$1.80(mf OTS).

Neutron cross sections of oxygen at 0.04 ev and in the energy region, 10 to 100 ev were measured to be 4.1 and 3.68 barns, respectively. No resonance levels were found in the regions studied. (C.W.H.)

### 3670 M-2555

Columbia Univ., New York.

NEUTRON BEAM SPECTROMETER STUDIES OF ARGON. E. Melkonian, W. W. Havens, Jr., and L. J. Rainwater. Aug. 8, 1947. Decl. Nov. 28, 1955. 7p. Contract AT-30-1-GEN-72. (DR-973) \$1.80(ph OTS); \$1.80(mf OTS).

Neutron cross sections for argon at 0.04 ev were measured to be 1.25 barns. The capture cross section for thermal neutrons is estimated to be 0.78 barn. (C.W.H.)

### 3671 M-4576

Monsanto Chemical Co., Dayton, Ohio.

CALCULATIONS OF FUNDAMENTAL CONSTANTS AND CONVERSION FACTORS. 1947 VALUES. (Supplement to Information Report No. 37). R. A. Staniforth. Jan. 5, 1948. Decl. Dec. 8, 1955. 20p. \$3.30(ph OTS); \$2.40(mf OTS).

Included are calculations of the packing fractions of  $\text{Pb}^{206}$  and  $\text{Po}^{210}$ , the rest masses of  $\text{Pb}^{206}$  and the recoil fragments from Po disintegration, the energies of Po  $\alpha$  particles and the recoil fragments of Po disintegration, the gram atomic weights of  $\text{Po}^{210}$  and  $\text{Pb}^{208}$ . Conversion factors for units used in radioactivity are listed. (B.J.H.)

## NUCLEAR REACTORS

### 3672 AECD-3862

North American Aviation, Inc., Los Angeles.

IMPREGNATION OF BERYLLIUM OXIDE WITH URANIUM. M. C. Sanz and R. Randolph. Aug. 20, 1947. Decl. Dec. 5.



1955. 18p. (NAA-AL-228). \$3.30(ph OTS); \$2.40(mf OTS).

A method of impregnating porous beryllium oxide uniformly with  $UO_3$  has been developed. Physical and ceramic properties of beryllium oxide are tabulated. (C.W.H.)

**3673** AECD-3869

Clinton Labs., Oak Ridge, Tenn.

CHEMICAL STABILITY OF HIGH TEMPERATURE POWER PILE. S. L. Simon and J. V. Fitzgerald. Feb. 4, 1947.

Decl. Dec. 7, 1955. 16p. Contract [W-7405-eng-39].

(CL-SLS-1). \$3.30(ph OTS); \$2.40(mf OTS).

Free energies, heats and entropies of formation, vapor pressures, and melting points of compounds of U, Th, Nb, Fe, and C, and free energies at 1500°K of chemical reactions involving reactor constituents are tabulated. The possible chemical reactions in a sample reactor are discussed. (C.W.H.)

**3674** AECD-3931

Oak Ridge National Lab., Tenn.

ENERGY PER FISSION AND POWER OF THE BULK SHIELDING REACTOR. J. L. Meem, E. B. Johnson, and H. E. Hungerford. May 12, 1953. Decl. with deletions Dec. 22, 1955. 9p. Contract [W-7405-eng-26]. \$1.80 (ph OTS); \$1.80(mf OTS).

The energy per fission in the BSR was re-measured and the new value is given. Using this result and the re-calibration results of the ORNL Graphite Reactor, the absolute power may be determined within a few percent. A list of reports in which data should be corrected is given. (D.E.B.)

**3675** AECD-3971

Oak Ridge National Lab., Tenn.

SCALE-UP OF ALTERNATE HRT CORE. L. B. Lesem and P. H. Harley. May 7, 1954. Decl. with deletions Jan. 3, 1956. 6p. Contract [W-7405-eng-26]. \$1.80 (ph OTS); \$1.80(mf OTS).

In order to determine the factors involved in the scale-up of cores, several models were assembled and tested. Visual studies were made of dye and gas behavior in the sphere of the core, and the static pressure drop across the core was measured. (B.J.H.)

**3676** AECD-3989

Oak Ridge National Lab., Tenn.

MEASUREMENTS OF A  $B_4C$  AND  $H_2O$  SHIELD IN THE LID TANK—EXPERIMENT II. E. P. Blizard and C. E. Clifford. Dec. 15, 1950. Decl. with deletions Nov. 30, 1955. 19p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

The attenuation of neutrons and  $\gamma$  rays in solid  $B_4C$  of various thicknesses followed by  $H_2O$  containing 0.5% B by weight was measured in the Lid Tank. Complete results are given in both graphical and tabular form. (B.J.H.)

**3677** ANL-4428

Argonne National Lab., Lemont, Ill.

REACTOR ENGINEERING DIVISION QUARTERLY REPORT [FOR] DECEMBER 1, 1949 THROUGH FEBRUARY 28, 1950. W. P. Bigler. Mar. 17, 1950. Decl. Dec. 13, 1955. 25p. Contract W-31-109-eng-38. \$4.80(ph OTS); \$2.70(mf OTS).

Operation of the Argonne Heavy Water Reactor is summarized. Design characteristics of the Argonne Research Reactor are discussed. Diagrams are given of the reactor and of the apparatus for stopping the reactor.

Data on the effects of irradiation on the tensile strength and hardness of nickel bars are tabulated. (B.J.H.)

**3678** ANL-4487

Argonne National Lab., Lemont, Ill.

THE CALCULATION OF INDUCED GAMMA ACTIVITY IN COMMERCIAL MATERIALS. Paul J. Persiani. Aug. 8, 1950. Decl. Dec. 14, 1955. 34p. Contract W-31-109-eng-38. \$6.30(ph OTS); \$3.00(mf OTS).

In many materials it is possible to effect a considerable reduction in pile-induced gamma activity by decreasing the content of one or more impurity. However, there are many factors to consider before setting up preliminary specifications. Some of these factors are the period of irradiation required, the time after irradiation at which the material is to be handled, and the feasibility of decreasing the amount of an impurity. Gamma activity data are presented for some commercial materials that may be used in the Materials Testing Reactor. A summation of the activities of the more significant elements present in each material is made on a log-log plot. The plots serve to indicate the contribution of the "impurities" to the total activity of a material at a particular time of decay. (auth)

**3679** BNL-2393

Brookhaven National Lab., Upton, N. Y.

LIQUID FUEL REACTORS. (Reprint of Project Dynamo Report PD-32). J. Chernick. Aug. 25, 1953. Decl. Dec. 12, 1955. 11p. \$3.30(ph OTS); \$2.40(mf OTS).

The results of liquid fuel reactor studies are reported. The two reactor concepts most intensively studied are: a reactor core consisting of a solution of  $U^{233}$  in Bi, Be or graphite rods as moderator, and a blanket of  $ThF_4$  pellets; and a graphite structure with U-Pb-Sn slurry fuel separated from the  $Th_3Bi_5$  slurry coolant. Some problems of liquid fuel reactors are discussed, including the  $U^{233}$ -Th breeding cycle, the container problem, location of moderator rods, delayed neutron losses, and core geometry. (M.P.G.)

**3680** C-192

[Chicago. Univ. Metallurgical Lab.]

SOME PHYSICAL CONSTANTS IMPORTANT IN THE DESIGN OF AN ATOMIC POWER PLANT. T. M. Snyder and R. L. Kamm. [nd]. Decl. Dec. 12, 1955. 56p. Contract [W-7401-eng-37]. (A-230). \$9.30(ph OTS); \$3.60(mf OTS).

The determination of a number of physical constants, primarily those connected with the heat transfer in an atomic power plant has been carried out. The thermal conductivity of a number of U materials was investigated in order to determine from which the large amounts of heat generated could be most easily extracted. Uranium itself and its sintered carbide proved most promising with conductivities of .045 and .08 cal/cm sec deg respectively. The electrical conductivity of the metal was also measured and found to give a good Wiedemann Franz ratio using this value of the thermal conductivity. In the present design of a power plant, graphite would be used as a neutron damper and perhaps in construction of cooling fins or ducts. The conductivity is found to be .28 near room temperature for most samples and to decrease with increasing temperature. In addition the thermal conductivities of other materials of possible use in design of such a plant were determined. Experiments on thermal transfer coefficients between two conductors showed that they depend almost entirely on the type of contact established between the two materials.

The thermal coefficient of expansion, elastic constants and ultimate strength of U were measured to determine the conditions for rupture under differential thermal expansions. It was found that a cylinder would split when the temperature difference between its center and the outside was between 450° and 1400°C, depending on the sample of metal used. In conclusion, several other properties such as hardness, density, and machining properties are discussed. (auth)

**3681** CC-1383

[Chicago. Univ. Metallurgical Lab.]

CHEMICAL RESEARCH. THE HEAVY-WATER HOMOGENEOUS PILE: A REVIEW OF CHEMICAL RESEARCHES AND PROBLEMS. C. F. Hiskey. Feb. 28, 1944. Decl. Dec. 13, 1955. 85p. (A-2024) \$13.80(ph OTS); \$4.80(mf OTS).

A generalized review of the chemical problems and researches related principally to the heavy water homogeneous pile is presented herewith. This report covers researches performed principally by the Columbia Group who initiated the study. This report contains a chronological outline of the development, a discussion of some special topics whose significance is paramount in any slurry pile discussion, and finally an outline of important research problems remaining, roughly graded in order of their importance. No attempt was made to be either complete or detailed in the discussion. The emphasis was principally on furnishing a broad guide to those who may at some future date take up this work. (auth)

**3682** CE-805

Chicago. Univ. Metallurgical Lab.

GENERAL ENGINEERING DESIGN FEATURES OF THE PILE FOR A LIGHT WATER COOLED P-9 POWER PLANT. L. A. Ohlinger. July 16, 1943. Decl. Dec. 12, 1955. 33p. \$9.30(ph OTS); \$3.60(mf OTS).

This report presents and discusses some of the general engineering problems and details involved in the design of a light water cooled pile for a D<sub>2</sub>O power plant producing 50,000 Kw or better from about 10 tons of D<sub>2</sub>O moderator and 6 tons of metal. Drawings are included to show some designs and variations in both horizontal and vertical piles, with miscellaneous details developed. (auth)

**3683** CE-1132

[Chicago. Univ.] Metallurgical Lab.

DESIGN OF SEMI-WORKS, LIGHT-WATER-COOLED HETEROGENEOUS P-9 PILE. Terminal Report. Dec. 14, 1943. Decl. Dec. 14, 1955. 45p. Contract [W-7401-eng-37]. (A-1620). \$19.80(ph OTS); \$6.30(mf OTS).

This is a report of the work performed in finding and solving several problems, mainly of an engineering nature, attending the design of a light-water-cooled, heterogeneous D<sub>2</sub>O pile of semi-works size. Such problems as the feasibility of a thorium blanket, heat removal, cooling water and power requirements, shielding, physical layout of manifolding systems for the cooling water, rod centering and replacement, tube replacement, etc., were considered. The physics design requiring 10 metric tons of D<sub>2</sub>O and 6 tons of metal was used as a basis for the work. Allowable aluminum sheath temperature of 70°C, probable limit of cooling water velocity of 35 ft/sec, and optimum annulus dimensions for heat transfer (within the restrictions imposed by physics design) limit the plant power output to 50,000 Kw with cooling water available at 10°C. For Site X, the 35°C cooling water limits the power to 30,000

Kw. A cooling water piping system providing for individually controlled feed and exit lines is now recommended, because it provides needed flexibility of control and large savings in water and power requirements. The structural difficulties of providing individual control for 460 rods have been shown to be surmountable; detailed drawings and photographs of models are presented in the Appendix. Detailed drawings of satisfactory designs for rod and tube replacements are also included. Charts of the power output as limited by the temperature of the cooling water, the maximum allowable rod sheath temperature and the water flow rate are presented. "Boiling disease" can be eliminated if a pressure of 67 lb/in<sup>2</sup> is used on the inlet cooling water. The aluminum temperatures in the region of a rib may be as much as 25°C higher than the average metal temperature. A recycling helium gas system requiring 2 liters of catalyst, 100 ft<sup>2</sup> condenser area and 4 h.p. will serve to recombine the gases formed from the D<sub>2</sub>O. Individual feed of cooling water to each rod will result in 50% saving in total water required. In addition, recycle cooling water will save in raw water purification at the expense of an air cooling system or liquid-liquid heat exchanger system employing raw river water on one side. Requirements of cooling water after shutdown become relatively negligible after one day. The knowledge accumulated and designs presented in this report and CE-805 would permit fairly rapid detailing and construction of this type of pile. No particular difficulties have appeared for which solutions have not been found. (auth)

**3684** CE-1149

Chicago. Univ. [Metallurgical Lab.]

ENGINEERING INVESTIGATION OF P-9 HOMOGENEOUS PILE. Terminal Report. J. H. Chapin and F. R. Ward. Jan. 13, 1944. Decl. Dec. 15, 1955. 29p. Contract [W-7401-eng-37]. (A-1635). \$15.30(ph OTS); \$5.40(mf OTS).

The engineering design of a homogeneous, D<sub>2</sub>O-moderated, slurry reactor was investigated. It was found that, provided the proper pumps and heat exchangers can be provided, D<sub>2</sub>O utilizations of the order of 75,000 Kw/ton of D<sub>2</sub>O external to the reactor, may be obtained with equipment of sizes common in industry. It was also found that approximately 9,000 Kw/ton of D<sub>2</sub>O external to the pile can be removed from a reactor, discharging at 120°C, by a thermal syphon utilizing the thermal expansion of D<sub>2</sub>O. Recommendations for further studies are given. (B.J.H.)

**3685** CE-1150

[Chicago. Univ. Metallurgical Lab.]

THERMAL SYPHON FOR HEX P-9 PILE. G. F. Quinn. Jan. 10, 1944. Decl. Dec. 13, 1953. 13p. (A-1636) \$3.30(ph OTS); \$2.40(mf OTS).

The use of a D<sub>2</sub>O-moderated reactor in which UF<sub>6</sub> fuel would be circulated through the pile and through external heat exchangers by means of a thermal syphon is suggested. The quantities of power which might be dissipated in such a system and the price of this power in terms of tons of UF<sub>6</sub> are investigated. The large quantities of UF<sub>6</sub> required indicate that the use of such a system is not attractive. (B.J.H.)

**3686** CF-46-6-23

[Clinton Labs., Oak Ridge, Tenn.]

THE [HANFORD] TEST PILE. L. A. Ohlinger. [1946?] Decl. Dec. 21, 1955. 11p. (Z-12). \$3.30(ph OTS); \$2.40(mf OTS).



A very general description is given of the Hanford Test Reactor. (B.J.H.)

**3687** CF-47-4-34

Oak Ridge National Lab., Tenn.

RESEARCH PILE EXPERIMENTAL FACILITIES. J. T. Weills. Apr. 28, 1947. Decl. Dec. 7, 1955. 15p. Contract [W-7405-eng-26]. \$13.80(ph OTS); \$4.80(mf OTS).

Complete descriptions and blueprints are given of the ORNL Low Intensity Training Reactor (LITR) experimental facilities, including tubes for hydraulically actuated samples, tubes for pneumatically actuated samples, horizontal beam holes, etc. (B.J.H.)

**3688** CF-48-2-139

[Oak Ridge National Lab., Tenn.]

DESIGN OF SHIM-SAFETY RODS. D. Nicoll. Feb. 4, 1948. Decl. Dec. 15, 1955. 14p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

The shim-safety rods for the high flux pile have been designed to meet the specifications set by the Physics Division and the mechanical limitations imposed by the pile. The shim-safety rods have adequate strength and sufficient cooling capacity to enable them to perform their function. The drive mechanism is capable of lifting and lowering the rods at the rated speed of 0.2 cm per second without exceeding the permissible overtravel during reversal of direction. The magnetic coupling is designed to lift over a thousand lbs without exceeding a coil current of 200 ma; and to give a release time of less than 30 msec. The energy acquired during the dropping of the shim-safety rod will be dissipated by the shock absorber within six inches travel of the rod. (auth)

**3689** CF-49-11-48

Oak Ridge National Lab., Tenn.

ALTERNATE DESIGN OF HOMOGENEOUS PILE REACTOR CHAMBER. C. L. Segaser. Nov. 3, 1949. Decl. Jan. 6, 1956. 4p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

A schematic sketch is presented for a design of a homogeneous pile reactor chamber. The sketch merely shows the core-tank as it would be assembled in the pressure vessel. An explanation of the system is included. (C.H.)

**3690** CF-49-12-1

Oak Ridge National Lab., Tenn.

HEAT PRODUCTION IN THE BOTTOM THERMAL SHIELD OF THE MATERIALS TESTING REACTOR. R. B. Briggs. Dec. 1, 1949. Decl. Dec. 20, 1955. 11p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

Preliminary calculations are presented on the heat production and temperature distribution in the thermal shield which served as a basis for an initial design of the Materials Testing Reactor. (C.H.)

**3691** CF-49-12-18

Oak Ridge National Lab., Tenn.

MTR SHIELD SURVEY. REPORT NO. 3. G. Thornton. Dec. 5, 1949. Decl. Dec. 15, 1955. 25p. Contract [W-7405-eng-26]. \$4.80(ph OTS); \$2.70(mf OTS).

Equations are derived for the activity of delayed neutrons, photoneutrons,  $\gamma$  rays, and  $\beta$  rays after MTR shutdown. Calculated activities are tabulated. Calculations of the  $\gamma$  radiation from the active section after shutdown, of the  $\gamma$  radiation through the top plug during operation, and of shield requirements for protection against decay gammas are also included. (B.J.H.)

**3692** CF-49-12-30

Oak Ridge National Lab., Tenn.

MTR DESIGN REPORT ON THE EXPERIMENTAL SHIELDING FACILITY. W. E. Sholl. Dec. 8, 1949. Decl. Dec. 20, 1955. 20p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

Specifications are presented for a proposed design for an experimental shielding facility for the Materials Testing Reactor. The proposed design includes a water shield tank, a deep well storage pit, a shielding facility hole and associated watertight bulkhead, a shielding slab dolly, a converter plate, and necessary service facilities. The facilities are described and detailed drawings are included. (C.H.)

**3693** CF-49-12-48

Oak Ridge National Lab., Tenn.

DISCHARGE TIMES OF HOMOGENEOUS REACTOR PILOT MODEL REFLECTOR FLOWING THROUGH 2-INCH PIPE FROM PRESSURE TANK. C. L. Segaser. Dec. 9, 1949. Decl. Dec. 20, 1955. 12p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

One safety device proposed for control of the homogeneous pilot reactor consists of discharging the reflector by gravity flow through a quick-acting automatically-actuated safety valve into a storage tank presumably located immediately below the reactor. A visualized arrangement for such a tank is presented schematically. Calculations are presented on the discharge times of the reflector flowing through 2-in. pipe from the pressure tank. (C.H.)

**3694** CF-49-12-82

Oak Ridge National Lab., Tenn.

HOMOGENEOUS REACTOR PILOT PLANT DESIGN STUDY. C. L. Segaser. Dec. 19, 1949. Decl. Jan. 6, 1956. 3p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

A diagrammatic sketch is presented of an arrangement for a steam pressurizer, gas recombiner, and core-tank in the pressure shell of the Homogeneous Reactor Pilot Plant. Advantages of this arrangement are discussed briefly. (C.H.)

**3695** CF-49-12-83

Oak Ridge National Lab., Tenn.

XENON POISONING AT VARYING POWER LEVELS. J. A. Lane. Dec. 14, 1949. Decl. Dec. 20, 1955. 7p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Calculations are presented for estimating the effect of xenon poisoning as a function of power level for the Materials Testing Reactor. (C.H.)

**3696** CF-50-4-17

Oak Ridge National Lab., Tenn.

COOLING REQUIREMENTS AT REDUCED POWER LEVELS. J. A. Lane. Apr. 3, 1950. Decl. Dec. 21, 1955. 4p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Calculations are presented on the water flow required for active lattice cooling and Be cooling of the MTR at reduced power levels. (C.H.)

**3697** CF-50-4-148

Oak Ridge National Lab., Tenn.

LITERATURE SURVEY RE: BUBBLE FORMATION. R. H. Wilson. Apr. 27, 1950. Decl. Nov. 29, 1955. 5p. Contract W-7405-eng-26. \$1.80(ph OTS); \$1.80(mf OTS).

Bubble formation in a mock-up of the Homogeneous

Reactor Experiment core is discussed. A literature survey of bubble formation is included. 17 references. (C.H.)

**3698** CF-50-5-140

Oak Ridge National Lab., Tenn.

INTERIM REPORT OF NEUTRON AND GAMMA EXPERIMENTS ON THE MTR MOCK-UP. S. E. Beall, W. M. Breazeale, R. B. Briggs, A. D. Callihan, and W. H. Jordan. May 11, 1950. Decl. Jan. 5, 1956. 37p. Contract [W-7405-eng-26]. \$6.30(ph OTS); \$3.00(mf OTS).

The loading and the startup of the MTR mock-up are described. Criticality was attained Feb. 4, 1950 with 2020.4g of  $U^{235}$  in 13 fuel elements. The fuel elements with 2 safety rods were arranged in a slab 3 assemblies wide and 5 assemblies long. Beryllium pieces surrounded the fuel pieces. The arrangement is illustrated graphically. Neutron and  $\gamma$  flux measurements are described. The details of the physical arrangement of the experimental facilities and instrumentation are appended. Data from the measurements are presented graphically and results are compared with calculated data. (C.H.)

**3699** CF-50-9-139

Oak Ridge National Lab., Tenn.

HRE-SLOW FLUX IN THE SHIELD. H. L. F. Enlund. Sept. 25, 1950. Decl. Dec. 19, 1955. 4p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Slow neutron fluxes were calculated in two types of barytes concrete shielding for the Homogeneous Reactor Experiment, and results are given in graphical form. (B.J.H.)

**3700** CF-51-7-106

Oak Ridge National Lab., Tenn.

CRITICALITY OF HRE WITH LOW ENRICHMENT, HIGH CONCENTRATION  $UO_2SO_4$ -WATER SOLUTION. L. H. Thacker and H. T. Williams. July 23, 1951. Decl. Dec. 2, 1955. 2p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

**3701** CF-52-2-232

Oak Ridge National Lab., Tenn.

HYDRAULIC TESTS FOR THE MTR. R. B. Briggs. Feb. 28, 1952. Decl. Dec. 15, 1955. 23p. Contract [W-7405-eng-26]. \$4.80(ph OTS); \$2.70(mf OTS).

The cooling water pressure distribution in the active lattice and the reflector of the MTR were measured as a means of evaluating whether the coolant flows and pressure distribution prescribed by the design were attained. Results indicate that the pressure distribution and coolant flow are acceptable. Complete data are summarized. (B.J.H.)

**3702** CF-52-9-75

Oak Ridge National Lab., Tenn.

EFFECT OF POISONS ON THE CRITICALITY OF THE ISHR AT 250°C and 100°C. Chandler Barkeley and Melvin Tobias. Sept. 16, 1952. Decl. Dec. 19, 1955. 4p. \$1.80(ph OTS); \$1.80(mf OTS).

This effect was calculated from the standpoint of various assumed conditions of operation in terms of lowering of temperature which would be necessary to maintain criticality at the fuel enrichments corresponding to the stated temperatures at a concentration of 250g of U per liter of solution. Estimations for the poisons were made by incorporating the absorptions into previously made two-group calculations for a "clean" reactor. (L.M.T.)

**3703** CF-53-9-134

Oak Ridge National Lab., Tenn.

HRP DYNAMIC CORROSION STUDIES. Summary of Runs D2-9 Through D2-11. J. C. Griess and R. E. Wacker. Sept. 24, 1953. Decl. Dec. 20, 1955. 14p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

A series of runs were made in a loop in order to determine the effectiveness of a certain decontamination procedure for radiozirconium and radioniobium in the loop. Uranyl sulfate containing Zr and Nb was used to contaminate the loop. (B.J.H.)

**3704** CF-54-3-175

Oak Ridge National Lab., Tenn.

ESTIMATE OF SHIELDING REQUIREMENTS FOR THE HRT DUMP TANKS. C. L. Segaser. Mar. 16, 1954. Decl. Dec. 19, 1955. 7p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

An estimate has been made of the shielding requirements of a proposed dump tank arrangement for the HRT. The dose rate on the surface of the dump tank shield one day after a dump has been calculated as a function of shield thickness. It was found that  $3\frac{1}{2}$  ft. barytes concrete of density 3.5 g/cm<sup>3</sup> will reduce radiation dosage to 1 r/hr 24 hr after a shutdown when the reactor has been in operation for a long period of time. (M.P.G.)

**3705** CF-54-12-143

Oak Ridge National Lab., Tenn.

OPERATION OF HRT CHARCOAL BEDS AT 10 MW REACTOR POWER. I. Spiewak. Dec. 20, 1954. Decl. Dec. 20, 1955. 5p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

The use of the Homogeneous Reactor Experiment charcoal absorbers for gas disposal from the Homogeneous Reactor Test is described. Heating for the charcoal beds, based on 10 Mw reactor operation, and the maximum heating of the charcoal beds were calculated. Two possible dump situations were considered: the first in which the reactor is not operating at power and only oxygen is released, and the second where power operation has been in progress and considerable quantities of radiolytic gas are dumped. (C.H.)

**3706** CF-55-1-120

Oak Ridge National Lab., Tenn.

TWO-REGION THORIUM BREEDER-POWER REACTOR-PROGRESS REPORT NO. 3. M. Tobias and H. C. Claiborne. Jan. 19, 1955. Decl. Dec. 20, 1955. 5p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Calculations show that errors in estimates of two-group constants are of secondary economic importance in TBR power considerations. (C.W.H.)

**3707** CF-3341

Chicago. Univ. Metallurgical Lab.

WATER EFFECTS ON A BeO PILE. J. Ernest Wilkins, Jr. and F. L. Friedman. Nov. 14, 1945. Decl. Dec. 15, 1955. 10p. Contract W-7401-eng-37. \$1.80(ph OTS); \$1.80(mf OTS).

An investigation was made of the changes in reactivity of a BeO-moderated pile which would be caused by the condensation of various amounts of H<sub>2</sub>O. Complete results are given in both tabular and graphical form. (B.J.H.)

**3708** CP-499

[Chicago. Univ. Metallurgical Lab.]

RADIOACTIVITY OF THE COOLING WATER. E. P.



Wigner. Mar. 1, 1943. Decl. Jan. 4, 1956. 8p. Contract [W-7401-eng-37]. \$1.80(ph OTS); \$1.80(mf OTS).

The most important source of radioactivity at the exit manifold of the pile was found to be  $O^{18}$ , formed by neutron absorption in  $O^{18}$ . It was estimated that it would be safe to stay ~80 min daily close to the exit manifolds without any shield. Estimates are given for the radioactivities from other sources, both in the neighborhood and farther away from the pile. (auth)

### 3709 CP-1350

Chicago. Univ. Metallurgical Lab.  
PERIPHERAL PRODUCTION. J. Stephenson. Mar. 30, 1944. Decl. Dec. 14, 1955. 12p. Contract [W-7401-eng-37]. (A-1899). \$3.30(ph OTS); \$2.40(mf OTS).

The production of radioactive materials by absorption of neutrons escaping the reactor is discussed. Calculations of the efficiency with which the escape neutrons are utilized by the absorber and efficiency of the reflector are presented. (C.W.H.)

### 3710 CP-1456

Chicago. Univ. Metallurgical Lab.  
CALCULATIONS FOR SOME PILE SHAPES OF WHICH THE BOUNDARIES ARE PARTLY SPHERICAL. G. Young, F. H. Murray, and H. Castle. CHARACTERISTIC NUMBERS AND FUNCTIONS FOR REGIONS WHICH ARE APPROXIMATELY CYLINDRICAL OR SPHERICAL. F. H. Murray. Feb. 25, 1944. Decl. Dec. 13, 1955. 11p. (A-2043). \$3.30(ph OTS); \$2.40(mf OTS).

Some methods for calculating the k requirements of various shaped piles are indicated, with particular reference to the shape of the tank in the homogeneous plant. (auth)

### 3711 CP-1662

Chicago. Univ. Metallurgical Lab.  
ON THE BOUNDARY CONDITION BETWEEN TWO MULTIPLYING MEDIA. F. L. Friedman and E. P. Wigner. April 19, 1944. Decl. 13, 1955. 13p. \$3.30(ph OTS); \$2.40(mf OTS).

The transition region between two parts of a pile which have different compositions is investigated. In the case where the moderator is the same in both parts of the pile, it is found that the diffusion constant times thermal neutron density plus diffusion constant times fast neutron density satisfies the usual pile equations everywhere, right to the boundary. More complicated formulas apply in a more general case. (auth)

### 3712 CP-2907

[Chicago. Univ. Metallurgical Lab.]  
THEORY OF OSCILLATING ABSORBER IN A CHAIN REACTING PILE. A. Cahn, Jr., A. T. Monk, and A. M. Weinberg. Apr. 6, 1945. Decl. Dec. 15, 1955. 23p. Contract W-7401-eng-37. \$4.80(ph OTS); \$2.70(mf OTS).

The fluctuation in pile intensity caused by an oscillating point absorber is calculated. It is found that the nature of the response depends on the frequency of the impressed oscillation. If the frequency is high compared to the decay rate of the high harmonics, the response consists of a wave which is propagated away from the oscillator. If the frequency is low, the propagated wave character of the response disappears and the intensity of the whole pile tends to oscillate with the same phase. The amplitude of the response decreases with increasing frequency. (auth)

### 3713 CT-883

Chicago. Univ. Metallurgical Lab.  
TEMPERATURE DISTRIBUTION IN AN ALUMINUM SHEATH. Karl Cohen and Irving Kaplan. Aug. 2, 1943. Decl. Dec. 12, 1955. 20p. (A-1315). \$4.80(ph OTS); \$2.70(mf OTS).

The design of a water-cooled pile requires a U rod sheathed in aluminum and surrounded by an Al tube. Cooling water is to flow in the annular space between the two Al cylinders. In order to center the U rod, the design calls for ribs on the outer Al tube. A theoretical treatment is given for the problem of the temperature distribution on the surface of an Al sheath in the neighborhood of a rib. A general treatment is given as well as the solutions corresponding to two simple profiles of the heat transfer coefficient. The results indicate an appreciable temperature rise in the neighborhood of the rib. For a 35,000 kw pile, with a velocity of cooling water of 35 ft/sec., the temperature rise at the hot spot for a rod at the center of the pile may reach 30°C. For piles operating at higher energy output, or with lower velocities of the cooling water, the temperature rise will be considerably greater, and will effectively prevent the use of ribs. (auth)

### 3714 CT-969

Chicago. Univ. Metallurgical Lab.  
P-9 (HEAVY WATER) UTILIZATION IN SLURRY PILE COOLING SYSTEM. F. R. Ward and J. T. Weills. Oct. 5, 1943. Decl. Dec. 13, 1955. 32p. \$6.30(ph OTS); \$3.00(mf OTS).

Preliminary investigations were made on the problems of heat transfer and  $D_2O$  utilization in the cooling system of a 40-ton homogeneous reactor. The most satisfactory designs, from these viewpoints, are discussed. (B.J.H.)

### 3715 CT-1897

Michigan. Univ., Ann Arbor.  
SUPERSONIC TRANSMISSION MEASUREMENTS ON VARIOUS SAMPLES. Preliminary Report. F. A. Firestone and W. G. Langton. July 4, 1944. Decl. Dec. 13, 1955. 16p. (A-2663). \$3.30(ph OTS); \$2.40(mf OTS).

Supersonic transmission data were obtained for 22 sample slugs at 2.25 and 1.0 Mc. A one-inch square crystal was used for all measurements. The results of the tests are described in detail. (B.J.H.)

### 3716 HW-10940

Hanford Works, Richland, Wash.  
BORON STAINLESS STEEL FOR DROP RODS. A. C. Callen, Jr. and A. L. Heckman. Sept. 7, 1948. Decl. Dec. 28, 1955. 13p. Contract W-31-109-eng-52. \$3.30(ph OTS); \$2.40(mf OTS).

The corrosion resistance of the boron stainless steel and 347 stainless steel was found to be highly superior to the corrosion resistance of the boron steel being used. Examination of the microstructure showed the boron stainless steel to be similar to that of type 302 stainless except for the presence of the boron compounds distributed in the austenite matrix. The ultimate strength was raised 40 to 50% by the presence of boron, which also embrittled the material to a high degree. Impact results equivalent to those obtained for 18-8 stainless steel samples are possibly misleading. The machinability of the material is at a par with that of normal types of 18-8 stainless steel. Centrifugal casting produces an extremely sound metal

lacking in faults or porosity. The need of further investigation of the physical properties obtainable by annealing at higher temperatures is pointed out. (auth)

### 3717 IDO-16078

Phillips Petroleum Co. Atomic Energy Div., Idaho Falls, Idaho.

THERMAL NEUTRON FLUX DISTRIBUTION IN THE HORIZONTAL THROUGH FACILITY IN THE MATERIALS TESTING REACTOR. G. O. Bright. Mar. 27, 1953. Decl. Jan. 5, 1956. 26p. Contract AT(10-1)-205. \$4.80(ph OTS); \$2.70(mf OTS).

A thermal neutron flux survey has been made as part of a complete flux determination in the HT-1 facility. Indium foil measurements along the centerline of the facility have been made over a four foot length in the highest flux zone. A series of cobalt wire measurements has been made to show the variation in flux from top to bottom and from side to side in the facility. These measurements were made at two shim-safety rod positions in order to determine changes in the neutron flux between startup and shutdown conditions. (auth)

### 3718 KAPL-24

[Knolls Atomic Power Lab., Schenectady, N. Y.]

TWO-GROUP REPRESENTATION OF AN INTERMEDIATE PILE. L. Tonks and R. Ehrlich. Jan. 19, 1948. Decl. Dec. 5, 1955. 18p. Contract [W-31-109-Eng-52]. \$3.30 (ph OTS); \$2.40(mf OTS).

A two-group (2G) formulation of the intermediate pile problem has been worked out on a semi-theoretical basis. The coefficients in the equations are calculated as weighted mean cross-sections, the weighting being based on an exact multigroup (M-G) calculation. The transfer from upper to lower group is also based on this calculation. For rather substantial variations of pile structure and constitution from that of the M-G basis the 2G method yields changes in  $\nu_c$  which are 44 to 83% of those found by other M-G calculations. Better agreement is expected for smaller variations. (auth)

### 3719 KAPL-304

Knolls Atomic Power Lab., Schenectady, N. Y.

PERTURBATION THEORY FOR BOLTZMANN EQUATION. H. Brooks. Feb. 27, 1950. Decl. Dec. 5, 1955. 13p. Contract W-31-109-Eng-52. \$3.30(ph OTS); \$2.40(mf OTS).

A first order perturbation theory is developed for the rigorous Boltzmann formulation of the pile equation. The physical significance of the resulting formalism is discussed for some examples corresponding to actual experiments conducted in the Preliminary Pile Assembly. (auth)

### 3720 KAPL-527

Knolls Atomic Power Lab., Schenectady, N. Y.

PILE NEUTRON PHYSICS II; NUCLEAR ENGINEERING COURSE; 1948-1949. A. M. Anderson. Jan. 13, 1949. Decl. Dec. 6, 1955. 18p. \$3.30(ph OTS); \$2.40(mf OTS).

Course lecture notes are presented on the following subjects: method of calculation of the distance neutrons travel before absorption; consideration of a diffusion equation which accounts for the flux in any unit volume of an infinite medium wherein there is a distributed source of neutrons which is proportional to the flux at any point; neutron density for a bare spherical pile, a pile with an infinite reflector, a pile with a finite reflector breeding blanket, and near a boundary; consideration of neutron

density for cubical, spherical, and cylindrical geometry. (C.H.)

### 3721 KAPL-528

Knolls Atomic Power Lab., Schenectady, N. Y.

SLOWING DOWN THEORY; NUCLEAR ENGINEERING COURSE; 1948-1949. H. E. Stevens. Jan. 20, 1949. Decl. Dec. 6, 1955. 14p. \$3.30(ph OTS); \$2.40(mf OTS).

Lectures presented during a course in Nuclear Engineering cover the following subjects: application of a slowing down theory to the position and energy changes of neutrons as they lose energy by collision; slowing down density in an infinite medium without absorption, slowing down density with absorption, and slowing down equation in a homogeneous pile. (C.H.)

### 3722 KAPL-551

Knolls Atomic Power Lab., Schenectady, N. Y.

PILE CONTROL I; NUCLEAR ENGINEERING COURSE; 1948-1949. F. E. Crever. Jan. 27, 1949. Decl. Dec. 6, 1955. 8p. Contract [W-31-109-Eng-52]. \$1.80(ph OTS); \$1.80(mf OTS).

The theory of reactor control and reactivity is discussed. Equations for the determination of neutron buildup in reactors are included. (C.W.H.)

### 3723 KAPL-964

Knolls Atomic Power Lab., Schenectady, N. Y.

BLANKET FISSIONS IN PPA-11. J. A. Bistline, Jr. Jan. 1952. Decl. Dec. 5, 1955. 38p. Contract W-31-109-Eng-52. \$4.80(ph OTS); \$2.70(mf OTS).

The blanket fissions in Preliminary Pile Assembly 11 were investigated under the Intermediate Power Breeder Program at KAPL and found to be 12.5 and 8.9% of the total core fissions for  $U^{238}$  and  $U^{235}$ , respectively. The conversion ratio for this type of reactor was found to be 1.20. The results are compared with those from Preliminary Pile Assembly 5 and from a  $U^{235}$  reactor directly surrounded by a uranium blanket. The comparison shows that breeding is greatly favored where the fast fission spectrum falls directly on the natural uranium. (auth)

### 3724 LA-47

Los Alamos Scientific Lab., N. Mex.

CRITICAL SIZE AND MULTIPLICATION NUMBER FOR UNTAMPED RECTANGULAR BLOCK BY VARIATION METHOD. Paul Olum and R. R. Davis. Jan. 8, 1944. Decl. Dec. 16, 1955. 18p. Contract [W-7405-eng 36]. \$3.30(ph OTS); \$2.40(mf OTS).

Critical sizes and multiplication numbers for rectangular parallelepipeds of square cross section are calculated using the integral variation method and a one-velocity group theory. (B.J.H.)

### 3725 MonC-398

Oak Ridge National Lab., Tenn.

ACTIVATION MEASUREMENT OF THE C-NEUTRON FLUX IN THE CLINTON REACTOR. J. W. Jones, H. M. Clark, and R. T. Overman. Feb. 27, 1948. Decl. Dec. 8, 1955. 37p. Contract W-7405-eng-26. \$6.30(ph OTS); \$3.00(mf OTS).

Measurements of the C-neutron flux in the ORNL Graphite Reactor were carried out by activation of a series of elements: gold, silver, copper, manganese, aluminum, sodium, and indium. The activities were measured principally by a  $\gamma$  ion chamber. Activation of the elements was carried out both with and without Cd foil



covering. The flux was calculated by use of known cross sections and by comparison with the Clinton Standard Pile. The average of eighteen independent determinations yields a flux of  $0.57 \times 10^{12}$  n/cm<sup>2</sup>/sec ( $\pm 10\%$ ) at the pneumatic tube for the pile loading at the times of the experiments and a power level of 3600 kilowatts. From the pneumatic tube to center ratio which was also determined, the neutron density was calculated for the center. The value calculated was  $n = 1.28$  n/cm<sup>3</sup>/watt. By use of these flux figures the cross section for  $5.3\text{-}\gamma$  Co<sup>60</sup> has been determined. The variation of activation with power level and the time of leveling of activity immediately after a change in power level were also studied. (auth)

### 3726 MonP-428

[Clinton Labs., Oak Ridge, Tenn.]

DISTRIBUTION FUNCTIONS AND FISSION PRODUCT POISONING. G. Young and L. Noderer. Nov. 6, 1947. Decl. Dec. 8, 1955. 21p. Contract W-35-058-eng-71. \$4.80(ph OTS); \$2.70(mf OTS).

Estimates for poisoning are calculated from functions previously used in describing the statistical distribution in capture cross section of fission products and from a later study of the distribution of known thermal capture cross sections. (L.M.T.)

### 3727 MonP-434

[Clinton Labs., Oak Ridge, Tenn.]

CRITICAL CONDITIONS FOR A MULTIPLYING SLAB REACTOR WITH A NON-MULTIPLYING REFLECTOR OF FINITE THICKNESS. H. L. Garabedian. Nov. 19, 1947. Decl. Dec. 8, 1955. 30p. Contract W-35-058-eng-71. \$4.80(ph OTS); \$2.70(mf OTS).

The pile equation for a multiplying region surrounded by an infinite non-multiplying reflector having the same scattering properties as the active pile is formulated as an integral equation with a symmetric displacement kernel. A variational technique is applied for the determination of the critical multiplication constant. (C.H.)

### 3728 MonP-457

[Clinton Labs., Oak Ridge, Tenn.]

CRITICAL MASS NEEDED TO OVER-RIDE Xe. G. Young. Dec. 19, 1947. Decl. Dec. 5, 1955. 13p. Contract W-35-058-eng-71. \$3.30(ph OTS); \$2.40(mf OTS).

### 3729 ORNL-563

Oak Ridge National Lab., Tenn.

"GO-NO GO" PLATE SPACING GAGES FOR THE MATERIALS TESTING REACTOR FUEL ASSEMBLIES. F. Kerze and J. T. Howe. Jan. 3, 1950. Decl. Jan. 5, 1956. 8p. Contract W-7405-eng-26. \$1.80(ph OTS); \$1.80(mf OTS).

Two types of go-no go gages have been designed for the inspection of the deep, narrow interplate spacings of the Materials Testing Reactor fuel assemblies. One of these gages has been constructed and has proved satisfactory for the rapid inspection of these channels. (auth)

### 3730 ORNL-701

Oak Ridge National Lab., Tenn.

MOCK-UP DESIGN REPORT. W. R. Gall and D. J. Mallon. Oct. 27, 1949. Decl. Dec. 8, 1955. 137p. Contract [W-7405-eng-26]. \$22.80(ph OTS); \$7.20(mf OTS).

Design work done on the mock-up of the Materials Testing Reactor (MTR) is discussed in detail. Each detail is explained as to the basis for design and reasons for

particular solutions that were selected. The outline starts with the tanks and then takes each item from the top plug down through the grids and grid supports to the bottom of the tank. Calculations are not given in detail, but results are given and general methods used are explained. Alternate designs are briefly discussed in some cases so that it will be known what others were considered and what the reasons were for their elimination. The reflector and the control system have been covered only briefly without going into the same detail as for the mechanical design of the tank, grids, etc. Conceptual design of the reactor for the most part was complete before design of the mock-up started, so that this was primarily a detailing job. Where conception was required it related to mechanical details and not to the over-all picture of the arrangement of the reactor. (auth)

### 3731 TID-5048

Brookhaven National Lab., Upton, N. Y.

INITIAL EXPERIMENTS ON THE BROOKHAVEN REACTOR. [PART] I. J. Chernick. Mar. 7, 1949. Decl. Dec. 8, 1955. 3p. \$1.80(ph OTS); \$1.80(mf OTS).

Observations from an analysis of start-up data of the ORNL Graphite Reactor are presented for use in the design and interpretation of the initial experiments on the Brookhaven Reactor. (L.M.T.)

Refer also to abstracts 3636 and 3744.

## NUCLEAR TRANSFORMATION

### 3732 CF-45-2-1

Clinton Labs., Oak Ridge, Tenn.

RELATIVE AND ABSOLUTE YIELD FROM ANTIMONY AND LANTHANUM PHOTONEUTRON SOURCES. A. H. Snell. Feb. 6, 1945. Decl. Dec. 20, 1955. 6p. Contract [W-7405-eng-26]. \$1.80(ph OTS); \$1.80(mf OTS).

Preliminary data are tabulated on photoneutron yields of Be when irradiated by  $\gamma$  rays from Sb<sup>124</sup> and La<sup>140</sup>. The results show that for equivalent total  $\gamma$  strength, the Sb produces 47 times as many photoneutrons as the La, while for equivalent millicurie strength, the Sb produces 200 times as many photoneutrons as the La. (B.J.H.)

## PARTICLE ACCELERATORS

### 3733 AECD-3930

California Research and Development Co., Livermore, Calif.

STRUCTURAL TARGET DAMAGE ACCOMPANYING SUDDEN LOSS OF VACUUM. J. P. Frankel. Aug. 24, 1951. Decl. with deletions Dec. 20, 1955. 5p. \$1.80(ph OTS); \$1.80(mf OTS).

### 3734 AECD-3941

California Research and Development Co., Livermore, Calif.

TRANSIENT THERMAL STRESSES IN UNRESTRAINED FLAT PLATES AND THIN WALLED CYLINDRICAL TUBES. N. C. Ostrander. Aug. 6, 1951. Decl. Dec. 20, 1955. 7p. (CRD-T2B-47). \$1.80(ph OTS); \$1.80(mf OTS).

The magnitude of transient thermal stresses are calculated for the flat plates and thin-walled cylindrical tubes to be used as Materials Testing Accelerator targets. (B.J.H.)



**3735 M-3712**

[California. Univ., Berkeley. Radiation Lab.]

**184" CYCLOTRON DEUTERIUM ELECTROLYZER**

TESTS. Report No. 11. W. J. Stephan. Mar. 20, 1947.

Decl. Nov. 29, 1955. 9p. Contract [W-7405-eng-48].

\$1.80(ph OTS); \$1.80(mf OTS).

Several operational characteristics of the D<sub>2</sub> electrolyzer were investigated to determine the feasibility of using the electrolyzer with the 184-in. cyclotron. These characteristics included temperature variations, automatic cut-off, and electrode geometry. (C.W.H.)

**RADIATION ABSORPTION AND SCATTERING****3736 CP-1676**

Indiana. Univ., Bloomington.

**RESONANCE ABSORPTION OF URANIUM IN MIXTURES.**

Allan C. G. Mitchell, Leon J. Brown, John R. Pruett, and

Evar D. Nering. Mar. 31, 1944. Decl. Dec. 12, 1955.

14p. (A-2412). \$3.30(ph OTS); \$2.40(mf OTS).

Experiments were made on the neutron resonance absorption of U when admixed with various substances. The experiments were carried out in a graphite pile 60 in. by 56 in. situated near the probe of the Indiana University cyclotron. The experimental arrangements and technique are described. The container of U mixtures was located at a place in the cyclotron pile at which the resonance activity was comparable to that in the Argonne U-graphite pile. Measurements were made on UO<sub>2</sub>; several mixtures of UO<sub>2</sub> and C in the form of graphite; mixtures of sugar, used as a source of pure H, and UO<sub>2</sub>; slurries of UO<sub>2</sub> and H<sub>2</sub>O or D<sub>2</sub>O; and thin films containing U. Data are tabulated. (C.H.)

**3737 Y-389**

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

**MATERIALS TO RESIST ION BEAM EROSION.** W. L.

Ross. Apr. 15, 1949. Decl. Dec. 7, 1955. 22p. Contract

W-7405-eng-26. \$4.80(ph OTS); \$2.70(mf OTS).

A series of tests were made to find a material to resist calutron ion beam erosion. Various materials were exposed to ion beams and the amount of erosion compared to a standard, C-18 graphite. Extruded graphites (AGHT and ECA) were only slightly better than C-18. BN and CbC were as good as C-18 graphite. None of the materials were definitely superior to C-18. (auth)

Refer also to abstract 3676.

**RADIATION EFFECTS****3738 AECD-3928**

North American Aviation, Inc. Downey, Calif.

**RADIATION EFFECTS QUARTERLY PROGRESS REPORT**

[FOR] JANUARY - MARCH 1954. F. E. Faris, ed. Aug.

15, 1954. Decl. with deletions Dec. 9, 1955. 47p. Con-

tract AT-11-1-Gen-8. \$7.80(ph OTS); \$3.30(mf OTS).

A study is made of the thermal conductivity of graphite, and the temperature dependence of  $[T^3/K]$  is shown for various graphites. The thermal conductivity and electrical resistivity of several brom-graphite residue compounds were measured between 10 and 300°K. Thermal conductivity curves are given for neutron-irradiated and untreated samples. The field dependence of the Hall coefficient and the magnetoresistivity were determined from 5 to 15

kilogauss for a series of irradiated graphite samples.

Cyclotron irradiations of graphite targets were made at various temperatures in order to gain information on the nature of the processes responsible for annealing of radiation damage in the low-temperature region. Analyses of the release of stored energy during quasi-isothermal annealing of graphite are shown, and the data are summarized. The cyclotron irradiation of Th, U, and Au is briefly discussed. Tempering curves are given for both cold worked and cyclotron irradiated Th. The results of pulse annealing cyclotron-irradiated samples of Cu wire are shown graphically. The formation of colloidal particles during thermal annealing of crystals is also discussed. (B.J.H.)

**3739 MIT-1028**

Massachusetts Inst. of Tech., Cambridge.

**CONDUCTIVITY CHANGES IN DIELECTRICS DURING****2.5 MEV X-RADIATION.** F. C. Armistead, J. C.

Pennock, and L. W. Mead. Aug. 8, 1949. Decl. Dec. 7,

1955. 30p. (deleted version: AECD-2641). \$4.80

(ph OTS); \$2.70(mf OTS).

An apparatus has been designed and constructed to measure the effect of 2 to 3 Mev x rays on the volume conductivity of dielectric materials during the actual irradiation period and to determine the recovery characteristics following the end of irradiation. A description of the apparatus and results of conductivity measurements made on three different dielectrics are given in this report. A high intensity (2000 R per minute) x-ray beam was obtained with the use of a Van de Graaff generator. Current through the samples of dielectrics was measured with an FP-54 electrometer tube used in a Penick type bridge circuit. Two dielectrics showed an increase in conductivity during irradiation, followed by recovery after the x-ray beam was turned off. The dielectrics differed in the time factors for increase and recovery. For the third material, polystyrene, only an upper limit could be set to the conductivity during irradiation; namely,  $2 \times 10^{-17}$  (ohm-cm)<sup>-1</sup>. (auth)

**RADIOACTIVITY****3740 MonC-132**

[Clinton Labs., Oak Ridge, Tenn.]

**THE PRODUCTION AND MASS ASSIGNMENT OF A 90****DAY ACTIVITY IN ELEMENT 43.** Progress Report [for]

April 1 to June 15, 1946. E. E. Motta and G. E. Boyd.

July 15, 1946. Decl. Nov. 28, 1955. 20p. Contract W-

35-058-eng-71. \$3.30(ph OTS); \$2.40(mf OTS).

The growth of a daughter activity from three-day Ru<sup>97</sup> has been observed. It has been shown that this activity is an isotope of element 43, thus permitting its assignment to Tc<sup>97</sup>. The activity has a half life of approximately 90 days and its radiations consist largely of very soft electrons having a half thickness of 1.5 mg/cm<sup>2</sup> of aluminum. (auth)

**SHIELDING****3741 A-4047**

Iowa State Coll., Ames.

**RADIATION SHIELDS AND THEIR FABRICATION.** W.



Calderwood and C. F. Grey. Dec. 1945. Decl. Dec. 14, 1955. 17p. \$3.30(ph OTS); \$2.40(mf OTS).

A satisfactory sillimanite insulation-radiation shield was developed for use in the casting of U that could be easily fabricated and easily assembled and disassembled. For other high temperature experiments, an alundum cement insulation-radiation shield was developed which was satisfactory for continuous use up to 1800°C. (auth)

### 3742 AECD-3984

Oak Ridge National Lab., Tenn.

#### MEASUREMENTS OF AN IRON AND BORATED WATER SHIELD IN THE LID TANK—EXPERIMENT 10. E. P.

Blizard and C. E. Clifford. Dec. 14, 1950. Decl. with deletions Dec. 12, 1955. 24p. Contract [W-7405-eng-26]. \$4.80(ph OTS); \$2.70(mf OTS).

Measurements were made in a shield mockup consisting of various numbers of Fe plates followed by a layer of varying thicknesses of  $B_4C$  and a region of borated  $H_2O$ . Thermal and fast neutron and  $\gamma$  measurements were taken in the water behind the iron. Results are given in both tabular and graphical form. (B.J.H.)

### 3743 BNL-2158

Brookhaven National Lab., Upton, N. Y.

#### EFFECT OF SPHERICAL VOIDS ON GAMMA RAY PENETRATION. William W. Pratt and Herbert J.

Kouts. Feb. 8, 1952. Decl. Dec. 15, 1955. 4p. \$1.80(ph OTS); \$1.80(mf OTS).

Preliminary results are presented on the effect of aluminum spheres submerged in water on  $\gamma$ -ray penetration through the water. The spheres varied in diameter from 4 to 18 in. and were submerged from 0 to 36 in. below the surface of the water. It was found that the increase in  $\gamma$ -ray leakage integrated over the surface of the water was not very sensitive to the depth of the sphere. (M.P.G.)

### 3744 CF-54-5-200

Oak Ridge National Lab., Tenn.

#### REQUIREMENTS FOR HRT TOP PLUG. P. N.

Haudenreich. May 27, 1954. Decl. Dec. 21, 1955. 14p. Contract [W-7405-eng-26]. \$3.30(ph OTS); \$2.40(mf OTS).

The shield directly over the HRT core should be no thicker than 5 ft. Various shielding materials and arrangements have been investigated, and the results are summarized. Shields composed of iron-aggregate concretes and 1 in. of Pb appear to be the most satisfactory. A shield of Fe and  $H_2O$  would also be satisfactory but might be much more expensive. (M.P.G.)

## SPECTROSCOPY

### 3745 ANL-4400

Argonne National Lab., Lemont, Ill.

#### MASS SPECTROSCOPY AND CRYSTAL STRUCTURE DIVISION QUARTERLY [FOR] SEPTEMBER 1, 1949

THROUGH NOVEMBER 30, 1949. Jan. 19, 1950. Decl. Dec. 13, 1955. 16p. Contract W-31-109-eng-38. \$3.30(ph OTS); \$2.40(mf OTS).

A new stable isotope was found to be present in V at mass 50 with an abundance of one part in 400 of the main isotope at mass 51. A sample of fission I was found to have a ratio of  $I^{129}$  to  $I^{127}$  equal to 6.44; this permitted an accurate determination of the half life of  $I^{129}$ . Three irradiated Pu samples were analyzed to determine the

abundances of the three isotopes at 239, 240, and 241. It was found that an analysis could be obtained with as little as two  $\mu$ gms of Pu. It was found that residual gases are an important source of error in precise atomic mass comparisons owing to differential retardation of the ions during analysis. Two different types of stable quadruply charged Sm ions are produced by 600-volt electron bombardment. A change in the crystal structure of diamond caused by neutron irradiation is discussed. Crystal structure results are given for  $YF_3$ ,  $\alpha$ -YOF,  $\beta$ -YOF,  $BiF_3$ ,  $Bi_2OF_4$ ,  $\alpha$ -HBO<sub>2</sub>,  $\beta$ -HBO<sub>2</sub>, and  $La_2O(OH)_4$  and  $Nd_2O(OH)_4$ . (auth)

### 3746 CP-2261

Chicago. Univ. Metallurgical Lab.

#### A METHOD FOR NEUTRON ENERGY MEASUREMENT.

V. Alexander Nedzel. Oct. 18, 1944. Decl. Dec. 15, 1955. 11p. Contract [W-7401-eng-37]. \$3.30(ph OTS); \$2.40(mf OTS).

A special magnetic spectrometer for determining the momenta of recoil protons is designed. The spectrometer components are discussed, and the expected performance calculated. (D.E.B.)

### 3747 NYO-3535

New Hampshire. Univ., Durham.

PROGRESS REPORT. Helmut M. Haendler. July 15, 1954. Decl. Dec. 7, 1955. 13p. Contract AT(30-1)-1097. \$4.80(ph OTS); \$2.70(mf OTS).

The infrared and ultraviolet spectra of  $BrF_3$  and  $BrF_5$  were investigated. An ultraviolet absorption method for the determination of  $UF_6$  in gas streams is discussed. (C.W.H.)

## THEORETICAL PHYSICS

### 3748 CP-1818

Chicago. Univ. Metallurgical Lab.

THE EFFECT OF THE MAXWELL DISTRIBUTION OF VELOCITIES ON THE NEUTRON DENSITY AND DIFFUSION LENGTH IN A METAL SPHERE. Gilbert N. Plass. June 27, 1944. Decl. Dec. 19, 1955. 13p. Contract [W-7401-eng-37]. (A-2644). \$3.30(ph OTS); \$2.40(mf OTS).

The change in the simple  $Sh\mathcal{K}r/\mathcal{K}r$  distribution of neutrons in a spherical lump of U caused by the distribution in velocities of thermal neutrons is calculated. If the calculated curve is fitted as well as possible by a simple  $Sh\mathcal{K}r/\mathcal{K}r$  curve, it is shown that the value of  $\mathcal{K}$  obtained in this way is a function of  $r_0$ , the radius of the sphere. For small radii the  $\mathcal{K}$  obtained in this manner will be as much as 25% greater than the  $\mathcal{K}$  corresponding to average velocity neutrons. The change in the thermal utilization caused by the distribution in velocities is discussed. The flux of neutrons into a sphere is calculated taking into account the velocity distribution, and this is compared with the usual theory. (auth)

### 3749 LA-609

Los Alamos Scientific Lab., N. Mex.

CRITICAL DIMENSIONS OF WATER-TAMPED SLABS AND SPHERES OF ACTIVE MATERIAL. E. Greuling, H. Argo, G. Chew, M. E. Frankel, E. J. Konopinski, C. Marvin, and E. Teller. Aug. 6, 1946. Decl. Dec. 16, 1955. 24p. Contract [W-7405-eng-36]. \$4.80(ph OTS); \$2.70(mf OTS).

The magnitude and distribution of the fission rate per unit area produced by three energy groups of moderated neutrons reflected from a water tamper into one side of



an infinite slab of active material is calculated approximately. This rate is directly proportional to the current density of fast neutrons from the active material incident on the water tamper. The critical slab thickness is obtained by solving an inhomogeneous transport integral equation for the fast-neutron current density into the tamper. Slight alterations in the theory were made so that one could approximately compute the critical radius of a water-tamped sphere of active material. The derived formulae were applied to calculate the critical dimensions of water-tamped slabs and spheres of solid  $UF_6$  having various isotope enrichment fractions. (auth)

**3750** RL-15.6.49

[California. Univ., Berkeley. Radiation Lab.]  
THE MATHEMATICAL THEORY OF SCATTERING. D. Bohm, J. Weinberg, E. Barankin, and A. Horn. [1944?]. Decl. Dec. 7, 1955. 92p. Contract W-7405-eng-48. (Spec.-49). \$13.80(ph OTS); \$4.80(mf OTS).

Consideration is given to the mathematical theory of scattering as applied to electromagnetic separation processes for U. Included are discussions on single scattering, calculations of contamination, and contamination resulting from multiple scattering. (B.J.H.)

#### URANIUM AND URANIUM COMPOUNDS

**3751** A-1072

Madison Square Area, Manhattan District, New York.  
TECHNICAL INFORMATION REPORT FOR THE PERIOD JANUARY 1-JANUARY 31, 1945. Feb. 15, 1945. Decl. Dec. 8, 1955. 31p. \$6.30(ph OTS); \$3.00(mf OTS).

Graphite cakes were added as filling to the  $UF_4$ -Mg reduction bomb. Magnesium, high in N content, showed decreased recasting and remelting yields. Deoxidation and pressing the charge material did not change the casting yield. The processing of carnotites is described. (C.W.H.)

**3752** AECD-3856

Du Pont de Nemours (E. I.) & Co., Wilmington, Del.  
THE MAGNITUDE OF THE  $\eta$  EFFECT. E. P. Wigner. Apr. 25, 1951. 3p. Decl. Dec. 2, 1955. (DPW-2071). \$1.80(ph OTS); \$1.80(mf OTS).

**3753** AECD-3874

Carbide and Carbon Chemicals Corp. Y-12 Plant, Oak Ridge, Tenn.

CRITICAL DIMENSIONS OF UNTAMPED CONICAL VESSELS. Raymond Murray. Aug. 25, 1947. Decl. Dec. 6, 1955. 6p. [Contract W-7405-eng-26]. (A-4.390.31). \$1.80(ph OTS); \$1.80(mf OTS).

A mathematical analysis of Poisson's equation for a spherical sector, which approximates a right circular cone, is presented. The ratio of the critical dimensions of an equivalent sphere to the height of the sector for various sector angles is derived from a comparison of first eigenvalues. (auth)

**3754** AECD-3909

[Tennessee Eastman Corp., Oak Ridge, Tenn.]  
INTERACTION OF SOLUTIONS OF URANIUM SALTS. Raymond Murray and George W. Schmidt. Jan. 2, 1947. Decl. Dec. 13, 1955. 12p. (A-7.390.20). \$3.30(ph OTS); \$2.40(mf OTS).

Criticality studies on vessels containing U solutions in proximity with other containers are reported. Sample calculations are included. (C.W.H.)

**3755** CC-2522

California. Univ., Berkeley. Radiation Lab.  
MELTING POINT-COMPOSITION DIAGRAMS IN THE U- $UBr_3$  SYSTEM. Carl Thurmond. Dec. 20, 1944. Decl. Dec. 15, 1955. 5p. Contract W-7405-eng-48. \$1.80(ph OTS); \$1.80(mf OTS).

A portion of the liquid-solid phase equilibrium region of the system U- $UBr_3$  has been investigated by the method of thermal analysis. Uranium tribromide was prepared by introducing bromine vapor into a bulb containing finely divided uranium formed from the hydride. Cooling curves were obtained with the tribromide and then with various compositions of tribromide and uranium. The information obtained showed that no solid subhalide exists but that the metal was soluble in the halide. (auth)

**3756** CF-53-9-96

Oak Ridge National Lab., Tenn.  
SHIELDING PROPERTIES OF URANIUM. C. L. Storrs and J. M. Miller. Sept. 30, 1953. Decl. Dec. 19, 1955. 23p. Contract [W-7405-eng-26]. \$4.80(ph OTS); \$2.70(mf OTS).

Neutron and  $\gamma$  attenuation in a 3 in.  $\times$  3 ft.  $\times$  3 ft. slab of natural U were measured in the Lid Tank. Measurements were made with and without a thermal neutron shield of boron carbide-loaded plexiglass. Results are presented in graphical form. (B.J.H.)

**3757** CF-338

Columbia Univ., New York.  
MEMORANDUM ON THE CRITICAL CONDITION FOR A FAST NEUTRON CHAIN REACTION INSIDE A SPHERICAL SHELL OF URANIUM METAL. Bernard T. Feld and Leo Szilard. Dec. 26, 1941. Decl. Dec. 13, 1955. 8p. (A-387). \$1.80(ph OTS); \$1.80(mf OTS).

The critical size for the maintenance of a fast neutron chain reactor in a sphere of  $U^{235}$  or other element having high cross section for slow neutron fission is calculated when the material is surrounded by shell of uranium metal. The first approximation to the appropriate diffusion equation is used, in which it is assumed that there are two categories of neutrons: "slow," or neutrons below the fission threshold of  $U^{238}$ , and "fast" neutrons. The processes of fission, inelastic scattering and elastic scattering are considered. It is shown that the addition of the uranium metal shell reduces the mass of reacting material by a factor of about 12. The amount of core material would be 1.5 times greater if there were no fast neutron fission in the  $U^{238}$  shell. (auth)

**3758** CP-1589

Chicago. Univ. [Metallurgical Lab.]  
RESONANCE ABSORPTION IN LUMPS AND MIXTURES. S. M. Dancoff and M. Ginsburg. Apr. 17, 1944. Decl. Dec. 14, 1955. 47p. Contract [W-7401-eng-37]. (A-2254). \$7.80(ph OTS); \$3.30(mf OTS).

The resonance absorption of a lump is described in terms of three components. Calculations of resonance absorption are carried out using the model for the resonance spectrum of uranium recently derived; calculations are also made with variations of this model which involve local fluctuations in level strengths. For metal and oxide lumps the agreement with observation is satisfactory. For dilute mixtures, whose resonance activation was measured by Mitchell, computed values fall 20% to 30% above measured ones. (auth)



**3759** CP-1598

[Chicago. Univ. Metallurgical Lab.]

## THE INFLUENCE OF OPERATION ON TUBALLOY.

Frederick Seitz. Apr. 21, 1944. Decl. Dec. 15, 1955.

33p. Contract W-7401-eng-37. (A-2260). \$6.30(ph OTS); \$3.00(mf OTS).

The influence of pile operation on the mechanical properties of U is estimated, particularly the hardening which results from atomic displacement, and the changes in mechanical properties due to the presence of fission products. It is concluded that the metal would become very hard and brittle as a result of displacement during the first day of operation if the diffusion of the interstitial atoms and vacancies produced did not reverse the displacement. The volume of rare gases generated in 100 days of operation is sufficient to cause considerable trouble. (B.J.H.)

**3760** CP-1732

Chicago. Univ. Metallurgical Lab.

## THE DIFFUSION LENGTH OF THERMAL NEUTRONS IN URANIUM.

D. J. Hughes and E. W. Bragdon. May 27, 1944. Decl. Dec. 16, 1955. 10p. Contract [W-7401-eng-37]. (A-2445). \$1.80(ph OTS); \$1.80(mf OTS).

Measurements made in a uranium cylinder result in a mean value of 1.55 cm for the diffusion length  $L$  for distances of 1 to 4 cm from the base of the cylinder. Calculations give a value which agrees with the experimental result and show further that  $L$  increases from 1.40 to 1.63 cm as the neutrons diffuse a distance of 5 cm into the uranium. (auth)

**3761** CT-816

Ames Lab., Ames, Iowa.

## TECHNOLOGY RESEARCH—METALLURGY. PART II OF REPORT FOR MONTH ENDING JULY 24, 1943. 22p. \$4.80(ph OTS); \$2.70(mf OTS).

Additional properties of U-Al, U-C, and U-Bi alloys were determined. Anhydrous  $\text{ThF}_4$  was prepared. The effects of liner constituents, ammonium oxalate insoluble material, and bomb dimensions on U production were investigated. The U casting program was continued. (C.W.H.)

**3762** HW-12832

Hanford Works, Richland, Wash.

## THE SURFACE PREPARATION OF URANIUM FOR X-RAY DIFFRACTION STUDIES BY THE SPECTROMETER TECHNIQUE. J. H. Bach and J. B. Burnham, Jr. Mar. 24, 1949. Decl. Dec. 6, 1955. 6p. \$1.80(ph OTS); \$1.80(mf OTS).

Uranium samples cut from alpha rolled rods were subjected to three different treatments in order to determine the best method of surface preparation for x-ray-diffraction investigations by the spectrometer method. Electropolishing of the samples indicated three different surface conditions whose appearance or disappearance depended on the electropolishing time. The last of these phases, which begins to appear after 3 to 5 minutes electropolishing and completely dominates the surface after about 20 to 30 minutes of electropolishing, was found to be the desired surface, nominally free of strains imposed by the

cutting and grinding of the sample. This method has been adopted and will be used in future work of this type. Etching in warm 50% nitric acid produced identical results. This method is inferior to electropolishing because the reaction proceeds at a much slower rate, and long etching times result in excessively pitted surfaces. The classical metallographic technique, which consists in alternative polishing and etching the sample, produced a second x-ray-diffraction pattern which is superimposed upon the pattern predicted by the accepted uranium structure. This second pattern can be indexed as a simple cubic lattice with an " $a_0$ " of 6.642 Å, indicative of a new phase or compound formation. However, both the significance and the reason for the appearance of this pattern have yet to be explained satisfactorily. (auth)

**3763** K-299(Rev.)

Carbide and Carbon Chemicals Corp. K-25 Plant, Oak Ridge, Tenn.

## IMPROVEMENTS IN THE PRECISION AND ACCURACY OF THE FISSION COUNTING METHOD. C. A. Kienberger and R. E. Greene. Apr. 15, 1949. Decl. Dec. 27, 1955. 20p. Contract [W-7405-eng-26]. (KLO-50(Rev.)) \$3.30(ph OTS); \$2.40(mf OTS).

The precision of the fission counting method for  $\text{U}^{235}$  in the Works Laboratory was improved by locating and eliminating two large sources of error. A systematic study was made of each step in the analytical procedure. Variations in the surface condition of the Ni disks upon which the U is plated was the major cause of erratic sample results. A secondary cause was the rubber gaskets used in the electroplating operation, which deteriorate and consequently cause low results by absorption of the U. Electropolishing the surface of the Ni disks and the use of rubber gaskets showing no sign of aging have significantly increased the precision of the method. (auth)

**3764** LA-1188

Los Alamos Scientific Lab., N. Mex.

SHORT PERIOD  $\gamma$ -RAYS FROM  $\text{U}^{235}$  FISSION PRODUCTS.

J. E. Brolley, Jr. and M. S. Livingston. Jan. 15, 1951. Decl. Dec. 10, 1955. 22p. Contract W-7405-eng-36. \$4.80(ph OTS); \$2.70(mf OTS).

A search for  $\gamma$ -ray activities with period 1 to 100 msec from the thermal neutron fission of  $\text{U}^{235}$  gave negative results. The shortest observed was  $0.43 \pm 0.03$  sec. The period of  $\text{B}^{12}$  was found to be  $27 \pm 3$  msec. The cyclotron beam was pulsed to supply 1 to 10 msec neutron bursts. Coincidence scintillation detectors were employed. (auth)

**3765** NYO-5195

Mallinckrodt Chemical Works, St. Louis.

## A REPORT ON THE EXAMINATION OF URANIUM DIOXIDE WITH THE ELECTRON MICROSCOPE. W. A. Oppold. Aug. 27, 1946. Decl. Dec. 1, 1955. 4p. \$1.80(ph OTS); \$1.80(mf OTS).

No specific differences were noted in the particle size and shape of du Pont and Mallinckrodt samples of  $\text{UO}_2$ . (K.S.)

Refer also to abstracts 3601, 3672, and 3749.